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## LIST OF ABBREVIATIONS, ACRONYMS

DG	Distributed Generation
$C_{rotor}$	Rotor side converter DFIG
$C_{grid}$	Grid side converter
PID	Regulator Proportional, Integral, Derivative
$K_p$	Proportional gain of PID controller
$K_d$	Derivative gain of a PID controller
$K_i$	Integral gain of a PID controller
SW Bus	Balance bus or Swing Bus
PV Bus	Generator bus
PQ Bus	Load bus
DFIG	Double-fed induction generator
WRSG	Wound rotor synchronous generator
PMSG	Permanent magnet synchronous generator
WTIG	Wind turbine induction generator
WRIG	Wound rotor induction generator
WDHS	Wind diesel hybrid system
IGBT	Insulated-gate bipolar transistor
AGC	Automatic Generation Control
BESS	Battery-based energy storage system
DL	Dissipation load
WO	Wind mode only
DO	Diesel mode only

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WD	Wind-diesel mode
OLTC	On load transformer tap changer
SM	Synchronous machine
ASM	Asynchronous machine
PWM	Pulse width modulator
CCI	Current controlled inverter
PPL	Positive power limit
PLL	Phase Locked Loop
STATCOM	Static Synchronous Compensator
SVC	Static Var Compensator

## LIST OF SYMBOLS AND UNITS OF MEASUREMENT

$P_m$	Mechanical power delivered by the wind turbine	kW
$\lambda$	Wind generator speed ratio	without unit
$\beta$	Orientation angle of the blades 'pitch angle' wind	deg
$V_{wind}$	Wind velocity	m/s
$C_p$	Aerodynamic efficiency of the turbine	without unit
$\rho$	Density of air	Kg/m <sup>3</sup>
$A$	Swept area of the turbine	m <sup>2</sup>
$P_{m-pu}$	Nominal power	pu
$T_m$	Mechanical torque	pu
$R_m$	Radius assigned to the area A	m
$\Omega_m$	Speed of the wind generator	rad/s or pu
$V_r$	Voltage control of the rotor side converter of DFIG	pu
$V_{GC}$	Voltage Control of the grid side converter of DFIG	pu
$\Omega_r / \omega_r$	Rotation speed of wind rotor DFIG	rad/s or pu
$\Omega_s / \omega_s$	Stator speed of DFIG	rad/s or pu
$P_m$	Mechanical power generated by the wind turbine DFIG	kW or pu
$P_s$	Stator electrical power by the wind turbine DFIG	kW or pu
$P_r$	Rotor electric power	kW or pu
$P_{gc}$	Active power emitted by the converter Cgrid DFIG	kW or pu
$Q_s$	Reactive power emitted by the stator of the DFIG	kVAR or pu
$Q_r$	Reactive power transmitted by the rotor of the DFIG	kVAR or pu
$Q_{gc}$	Reactive power emitted by the converter DFIG	kVAR or pu

$T_m$	Mechanical torque applied to the rotor of DFIG	N.m or pu
$T_{em}$	Electromagnetic torque applied to the rotor by the DFIG	N.m or pu
$f$	Grid frequency	Hz or pu
$J$	Coefficient of inertia of the rotor and wind DFIG	without unit
$U_i$	Voltage at i bus	V or pu
$Q_{comp}$	Reactive power voltage compensation	kVAR / pu
$Q_{chg}$	Reactive power consumed by a load	kVAR / pu
$I_i$	Current at bus i	A or pu
$V_{L-L}$	Line voltage of WHDS	V or pu
$P_{STEP}$	Power to the last significant bit of WHDS	kW or pu
$P_{REF}$	Power frequency reference of WHDS	kW or pu
$P_D$	Power generated by the wind turbine of WHDS	kW or pu
$P_{D-NOM}$	Rated power dissipation of DL loads of WHDS	kW or pu
$P_T$	Power generated by the wind turbine WHDS	kW or pu
$P_{T-NOM}$	Rated power of wind turbine WHDS	kW or pu
$P_S$	Power consumption / generated by the BESS WHDS	kW or pu
$P_{S-NOM}$	Rated power of the BESS WHDS	kW or pu
$P_L$	Active power consumed by the WHDS	kW or pu
$P_{L-NOM}$	Nominal load power (kW) of WHDS	kW or pu
$p$	Number of pole pairs of the MS WHDS	without unit
$P_{S-REF}$	Reference power for controlling the BESS of WHDS	pu
$P_{DL}$	Reference power to control the load dissipation of WHDS	pu
$s$	Sliding MAS	without unit

## INTRODUCTION

### 3.1 General

The present demand for electricity is increasing in the worldwide day by day. Climate protection and environmental fossil sources of electric power require undertaking adequate technical and economic solutions to increase the production rate of power of non-fossil types. Moreover, the liberalization of electricity markets, which started a few years ago, also allows the development of a new offering for the production of electricity. Some small-scale producers cannot be connected to the transmission of electricity; the connection is made directly to the distribution network.

These specific behaviors have been gradually developed and now defined as the Distributed Generation and Decentralized Generation. The new situation created by this type of generation has made this problem one of the most studied in the field of electric power systems topics. The distributed generation systems include distributed generation (local) with small capacity installations connected to the electricity network. This type of production is generally associated with renewable energy sources such as: wind, solar, hydro, biomass, etc. Distributed generation allows the collection of energy from many sources allowing for a little detrimental impact environment.

Distributed generation resources are connected to the same transmission network for central stations. Various technical problems arise related to harmonics, reliability, protection, energy storage and control. In this scale, several researchers have made efforts to study and analyze the potential problems that might occur during the interaction between the DG's and the power grid, and have developed methods to understand the dynamic behavior of the variables involved such as frequency, voltage and electrical power of the new network architecture (Nazari et al., 2010). More recent research has been focused on one hand to improve the energy efficiency with the increasing penetration of DG's and reducing other costs from the creation of the most cost-effective technical solutions (Du Can et al., 2014). It is noted that, under certain conditions, the frequency level of the network may exceed its desired limits.

Hence, a problem of frequency fluctuation may arise in order to achieve a possible collapse of the network. Due to the fluctuating behavior of renewable energy sources (RES), balancing, generation and demand are not an easy task to control (because we do not get constant power from the renewable energy sources due to the natural situation). On other hand the standalone installation of renewable is not efficient. Therefore, power from renewable energy should inject in the traditional power grid to get a better efficiency. The integration of storage systems for power network can improve penetration of DG to provide backup sources or power to the loads (consumers). Therefore, this phenomenon leads to control the variables in order to maintain an acceptable level of frequency in the power network by increasing penetration of DG.

Therefore, analysis of the results found by some previous research will be explained in the literature review chapter.

### **3.2 Motivation**

Several problems must be faced in the power grid for the integration of DG's distribution systems. Some examples of these problems are showing below:

- i) The level of voltage: There are two types of DG's: rotary type (directly connected to the network via induction or synchronous generators), and the static type (indirect interface using power electronic converters). DG units equipped with an induction motor that is directly connected can affect the level of voltage due to their consumption of reactive power. Increasing the penetration of DG has a direct effect on the profile of the voltage distribution network. Moreover, the DG units are equipped with power converters and can have positive impacts on the voltage stability margin of the network, because the DG's can be adjusted to inject a fixed amount of reactive power to the system. At this stage, the methods of compensation for reactive power of DG's are established by adopting costly equipment. Power converters used for static type DG can also be a source of disturbance and harmonics on the stable operation of the network.

- ii) The level of power quality: Two types of power quality are significantly considered: (1) Transient voltage fluctuations and (2) The harmonic distortion of the voltage. Depending on the specific circumstances, the DG may either decrease or increase the quality of the voltage received by using the distribution network. Analyses were done to understand the dynamic aspect of the energy passed through the distribution lines. However, several other factors can be sources of this problem as DG's technology, the number of DGs and their locations, control devices etc.
- iii) The Energy Storage: Storage systems play a very important role to investigate a high penetration rate for DG. The dynamic interaction with the DG, power grid and, power converters can be a source of disturbance in the operation. Secondly, the energy storage equipment can provide increased penetration of DG. Many applications including micro-networks, the autonomous operation can be investigated.
- iv) Dynamic Stability: Traditional transmission network is a passive network (power flow in one direction). Indeed, the stability problem was not major but has an impact in most circumstances in the transmission network. With the integration of renewable resources, stability is highly considered in the evaluation of DG systems, especially in increasing the rate of penetration. Integration of DGs may have an impact on the system due to the generation of harmonics. In addition, active and reactive power compensators are normally attached to the certain types of DG, such as induction generators that are directly connected to the system. These compensators can change the system at certain levels. Several examinations of the dynamic behavior of the system parameters are made here. However, research at this stage is still unsatisfactory and has opportunities for improving the performance of control methods to improve the behavior of frequency to develop a modern distributed generation system.

### 3.3 Objectives

Referring to the points already mentioned above, several themes of objectives can be deployed. Including:

1. Investigate the literature in the field of research to identify the problems of frequency fluctuation in power systems with DG;
2. Analyze the technical impacts of DG on the distribution system: the behavior of the frequency and quality of active and reactive power during the power flow;
3. Model and assess the contribution of systems energy storage, especially batteries, on the overall system by connecting DG to the grid. This is to optimize the use of renewable energy resources in investigating the mode of operation of the network elements with respect to the availability of energy and loads connected to the network;
4. Investigate the frequency fluctuation in the presence of wind energy source;
5. Analyze the behavior of the frequency in the presence of wind turbine and an energy storage system.
6. Compare PID and Fuzzy logic controller and observe the fluctuation behavior of frequency.

## CHAPTER 1

### LITERATURE REVIEW

The contribution of this literature review is to collect the information and investigate the results of recent research based on the problems of penetration of DG and the problems of frequency control to identify the constraints in power grid also identify to the opportunities for its improvement. In the first part of this chapter, the system of distributed generation has been exposed. In the second part, we discussed the increasing penetration of DGs extensive research in their adaptation with the appropriate storage systems. The methods developed in this concern will be presented here. In the third part, the stability conditions of the frequency in the grid have been used in referring to the data from the present research.

#### 1.1 Concept of Traditional Power Systems

In this present time, most of power system generate and distribute electricity in terms of the following conditions (Kauhaniemi and Kauhaniemi, 2004).

- Power produced in large power generation plant. It normally situated very near to the primary energy source and away from the consumer.
- Power supplied to the consumer using with high voltage (HV), medium voltage (MV) and low voltage (LV) networks.
- To reach the electricity to the final stage (consumer), there are three steps to be considered; generation, transmission and distribution.

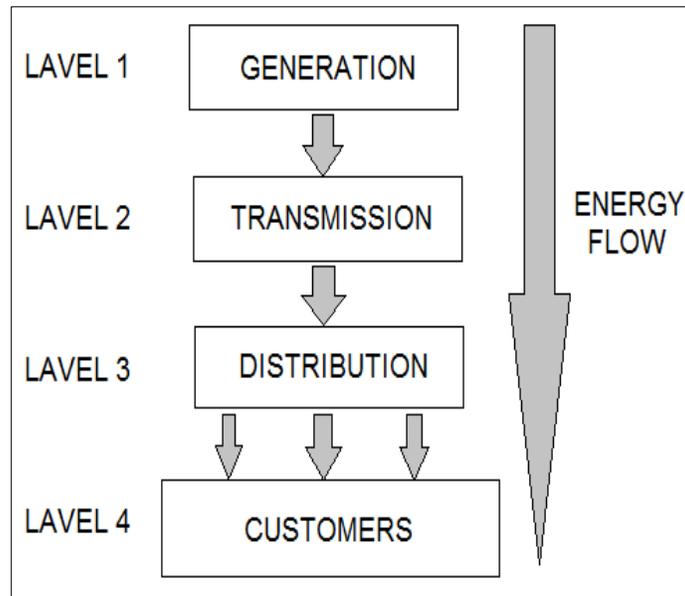


Figure 1.1: Traditional concept of power supply  
Adapted from Kauhaniemi and Kauhaniemi (2004)

## 1.2 Concept of New Power System

Today, new technologies have been developed to reduce the environmental pollution and fulfill the electricity demand in the power grid. These technologies permit to produce the electricity in a small power plant ( $5\text{kW} < 5\text{MW}$ ). Increasing penetration of RES to reduce the pollution of environment is leading to develop new power supply schemes in the power engineering sector. In this concept, shown in figure 1.2, the power can be supplied by both directions, one is from the centralized generation and another is from distributed generation. In this case, the energy can be produced very close to the consumers (Vignolo and Zeballos, 2002).

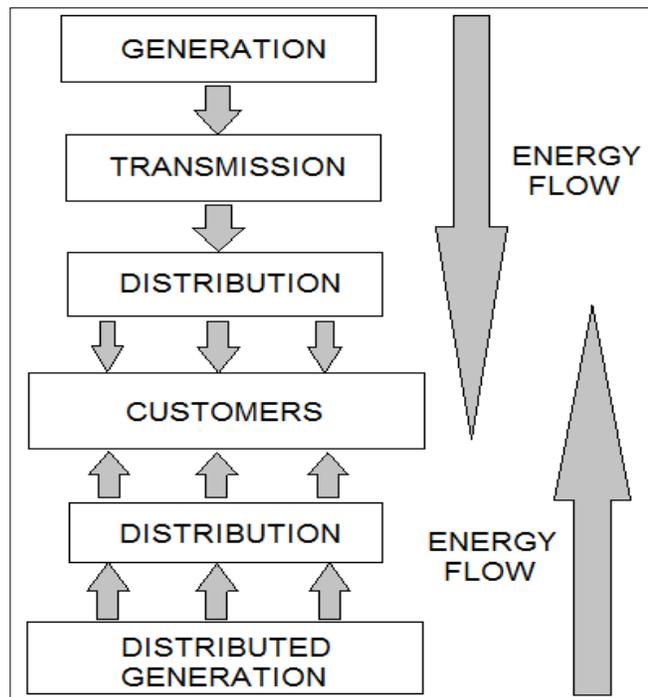


Figure 1.2: New concept of power supply  
Adapted from Vignolo and Zeballos (2002)

### 1.3 The Distributed Generation (DG)

The traditional power distribution networks have a vertical structure in which electricity is produced by power plants of large energy generation capacity, and is delivered to consumers through transmission and distribution lines. This type of networks is characterized by low energy efficiency and a harmful impact on the environment. DG technology, featuring a radial architecture is vastly developed to reduce the problems related to the environment and energy efficiency.

In this part, we present the definition of DG, followed by the associated technology, its scope and its modes of operation. The technical impact of frequency in the power grid will be exposed after accounting the potential benefits and drawbacks.

### **1.3.1 Definition**

Many authors have cited various types of definitions of DGs referring to the papers previously published. The Department of Energy of the United States (DOE) (Borenstein and Bushnell, 2015), defines DG as follows: "This is the modular electric generation where the storage is located near the consumer". DG Systems included with biomass, combustion turbines, solar/ photovoltaic systems, fuel cells, wind turbines, microturbines and storage technologies. The DG may be either independent or connected to the grid. Usually those are connected to the network in the distribution system.

Bayod Rùjula et al., (2005) cited an additional definition of DG: "The DG system is the integrated or stand-alone use of small resources of power generation by consumers". In practice, this is a facility for generating the electricity, which can be located at or near the consumers such as industrial areas, commercial buildings, etc. DG is a source of electrical energy, connected one side to the distribution network and another side to the load. Some energy sources of renewable energies are showing below:

- Wind Energy
- Micro-turbines;
- Hydro-electric energy;
- Biomass;
- Photovoltaic system
- Thermoelectric plants.

This type of energy is called non-fossil. It provides a non-destructive clean energy to the environment, without loss on the distribution network, with performance, reliability and better profitability.

### **1.3.2 Benefits of DG**

Barker and De Mello (2000) mentioned that the integration of large number of distributed generators at LV or MV can be used to supply electricity some loads. These types of

generators have smaller size than traditional generators. Some benefits of DG cited by (Van Thong et al., 2005) are shown below:

- Intention of DG connection to the grid is to increase the accuracy of electricity supply to the consumers using local sources, and to reduce losses of the transmission and distribution network.
- Connection of DG to the grid can improve frequency and voltage profile, quality of power and stability of voltage. Also, it can handle large loading situations in the network.
- Improved energy efficiency by cogeneration plants 'Combined Heat and Power' (simultaneous production of power and heat), especially for heat consumers;
- To setup a DG in a power system requires less time and investment to recover its initial cost in terms of profits in future.
- DG offers consumers a continuous and reliable supply;
- DG helps to raising the level of voltage in the grid: it is an advantage in terms of support to the networks with a difficult voltage supply;
- DG offers flexibility because of its small size and the time allotted for installation;
- DG systems can offer economic and environmental benefits.

### **1.3.3 Drawbacks of DG**

- Some technologies of DG are based on current sources which require power converters for connecting to the grid. This fact contributes to the generation of harmonics affecting the network voltage;
- DG may force a power flow in both directions. Therefore, energy can be supplied to an electric high-voltage grid. This can produce stability problems on the voltage and requires changes in the operation and protection system;
- Electricity sent to the grid can cause a power surge;
- The power flow in DG systems can be inefficient on the protection / security systems;

- DG can negatively affect the quality of power: The power generated is dependent on natural conditions (wind speed, sunny day);
- The penetration level of DG, power injection to the grid may cause power losses in the distribution network.

#### **1.3.4 The technologies of DG**

A large technology is implemented to meet the varied application of DG technologies. These applications are diverse with respect to the characteristics of the load that is connected to the DG (thermal, standalone or connected to the power grid with needs, size, condition and quality of energy, environmental constraints). Bayod Rùjula, (2009) cited some applications:

- Rural Technology (Autonomous DG);
- Reserve Sources;
- CHP (Combined Heat and Power) also called cogeneration system which injects energy through the grid when the DG capacity is greater than the demand of the load.

#### **1.3.5 Impact of DG on Power System**

The technical impact of DG on power systems can be evaluated at different stages; consistency of protection, stable state of equilibrium; and dynamic behavior. Assessments of the impact on the transmission system involving major studies, considering various emblematical operating scenarios (e.g., peak load). In the power systems, hydropower gives a very large amount of considerable contribution in the power network. The stochastic nature of few DG's (like wind) may also lead to consider alternative power sources with various levels of production. These scenarios can be analyzed by comparing the results get from before and after the integration of DG's for certain studies. Two types of analysis are performed by (Lopes et al., 2007):

- Overall performance of power systems;

- Analysis of the behavior of power networks in the specific areas, specificities of the adopted energy conversion systems and characteristics of any local power network.

### 1.3.6 Impact of DG on Voltage Regulation

In the power system DG regulate the voltage using the on-load tap changer transformer (OLTC) in substations. It is based on one way power flow where the voltage regulators are connected to the line drop compensation (LDC). Presence of DG in the power system can change the voltage profile in the feeder by switching the direction of active and reactive power flow. DG in voltage regulation has negative or positive impacts; it depends on the characteristics of DG installation areas and distributed generators (Barker and De Mello, 2000). Figure 1.3 shows, DG installed with LTC transformer that fitted with LDC. It also shows that with DG connected to the grid, lower voltage level is obtained in feeder rather than the connection without DG in the grid. The injection of large amount of active and reactive power from DG may cause over voltage in the distribution feeder.

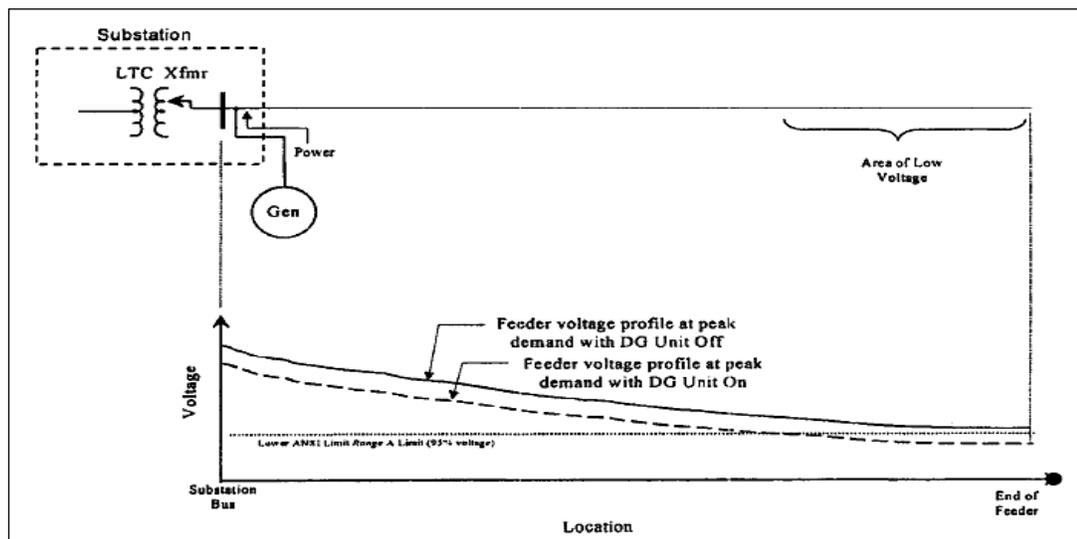


Figure 1.3: DG (with and without) voltage profiles  
Adapted by Barker and De Mello (2000)

### **1.3.7 Impact of DG on Losses**

One of the most common impacts of DG is the losses on the distribution feeder. Locations of DG units have an important role to reduce the losses in the power grid. Barker and De Mello, (2000) cited that optimal locations of DG can minimize losses as well as capacitor bank can minimize losses if it can be installed in a suitable location. The basic difference between DG and capacitor bank are, DG can inject both active and reactive power (P and Q) to the power network. On the other hand, capacitor bank can give reactive power (Q) flow to the power network.

The ideal areas of DG can be found using the load flow analysis, which can easily determine the optimum positions of DG in the network to reduce the losses. If any feeder creates large losses, installing a small DG on the system can have positive impact to reduce the losses.

### **1.3.8 Impact of DG on the Feeder Protection**

The most main characteristics of distribution networks is that the power flows radially, from the principal location of power generation to the feeders to maintain all loads. In this model it showed that protection device is connected to the feeders of the power network, in order to keep continues power supply to the loads and protect different types of equipment of power network from unbalance power flow (Khan, 2008). During the modeling of these protection devices, some features should be considered. It is true that the protection of whole power network is not possible using only of one kind of protection device. In large power network the protection is given by different types of protection devices based on the length of power network which can cover maximum length of protection. When modeling the protection strategy of a power network, operation between indicated protection devices should be able to reach a high range of reliable power network which can isolate the faulted portions of the networks and maintain the regular power flow in healthy parts of the networks. With this strategy, the global reliability of power network can be increased (Khan, 2008).

The DG in the power network will have a major impact on the operation of the protection devices, which affects the protection of distribution side feeder. The large penetration of DG in a distributed power network can increase the chance of fault in the whole power systems. This fault has also an impact on the protection devices. The protection devices can break down into two different ways: mal-trip (unplugging non-faulted parts) or fail-to-trip (by not unplugging faulted parts). A mal-trip is a case where a protection devices trip in place of other devices. This tripping happens when the protection device is outside of the protection zone while fault occurs. Figure 1.4 (a) shows mal-trip operation where a DG unit feeds a high level of fault. This type of operation isolates the healthy parts of the network to safe from the danger. Figure 1.4 (b) shows fail-to-trip operation where DG unit in a downstream fault condition (Häger et al., 2006).

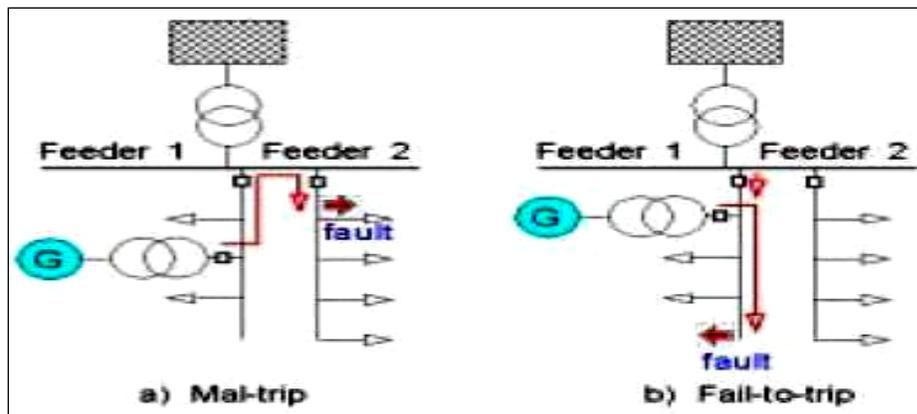


Figure 1.4: Mal trip and fail to trip  
Adapted from Häger et al. (2006)

### 1.3.9 Impact of the power converters to the DG

Renewable sources are generally connected to the main power networks via power converters, inverters and rectifiers. Under the effect of the dynamic interaction between the power grid and converter, the power quality is decreasing. DG connected to the distribution network can create a harmonic distortion to the system depending on which type of DG technology and power converters are connected. The implementation of passive filters can

limit the effect of this phenomenon by increasing the penetration rate of distributed generations. The purpose of this simulation is made by Kadir et al., (2012). They have modeled the system consisting of DC voltage source of DG, passive filter, inverter and P-Q control system.

### 1.3.10 Protection coordination

In power systems DG is connected to the grid with interconnection points known as points of common coupling (PCC). To keep away from damages on both sides (DG materials and utility materials during its fault condition) PCC has to be protected in the right way (Chattopadhyay et al., 1996).

(Perez and Urdaneta, 1999) mentioned that there are some protection rules and requirements for the interconnection points of DG. This interconnection protection of DG generally depends on transformer connection, kind of generators and the size of networks. Figure 1.5 shows DG connected to a power network through the transformer.

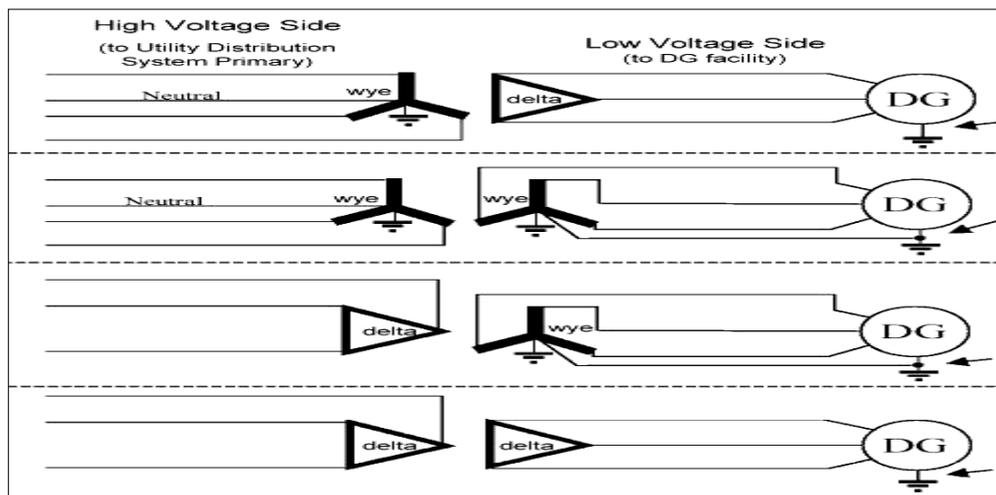


Figure 1.5: DG connected with power network using transformer  
Adapted by Khan (2008)

For load areas, there is a participation of DG. Short circuits in the transmission network may cause disconnection of a large portion of DG production and leading it to an overload situation. Furthermore, the voltage profiles in the area where DG has been disconnected can be affected seriously in the power network. Studies have shown that consistency time delays within the protection strategy of the transmission system and voltage of DG (interconnection protections) must be studied and implemented.

#### 1.4 Islanding of a power network

Barker and De Mello, (2000) observed that islanding occurs when one or more DG continuously supply a portion of power network which has been isolated from the main power system. The islanding only happens where generators can self excite and produce the power in an isolated area. The operation is shown in Figure 1.6, where the islanding could be done for the operation of an upstream breaker, automatic detection switch or a fuse. In some conditions, it is not preferable to reconnect the islanded portion when automatic reclosing switch is used. Moreover, the network system cannot able to maintain the power quality in the island (i.e. DG is no more under controlled by protection devices and continues supplying the power on its self island).

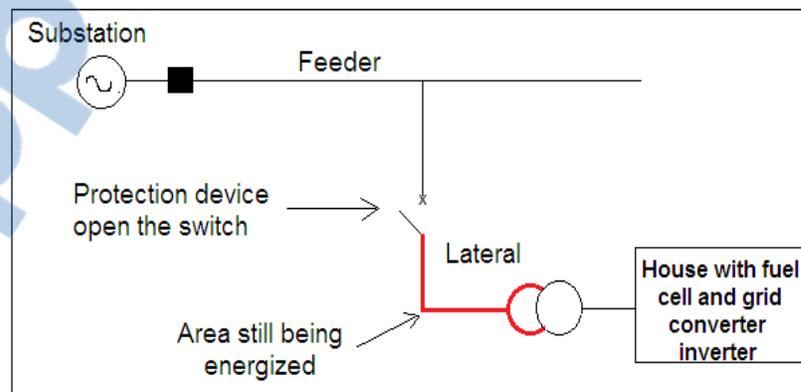


Figure 1.6: Islanding of a DG based power system  
Adapted from Barker and De Mello, (2000)

There are two forms of islanding; one is unintentional islanding and another is intentional islanding. An unintentional islanding is a situation where DG is no more running along with other power networks. Intentional islanding usually performed to increase the reliability of the power network.

#### **1.4.1 Intentional islanding**

Intentional islanding is a case where the reliability of power can be increased if a DG configured to maintain 'backup-islands' during upstream power outages. Barker and De Mello, (2000) described in their paper that during upstream faults the switch should open and generator should be able to maintain the demand of load on the islanded region and maintaining acceptable frequency and voltage levels in the islanded area. It is highly accepted that to support an island, DG must be assigned to be able to restart and carry the load of island after the switch has opened. Philip and Barker, (2000) also mention, to detect a fault in downstream of a switching area the switch has to be sensed and send a signal automatically to isolate the DG portions from the islanded fault zone.

#### **1.4.2 Islanding detection**

In the present time, to detect the islanding situation in a network, several methods and techniques are used based on the output of DG parameters and decision is taken to determine whether these parameters detect an islanding condition or not. The islanding determination methods may be defined into two main classes; local islanding and remote islanding methods. Pai and Huang (2001) and Mahat et al., (2008) mention that the local methods are divided into active and passive detection methods.

Remote islanding detection method is based on communication between the main power networks and DGs. This method is highly reliable than local detection methods, but it is expensive to apply in DG system. Local islanding detection method is depends on the measurement of system parameters in DGs area (i.e. voltage, frequency, etc). Active methods operation is directly connected to the power system but on the other hand passive methods

are based on detecting the fault on the measurement of the system parameters (Pai and Huang, 2001).

Passive methods observe the variation of parameters of power systems like phase displacements, levels of short circuit and rate of output power. In most situations disconnection of DG from power network affects the nominal network voltage, frequency and current. There is some negligible change in the power flow and the frequency when DG is connected to the main power network and it will not be enough for the beginning of a protective relay that is responsible for a DG disconnection from the network. One other side, if DG is not connected with the main power network, the variation in the output power and frequency will be enough to energize the protective relay to isolate the DG that preventing the occurrence of an islanding situation (Ropp et al., 2000). Active methods identify the islanding situation even there is perfect balance between loads and generation but in passive detection methods, it is not possible. Active detection methods directly cooperate with the operation of power system when small disturbance is introduced in the system.

## 1.5 Control of frequency

The balance between the load and the output power determines the frequency of the power system. In large interconnected networks, output power increases with frequency drop and vice versa. The first frequency control line is the local governor, which provides " reserve power flow " to the system. For DG, this type of control will be required for the operation of insulation. Frequency control in open loop always gives a constant value but in higher droop. For the case of closed loop control, the frequency is very sensitive with the actual energy (minimum droop), which requires control the governor to control the frequency.

In the present time, many researchers proposed a lot of control techniques in their pioneer research to develop the frequency controllers. The controllers are mainly based on Proportional, Integral and Derivative control techniques, Linear Quadratic Regulator (LQR) based control techniques, Classical control techniques. Artificial intelligence (AI) techniques and soft computing techniques are based on, Fuzzy logic techniques; Genetic Algorithm

based techniques, Particle Swarm based techniques and Neural network based techniques (Kouba et al., 2015).

Allu et al., (2015) considered a single area of power system to analyze the better performance of fractional order PID controller using root locus method. They compared fractional order PID controller with PID controller. After that they have extended their research work to the multi zone thermal power network with non linearity of generation rate constrain. Fractional order PID controller gives better response of dynamic system. In the end, they investigated the robustness of proposed controller by using transport delay.

Syamala and Naidu, (2014) illustrated the importance of automatic generation control and load frequency control in a power network. They have used automatic generation control system to maintain the defined frequency level in the power generators. Since, automatic generation control has feedback control system to control the frequency in a defined level. One of the basic objectives of automatic generation control system is to keep system frequency in a defined level to maintain the constancy performance of power networks. An expandable power network can be separated into a number of areas of load frequency control by connected with tie-lines. Without loss in the system, one can consider as a three area zone connected with tie-line. They are considering a hydro power system with two thermal power systems.

Zamee et al., (2013) found that due to increase of demand of power generation, increasing load in an industrial or any other area is a big threat for the power system. To solve this problem, balance between the load demand and generation is very important. In a large interconnected power network, an automatic generation control system is required for reliable operation of power generation. The main principle of automatic generation control system is to regulate the power outputs in a defined area to detect the change of frequency also the power of tie-line, so that the frequency can keep its desired value and power can interchange in the other area with a prescribed limit. In this paper, they have illustrated the use of artificial intelligence and PI controller to observe the load frequency control in an interconnected power network.

Kouba et al., (2015) presented the use of Artificial Bee Colony algorithm (ABC) with the load frequency control in a one, two and multi area interconnected power network. The proposed ABC computation is utilized to have better approximation of PID controller parameters which is based on load frequency control. The main capacity of load frequency control loop is to control the reactive power and frequency.

Nazari et Ilic., (2012) used the static droop to measure and analyze the sensitivity of the frequency with respect to disturbances due to increase penetration of DG in order to develop a decentralized frequency control system. They concluded that two main causes occur due to instability, improper setting of governors and the strong electrical interaction between DG. The system developed by Gerschgorin theory to use in overall system and provides flexibility between the DG. In addition, it has shown stability that applicable to all power distribution network based on low or medium penetration of DG. The system is made robust against minor disturbances on the electrical network. It requires high-performance of operation for all local controllers.

Ali and Abd-Elazim, (2013) observed an implementation of novel artificial intelligent search technique to observe the nonlinear load frequency controller parameters optimization with PID controller in a power network. Here, two area of non-reheat thermal system is taken which is controlled by PID controller. To reduce the time domain function, bacteria foraging optimization algorithm is used to find the parameters for the optimal controller.

Shiroie et al., (2013) analysed and proposed a robust multivariable type predictive controller to improve the load frequency control in multi zone power network. The control system is designed to study the nature of multivariable load frequency control system, uncertainty of power system and constraint of generation rate. The evaluation of results showed that the proposed control technique has satisfactory response with the system constraint and gives robust performance for a wide range of system uncertainty.

Vidyanandan and Senroy, (2013) proposed a method of primary frequency control by unloaded wind turbines using a variable droop. The application was carried out on a double-

induction motor connected to the network through the power converters. They presented the control of the active power of the variable speed wind turbines DFIG to participate in the primary control of the frequency. A reserve power generation capacity is needed to support the frequency control. The actual percentage of load shedding is to be decided according to the wind speed and the maximum allowed of the rotor speed of the DFIG. Using an additional control loop, these unloaded wind turbines are controlled in the same way as synchronous machines unstable frequency condition.

Ahmadi et al., (2013) proposed a novel converter and control scheme for flywheel energy storage systems to improve the grid frequency regulation and energy balancing in a smart grid network system. In this paper, they have used wind generator, PVs and some thermal units as a power network. The generated output power of wind turbine system is proportional to the cube of wind speed. If wind velocity changes for some reason, there will be some fluctuation in the generated wind power. The power fluctuation always leads the frequency fluctuation inside the power systems. That's why they have used energy storage systems to solve this problem whose object is to reserve energy when energy is plentiful and give back the energy at some emergency moment while energy is lacking on the power network. A fly wheel energy storage system is used here as a storage system.

Mohamed et al., (2012) showed a design of load frequency control using the technique of predictive control in a multi-zone electric system in the presence of wind turbines. In this system, each local controller is designed independently so that it can maintain stability of the entire closed-loop system. They have introduced a frequency-response model with multi-zone power system including wind turbines. Simulation results have shown that the closed loop system with the predictive controller is robust against the frequency disturbance of the system parameters. In addition, it noted that the wind turbine has a positive response on the overall system.

Takahashi and Tamura, (2008) have proposed an operation technique of fly wheel energy storage system (FESS) for improving the quality of network frequency in an isolated power system with a wind turbines. The frequency fluctuation due to output of wind generator is a

major problem in a power network. If wind farm installations increase day by day than it will be very difficult in the near future to control the frequency by using main power source. To improve the stability of wind farm power output, a storage system (fly wheel energy store system) for the output power smoothing has been proposed in this paper. As a storage system, they have used FESS. By using FESS, power compensation is very effective in power network. Also, this storage system has plentiful energy storage capacity and long life. The main thing of FESS is any emergency situation, it can response rapidly to control the power in large network. Any large power system, generally smoothing of rapid change of wind output power in short time is makeup by energy storage system. On the other hand, the slow change of wind output power during long term consists of other interconnected power plants for frequency control.

Alsokhiry and Lo, (2013) study the feasibility of DG based solar and wind power system to produce ancillary service in a medium level of micro grid, called frequency response ancillary service. To do this ancillary service they have proposed a battery storages system (FESS). Also, they have used a generic model of IEEE 13 buses distributed generation as a test network. Here the total generation from traditional power station is showing 50% of total generated power and the other 50% of power produce from renewable energy sources. To observe the impact of frequency response on DGs, they assumed two cases, before injecting the DGs based renewable sources on traditional generation system and after injecting the DGs based on renewable sources on traditional generation system. The results show that the load demand at all the buses is increased or decreased by 30 % to show the response of frequency in the system.

## **1.6 Micro grid**

A microgrid is a localized grouping of generating the power, storage of energy and loads. A microgrid is usually interconnected to the traditional centralized grid. The point of common coupling with the traditional distribution network can be disconnected. The microgrid can operate autonomously. The generation and the loads in a microgrid are usually connected to a

low voltage network defined as micro-network. Micro-generation network resources may include solar, wind, fuel cells or other energy sources. Multiple sources of generation and the possibility of isolating the microgrid provide a highly reliable electric power. The heat produced from generation sources such as microturbines could be used for heating. Marei and Mohamed (2012) proposed control strategies for the adaptation of decentralized generation units with autonomous micro-networks. They presented a model of a control system that coordinates the frequency and voltage of an inverter-based DG and an energy storage system. The interface of the DG not only used to control the flow of active power but to ensure the voltage regulation of the micro-network. Finally, the developed interface, DG and storage system ensured voltage regulation and frequency control for various disturbances.

## **CHAPTER 2**

### **CONNECTION OF WIND POWER IN THE POWER NETWORK**

#### **2.1 Introduction**

##### **2.1.1 Overview**

Nowadays, wind energy is the most common renewable energy in the world. Its large-scale integration poses new constraints to the electrical power systems compared to the conventional energy sources, whose behavior is well controlled. In order to meet the challenge of coordination, wind power generation with the other electrical systems, many countries have imposed new requirements in their network regulations for connection and operation of wind turbines. The aim of these regulations is to setup technical rules for connection of power transmission, distribution and operation of the electric system to ensure an adequate level of security and reliability.

The main constraint of integration of wind farms in power systems is related to the nature of wind variability. The electric power produced by wind turbines always fluctuates. It varies with the variation of the wind speed. This can be considered as a disturbance of electrical power injected into the system and can have a bad impact on the stability of the system. Furthermore, the wind can change the network structure. This disturbance changes the dynamic behavior of the machines. Hence, it is needed to develop new requirements for connection and operation of wind farms in order to keep maximum wind turbines connected to the grid. The power system must be robust to various disturbances and must have the ability to contribute to the stability and security of the network.

##### **2.1.2 Principle of wind generation**

Wind energy is produced by the force of wind that exerts on the blades of a wind turbine and turning them between 10 and 20 rpm. These blades are connected to a generator that converts mechanical energy into electrical energy. The amount of energy generated by a wind turbine

mainly depends on wind velocity; the area swept by the air density and turbine blades. Wind turbines require a minimum amount of wind, usually 12 to 14 km/h, to start rotating and generate electricity. With winds of 50 to 60 km/h, the wind turbine produces full power. Wind speed beyond 90 km/h, wind production is interrupted to generate power from wind turbine. The energy of wind has several advantages including cleanliness because it is not fossil type, also produced by the wind and renewable source. Nevertheless, we can neither store the wind nor control its speed.

In Germany, 959 new wind turbines were installed in 2012 (Fraunhofer Institute for Wind Energy and Energy System Technology, 2012); they represent a total capacity of 2332 MW. By comparison, all wind turbines installed in Germany represents a total capacity of 31,156 MW. Figure 2.1 shows the various wind farms in Quebec in 2015: those who are in service produce 2949.7 MW of electricity; early power for farms under construction is 247.3 MW and a projected park is 513.8 MW. In Quebec, two factors favor the development of wind energy including the presence of large reservoirs that instantly offset the intermittency of wind energy input and good territorial coverage of the transmission system, which allows integration of wind generation, including from remote areas (Figure 2.1).



Figure 2.1 Different operating wind farms in Quebec  
Adapted from Hydro-Québec (2015)

Wind power always variable and only partially predictable, it needs to associate with a programmable basic source of energy. Large wind power producing countries like Germany uses thermal power plants in addition of wind power. In Quebec, it is hydropower, renewable energy, which supports along with the wind power. The great challenge for Hydro-Québec is to increase the production of wind power and integrate the power network while increasing the level of penetration of distributed wind generators. Therefore, problems related to the stability of the electrical network are to face by the operators in terms of safety, reliability and network performance since the wind fluctuates depending on local weather conditions. Wind generation is highly variable while being partially predictable.

## **2.2 Conversion system of wind energy**

The main components of a regular wind energy conversion system is a turbine, a three-phase generator, an interconnect device and a control system, as shown in Figure 2.2. The turbine can be at a constant speed or variable speed. The variable speed turbines can produce 8-15% energy more than the turbines at a constant speed, but they must be equipped with an electronic power converter to produce a fixed voltage and frequency for the loads. Most turbine manufacturers are now installing a gearbox between the low-speed turbine rotor and the three-phase high-speed generator. The direct-drive configuration, where, the rotor of the turbine is directly coupled to the generator, is extremely reliable, requires minimal maintenance and often reduces costs. The turbines will be equipped with synchronous generators, synchronous permanent magnet generators or asynchronous generators, including models of squirrel cage and wound rotor. Permanent magnet generators and permanent squirrel cage induction generators are often used for small and medium turbines because of their reliability and lower cost. Various high-power turbines are currently equipped with induction generators or synchronous generators with permanent magnets.

Most modern turbines are equipped with pulse width modulation (PWM) to produce quality power at fixed voltage and frequency. Both converters were used for wind turbines. Some adjustment of the high-power turbine is ensured by a double PWM converter, which provides

power transmission in both directions between the generator of the turbine and the electric utilities. (Chang, 2002).

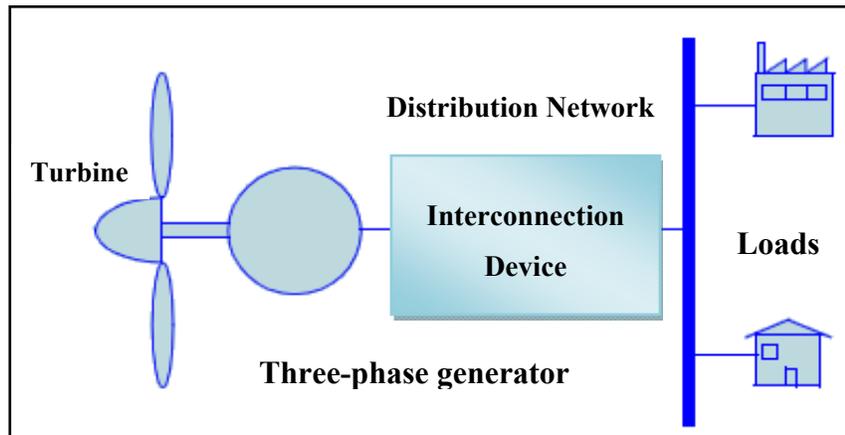


Figure 2.2 The conversion system of wind energy  
Adapted from Chang (2002)

## 2.3 Technical operation of the wind Turbine

### 2.3.1 Types of wind turbines

There are mainly four types of wind generator:

- 1 Squirrel cage asynchronous machine at variable speed;
- 2 Wind turbines induction generator (WTIG) at variable speed;
- 3 Doubly-fed induction generator (DFIG) power at variable speed;
- 4 Permanent magnet synchronous generator (PMSG) at variable speed

#### 2.3.1.1 The variable speed squirrel cage wind turbines

Variable speed wind turbines (Figure 2.3) are based on an asynchronous squirrel-cage machine which directly connected to the power grid. This machine is driven by a gearbox and its speed is kept constant by a pitch control system. The machine can operate at its synchronous speed.

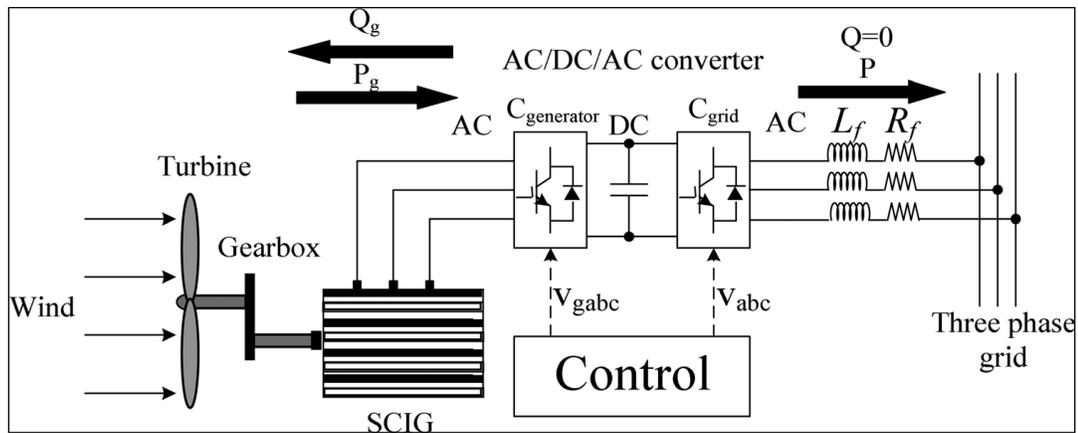


Figure 2.3 Wind turbine with a squirrel-cage induction generator  
Adapted from Boulouiha et al. (2012)

The theoretical setting of wind speed control is shown in Figure 2.3 for a wind turbine. The relatively slow dynamics of pitch control and rapid changes in wind speed leads this type of wind turbine to follow the approximately characteristic setting that illustrated by the deferred items, measured as a real wind turbine.

### 2.3.1.2 Wind turbine induction generator (WTIG)

WTIG is a wound rotor type generator. The stator winding is directly connected to the network. Here the rotor is driven by the wind turbine. The power generated by the turbine is converted into electrical energy using the induction generator and transmitted to the network by a stator winding. To bring the output power of the generator within nominal value at high wind speeds, the pitch angle has to be controlled. To produce power, the speed of the induction generator should be greater than the synchronous speed. However, the rate of change of speed is typically so small such that the WTIG may be considered a wind turbine as a fixed speed. The reactive power absorbed by the induction generator is powered by the electrical network or by devices such as capacitor banks, SVC, STATCOM or synchronous condensers. Figure 2.4 shows the general structure of a wind turbine induction generator.



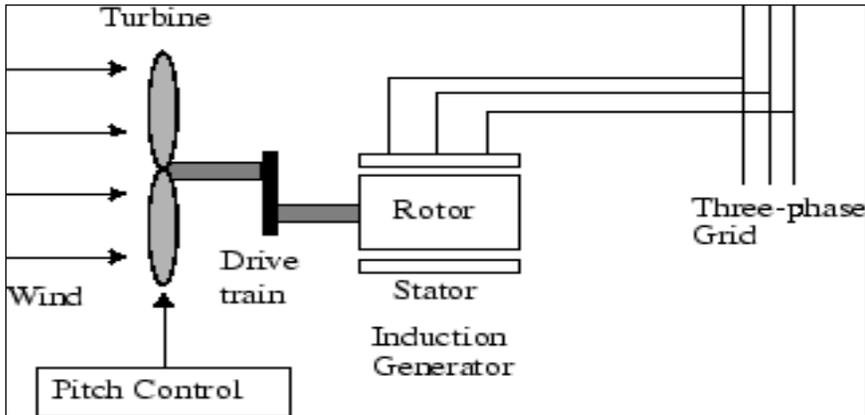


Figure 2.4 General structure of a wind turbine induction generator  
Adapted from Matlab (2017)

A proportional integral (PI) controller is used in order to control the pitch angle  $\beta$  to limit the electric power to the nominal mechanical power. The pitch angle is maintained constant at zero degree when the rated electric power is less than the nominal value. When it becomes higher than the nominal value, the PI controller increases the angle  $\beta$  to bring the measured power back to its nominal value. Speed control is achieved by changing the rotor resistance.

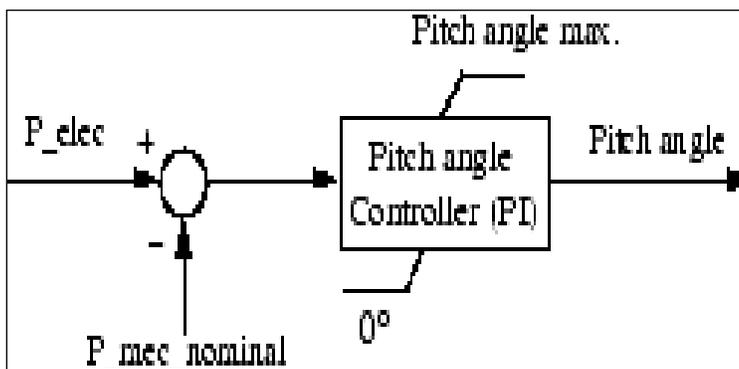


Figure 2.5 Control systems for wind turbine induction generator  
Adapted from Matlab (2017)

### 2.3.1.3 Doubly-fed induction generator (DFIG)

The doubly fed induction generator (DFIG) (Figure 2.6) is generally a type of wound rotor induction generator (WRIG) presented in Figure 2.6. The AC/DC/AC converter is divided into two parts: the rotor side converter ( $C_{rotor}$ ) and another is grid side converter ( $C_{grid}$ ). In IGBT,  $C_{rotor}$  and  $C_{grid}$  are voltage source that is used to generate an AC voltage from a DC voltage source. A capacitor bank is connected to the DC side to act as a DC voltage source. The inductance  $L$  is used to connect  $C_{grid}$  to the power grid. The windings of the three-phase rotor are connected to the  $C_{rotor}$  by using rings and brushes. Three-phase stator windings are connected directly to the grid. The power from the turbine is converted into electrical energy by using induction generator and it dispatched to the network by the rotor and stator windings. The control system produces pitch angle control and the control signals of the voltage  $V_r$  and  $V_{gc}$  for the  $C_{rotor}$  and  $C_{grid}$  respectively in order to control the power of wind turbine, the DC voltage, and the reactive power. Matlab (2017).

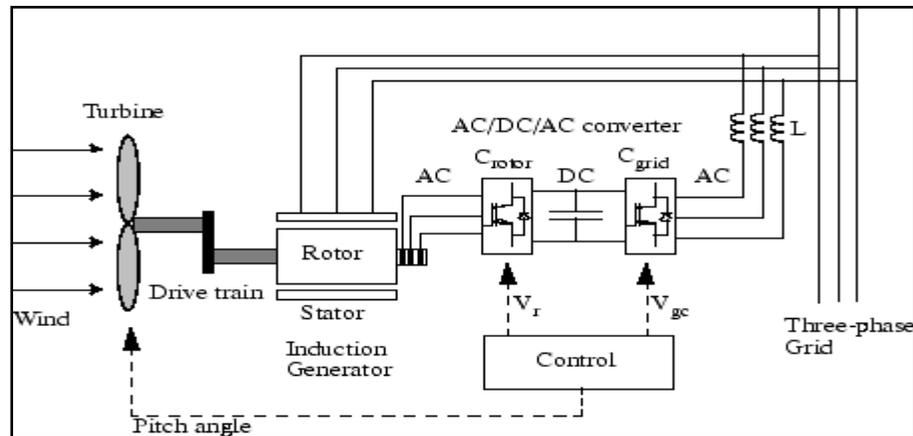


Figure 2.6 Operating Principle of the Doubly-Fed Induction Generator  
Adapted from Matlab (2017)

Figure 2.7 shows the operating mode and the power flow between the power grid and the wind turbine through the generator and the converter. In super-synchronous speed operation, rotor power, when  $P_r$  is positive; the power is transmitted from the rotor to the network

through the converter. The Mechanical rotational speed is higher than the synchronous speed

( $\omega_r > \omega_s$  and  $s < 0$ ). With  $s$ : slip of the ASM:  $s = \frac{\omega_s - \omega_r}{\omega_s}$

In super-synchronous speed operation, when  $P_r$  is negative; power is transmitted from the network to the rotor through the converter. The mechanical speed is comparably less than the synchronous speed ( $\omega_r < \omega_s$  and  $s > 0$ ). The converters can provide up to 25% of the rated power of the DFIG.

In both cases the stator power,  $P_s$  supplied to the network and the absolute value of  $s$  is less than 1.

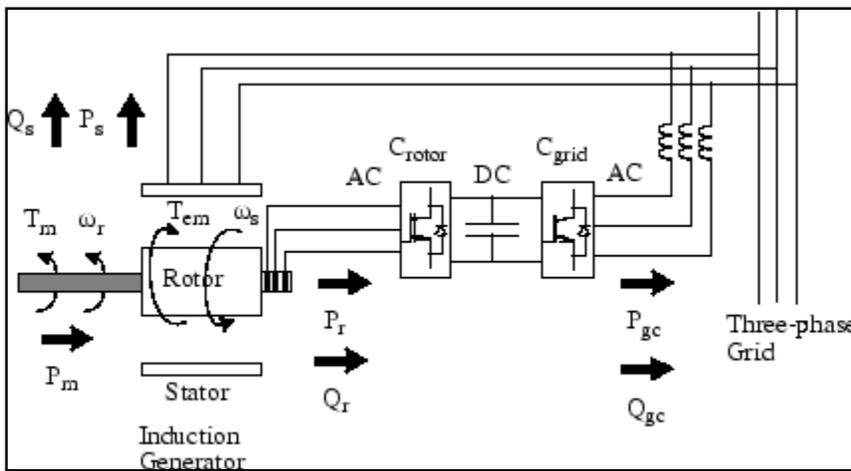


Figure 2.7 Power Flow of DFIG  
Adapted from Matlab (2017)

Mechanical power to the stator and the output electric power are expressed as follows:

$$\begin{aligned}
 P_m &= T_m \omega_r \\
 P_s &= T_{em} \omega_s
 \end{aligned}
 \tag{2.1}$$

The dynamics equation of the machine is:

$$J \frac{d\omega_r}{dt} = T_m - T_{em} \quad (2.2)$$

At the equilibrium:

$$T_m = T_{em} \text{ and } P_m = P_s + P_r \quad (2.3)$$

The power is controlled to follow a preset adjustment curve. An example is shown in Figure 2.8

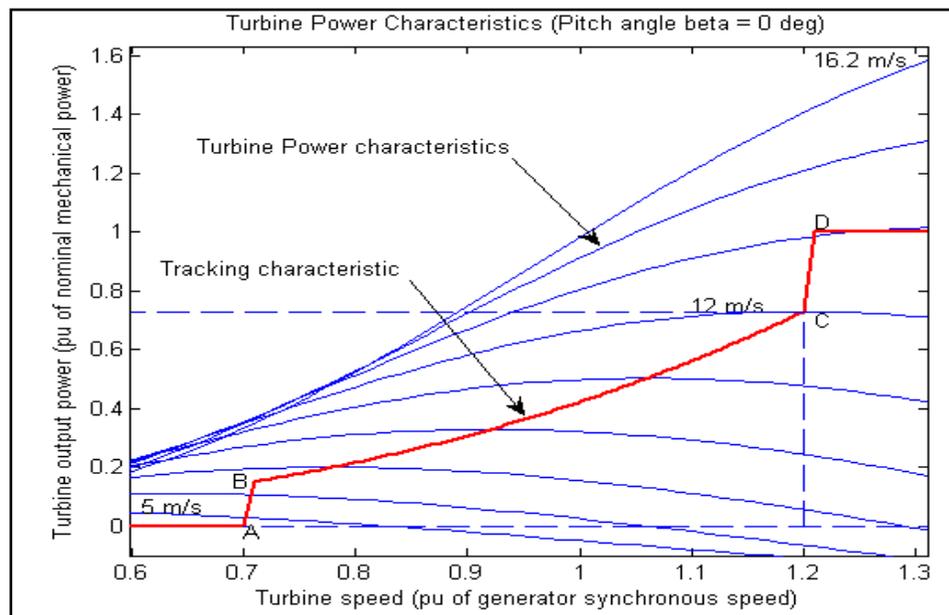


Figure 2.8 Adjusting power characteristic for a DFIG  
Adapted from Matlab (2017)

The actual speed  $\omega_r$  of the turbine is measured and the corresponding mechanical power is used as the reference power for the power control loop in this curve.

Where:

$P_m$	Mechanical power generated by the wind turbine and transmitted to the rotor
$P_s$	Stator electrical power output
$P_r$	Rotor electrical power output
$P_{gc}$	$C_{grid}$ electrical power output
$Q_s$	Stator reactive power output
$Q_r$	Rotor reactive power output
$Q_{gc}$	$C_{grid}$ reactive power output
$T_m$	Mechanical torque applied to rotor
$T_{em}$	Electromagnetic torque applied to the rotor by the generator
$\omega_r$	Rotational speed of the rotor
$\omega_s$	Rotational speed of the magnetic flux in the air-gap of the generator, this speed is named synchronous speed. It is proportional to the frequency of the grid voltage and to the number of generator poles.
$J$	Combined rotor and wind turbine inertia coefficient

There are five stages of operation of a DFIG wind turbine are defined by the control curve (Figure 2.8):

- Between 0 m/s velocity and A. The starting phase of the machine: electrical generation begins when the mechanical speed reaches about 70% of the synchronous speed of the generator but the electric power remains low;
- Between A and B the line is straight, the velocity of point B should be higher than the velocity of point A;
- Between B and C: The extraction phase of the maximum power, mechanical speed varies and can reach a value close to the rated speed and the electric power increases rapidly. The setting of blades angle  $\beta$  remains at its minimum value in order to obtain a maximum power coefficient. The maximum power is then obtained for each value of the mechanical speed and for the average wind speeds;

- Between C and D: The phase almost reach in constant with mechanical speed: the angle  $\beta$  varies in order to obtain a maximum electrical power for different values of wind (pitch control) and the electric power increases very quickly up to its nominal value;
- Beyond the point D: The phase remains at constant power. As wind speed increases, the pitch angle of blades becomes necessary to keep the nominal electric power constant.

The control of power generator can be gained by performing on the orientation of the blades, as well as controlling the torque of the asynchronous generator by means of the converter connected to the rotor.

#### **2.3.1.4 Permanent magnet synchronous generator (PMSG) at variable speed**

A permanent magnet synchronous generator (PMSG) excitation field consists of a permanent magnet in place of a coil. The term synchronous means that the magnetic field and the rotor of machine rotate with at speed. The magnetic field produces from the shaft which is mounted mechanism of permanent magnet.

Figure 2.9 shows, the general block diagram of PMSG with variable speed. This variable speed PMSG has large range of speed capacity and can provide more energy compared with the fixed-speed types PMSG. To protect from stronger winds, it is very important to have a power control system in order to avoid damaging of wind turbine. Basically, there are three techniques for securing modern wind turbines (Danish Wind Industry Association, 2003).

- Pitch controlled wind turbines;
- Passive stall controlled wind turbines;
- Active stall controlled wind turbines.

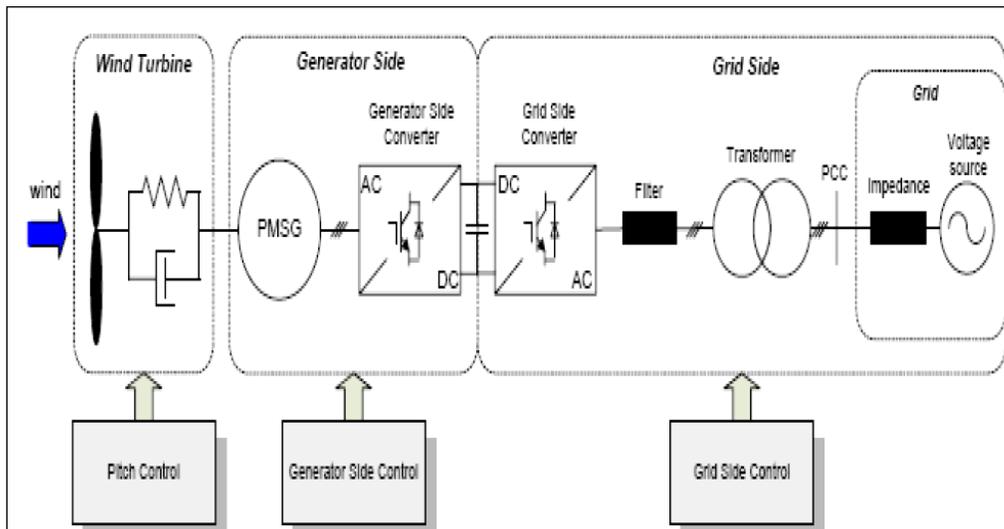


Figure 2.9 General block diagram of PMSG wind turbine  
Adapted from Kumar et al. (2013)

## 2.4 Connection of wind power to the grid

### 2.4.1 Network stability

The stability of the network is characterized by the fluctuations of power flow in the network and it's measured by the variations over time of voltages and frequency. It must be distinguished:

- **Steady state stability:** the network has a stable behavior, such as, subject to small disturbance, it returns to its initial operating point with possible damped oscillations until it returns to the balance condition;
- **Transient stability:** when moving from one steady state to another state, due to a disturbance, this change in equilibrium is accompanied by a damped oscillatory variable considered acceptable with respect to predetermined ranges of  $\Delta U$  (voltage),  $\Delta f$  (frequency) and  $\Delta t$  (time);

- Transient instability is observed when a major disturbance occurs and the damped oscillation is divergent. It causes a loss of power or a new unacceptable stable condition;
- Dynamic stability: the network is able to avoid any divergent oscillatory and return to an acceptable stable condition. Consider the main critical scenarios such as short circuit, loss of mechanical energy, loss of power source, load variation, process constraints. Can predict the behavior of the network disturbance. Specify the measurement of operation, such as type of protection, control relay, load shedding and configurations to avoid undesirable operating modes.

Analysis of the stability of electric networks is generally made by the power flow methods considering the parameters of the network buses under study. Table 1 shows the parameters for each type of bus.

With:

$V_i$  : voltage at the bus  $i$ ;

$P_i$  : active power at the bus  $i$ ;

$Q_i$  : reactive power at the bus  $i$ ;

$\delta_i$  : the phase angle between voltages at the bus  $i$ .

Table 2.1 Parameters of the buses for an electrical network

<b>Bus classification</b>	<b>Known parameters</b>	<b>Unknown parameters</b>
Balance Bus (Swing Bus)	$ V_1 ; \delta_1$	$P_1; Q_1$
Generation Bus (PV Bus)	$P_2; V_2$	$\delta_2; Q_2$
Load Bus (PQ Bus)	$P_3; Q_3$	$ V_3 ; \delta_3$

### **2.4.2 The network frequency**

In an electrical system, it is important to maintain the frequency around its nominal value (60 Hz in north America). The maintenance of this value is not only necessary for the better functioning of the loads, but it is also required for balance between the active powers produced and those consumed. Indeed, the frequency decreases if the consumption is higher than the production and increases when the consumption is lower than the production.

In the first installations of wind farms, when the frequency decreased, wind turbines were disconnected from the grid, which made it difficult to restore the system. In the recent network regulation, the wind turbines remain connected to the system and can operate in a frequency range close to the nominal value for a certain period which varies with the deviation. Frequency requirements vary by country. For example, in Québec, Hydro-Québec allocates to wind energy producers  $P_{nom} = 10\text{MW}$  at a rated a frequency of 60 Hz, which varies by  $\pm 1\%$  (from 59.5 Hz to 60.5 Hz) for a period maximum of 10 seconds for medium voltage networks (Hydro-Québec TransÉnergie).

### **2.4.3 Case study: connecting a wind turbine to the power grid without storage system**

In this case study, we will observe the frequency behavior without storage system in the network and according to this, we will try to improve the frequency quality response using storage system and controllers (PID and Fuzzy) in the next chapter. For this study, a model has been taken which is developed for the High Penetration, No Storage of Wind-Diesel system (HPNSWD). This strategy was promoted by Hydro-Quebec for a remote area to minimize the cost of power electricity. The maximum power from wind in the network depends on attainable wind resource and cost of fuel. Mott and Saulnier (2014) show the first commercial application of HPNSWD technology accepted in “1999 by Northern Power Systems (Vermont, USA) on St. Paul Island, Alaska”. For this case study a 480 V, 275 kVA wind turbine based on induction generator, a 480 V, 300 kVA synchronous generator, a

variable secondary load (0 to 446.25 kW) and a 50 kW consumer load is used. Matlab (2015).

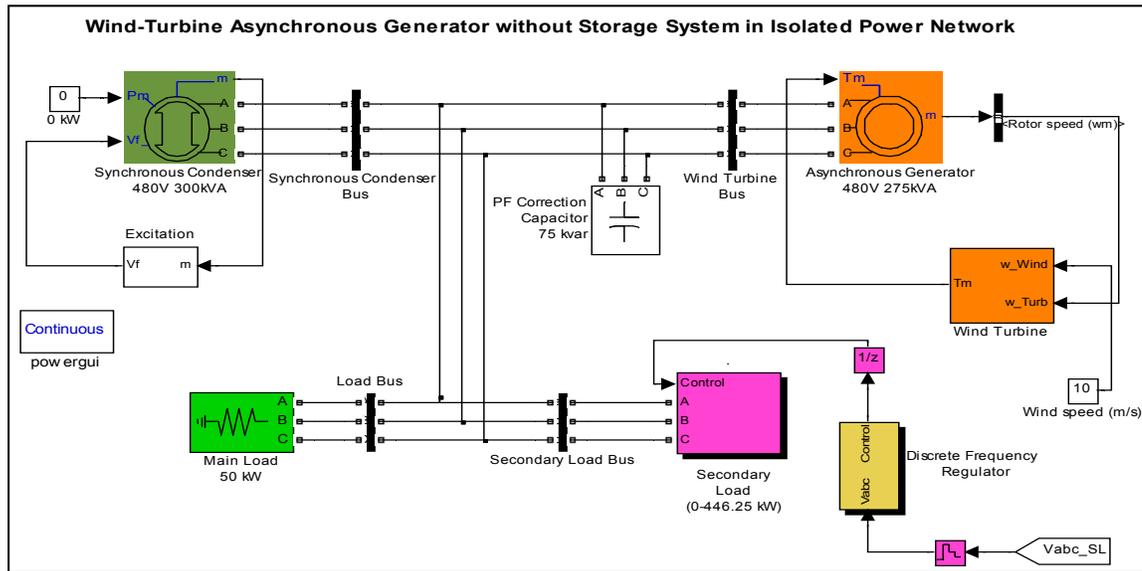


Figure 2.10 A wind turbine asynchronous generator power network

**a. Matlab Simulation**

Table 2.2 Wind turbine generation systems parameters (Gagnon et al. 2002)

Network	Synchronous Generator : 480 V, 300 kVA
Turbine	480 V, 275 kVA induction generator Pnom= 200 kW Wind speed Vwind_nom= 10 m/s Pitch angle = 0 deg, P=Pnom and V=Vnom
Buses	1. Synchronous Condenser Bus (SC) 2. Wind Turbine Bus (WT) 3. Secondary/Dump Load Bus (SL) 4. Main Load Bus (Load)
Load	Main Load 100 kW Extra Load 50 kW + 30 kW + 50 kW Secondary/Dump Load vary 0 to 446.25 kW by step of 1.75 kW

The induction and diesel based synchronous generator both are required to feed the load at lower wind speeds. When the value of wind power oversteps the load demand, the diesel generator will then shut down. In wind mode, grid voltage remains in nominal level by controlling the excitation system of synchronous generator and used it as a synchronous condenser. To control the system frequency, a secondary load is used. This secondary load regulates the frequency by absorbing wind power to maintain the exceeding of consumer load demand.

The secondary load is made by three-phase resistors, connected in series with thyristor switches. The nominal power of each switch maintains a binary development to vary load from 0 to 446.25 kW with steps of 1.75kW. Gate turn-off thyristor are simulated with ideal switches. Here frequency is controlled by discrete frequency regulator. To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). The frequency error is then integrated to obtain a phase error. The phase error is applied to the Proportional-Derivative (PD) controller to generate an output signal to get the required secondary load power as shown figure 2.11.

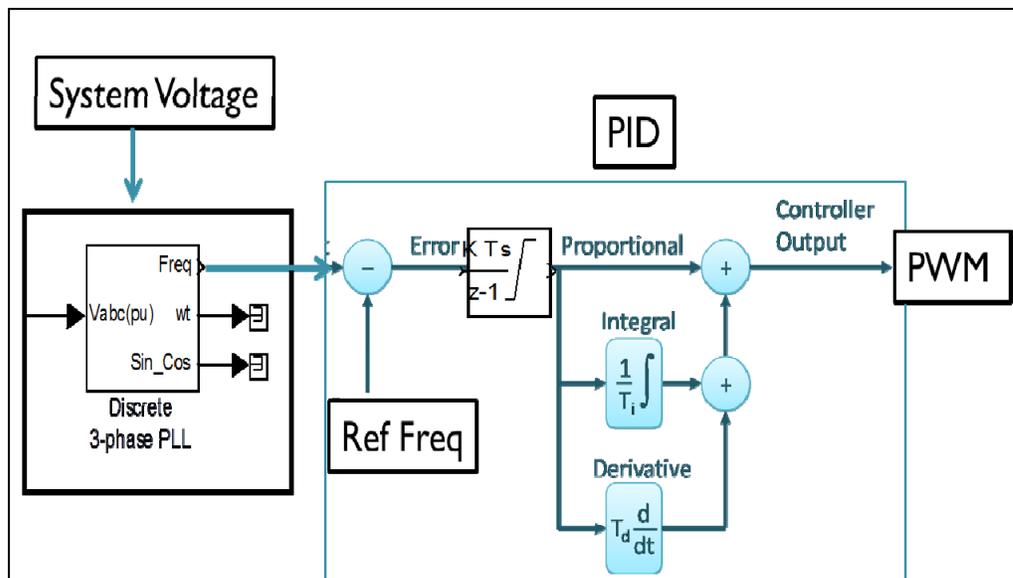


Figure 2.11 Block diagram of frequency control using PID controller

This output signal is then converted to a digital 8-bit signal (shown in figure 2.12). In order to mitigate the voltage disturbances, voltage is switched at zero value.

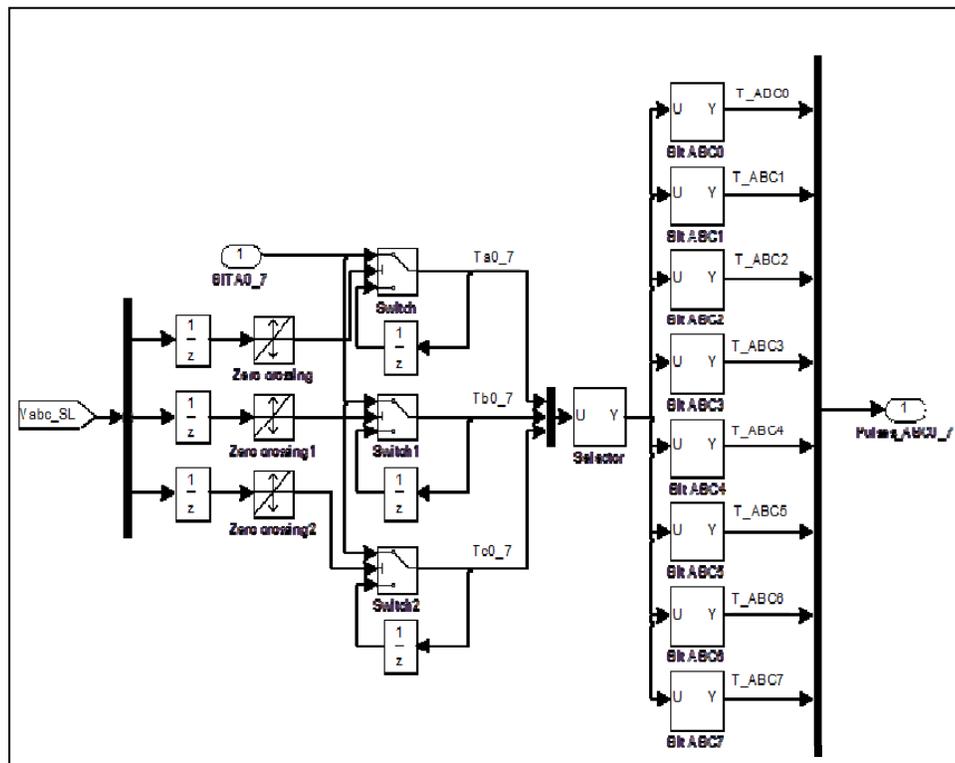


Figure 2.12 8-bit three three-phase digital signal

### b. Matlab Simulation

Here, (10 m/s) wind speed is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 2.13 (a). The secondary load absorbs 150 kW to regulate a 60 Hz frequency shown in figure 2.13 (b). Figure 2.13 (c) shows, the consumer (main) load is 50 kW.

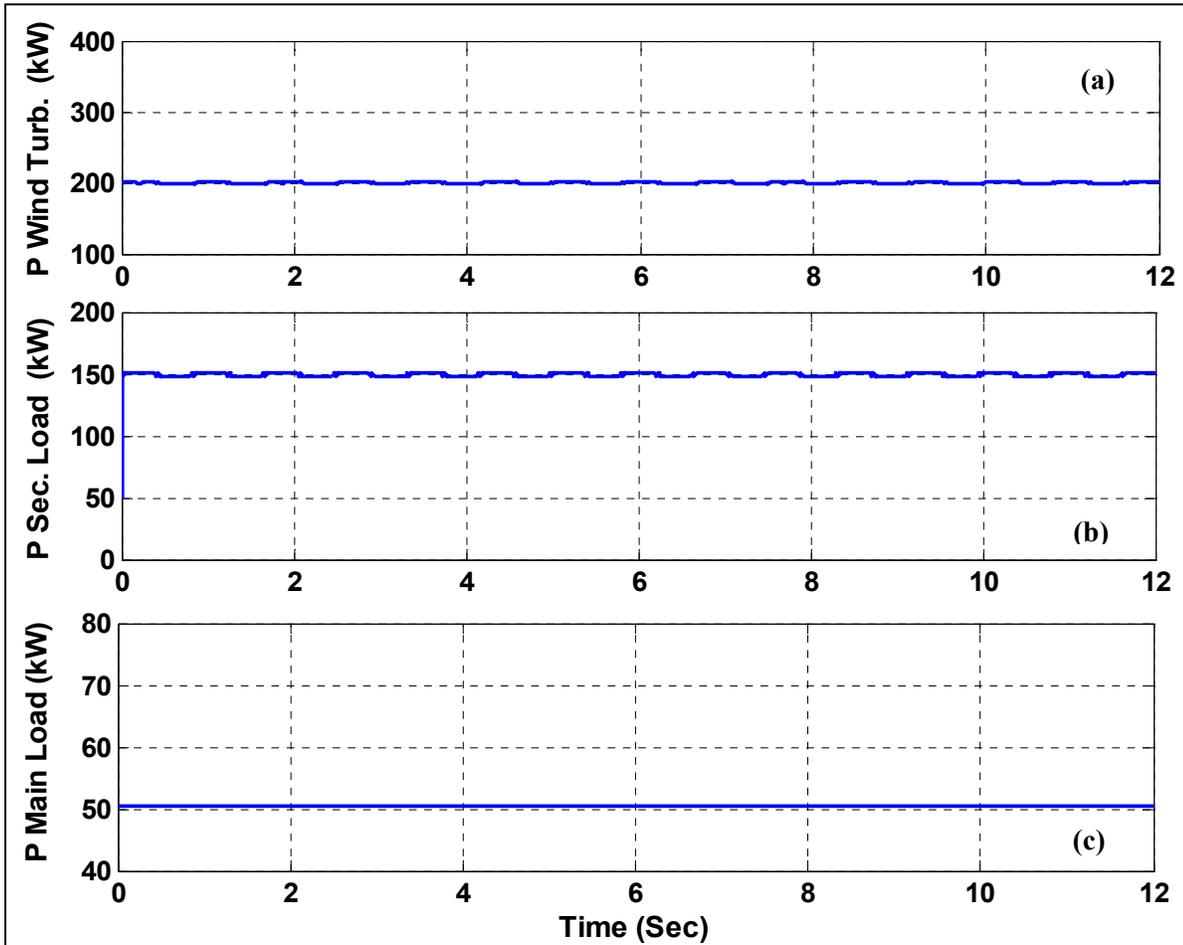


Figure 2.13 (a) Power from wind turbine, (b) Power absorbed by Secondary load and (c) Power absorbed by the main load

Figure 2.14 (b) shows, the speed of the asynchronous machine which is above 1.01 (pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when turbine runs at 10 m/s wind speed. Figure 2.14 (a) shows, after 12s simulation the frequency remains always 60 Hz without any disturbance. The discrete frequency regulator responds to mitigate the power which absorbed by the secondary load to fetch back the frequency to 60 Hz. Voltage remains at 1 pu. To see more details we took data from (6 - 6.5)s shown in figure 2.15.

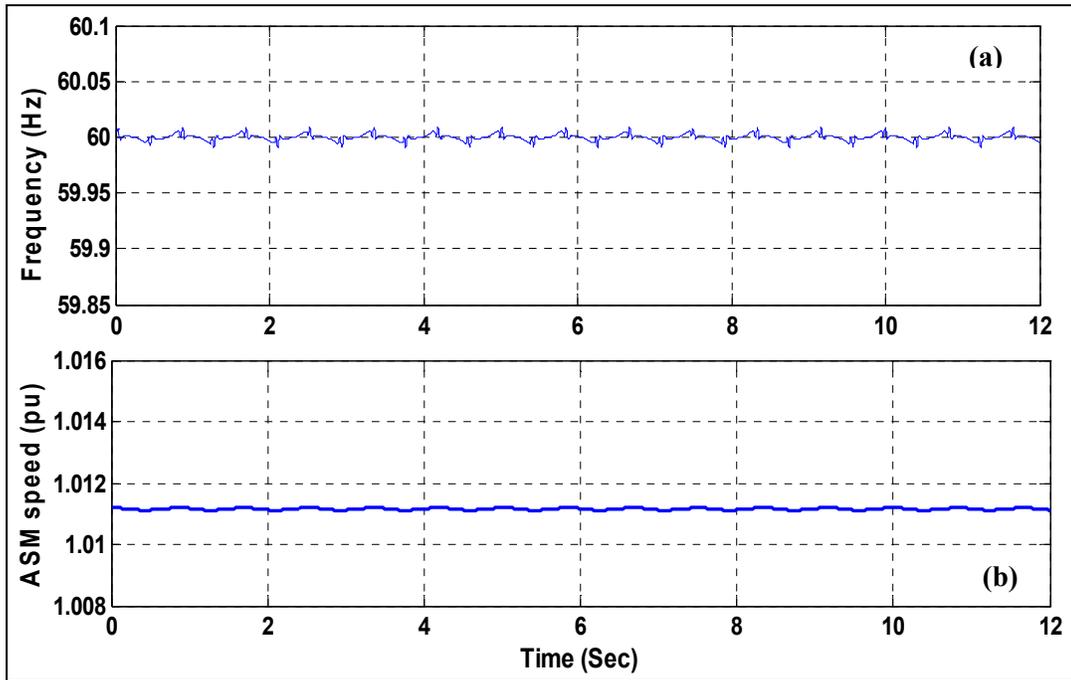


Figure 2.14 (a) Frequency at load bus, (b) Speed generated by asynchronous generator

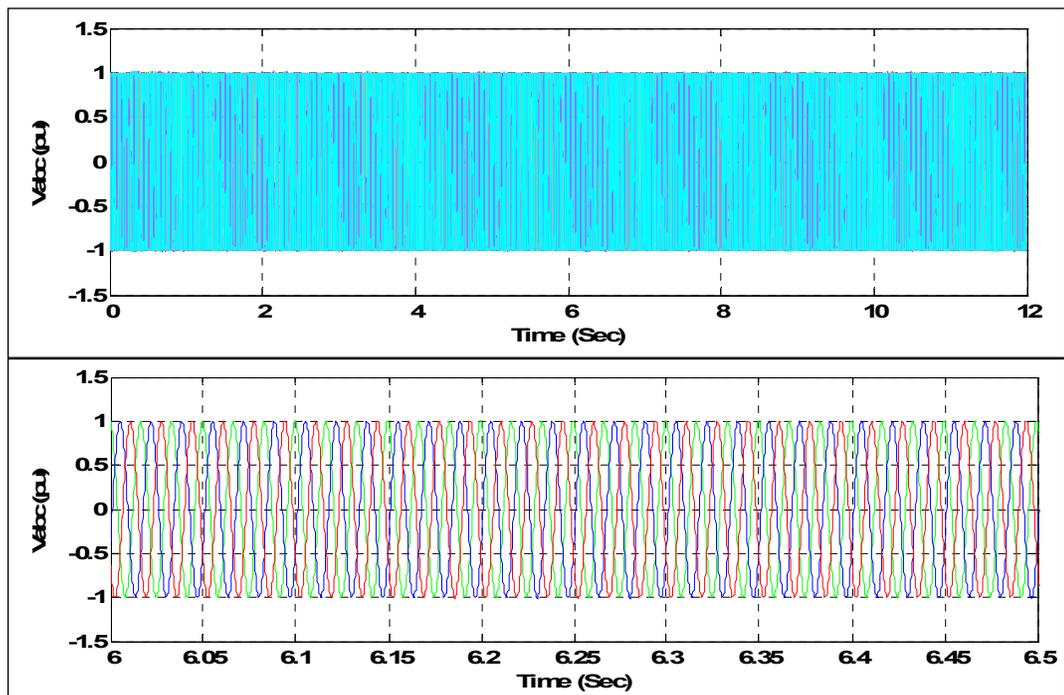


Figure 2.15 Voltage at load bus



## CHAPTER 3

### FLUCTUATION BEHAVIOR OF FREQUENCY FOR A HYBRID / WIND-BASED POWER BATTERY STORAGE SYSTEM USING DIFFERENT CONTROLLERS

#### 3.4 Introduction

The wind-based DG is a RES. The variations in power caused from wind fluctuations constitute the main disturbance of the wind conversion chain. Volumes and wind production periods do not match the volumes and periods of electricity consumption. The Wind-Diesel hybrid power system (WDHS) is an autonomous power generation system using wind turbines with a diesel generator for maximum contribution by the intermittent renewable resource to the total power generated while providing continuous electrical power quality. The main objective of these isolated electrical systems is to reduce fuel consumption and thereby reduce the cost of system operation and environmental impact. Generally, this type of system is considered a high penetration from DG so that diesel based system can operate as a part-time. The exploitation of energy resources from the wind is priority operation. Figure 3.1 shows the WDHS medium penetration and the elements that constitute the system with the diesel generator, wind and consumer load. Other components are shown in Figure 3.1, in particular, secondary load also called Dump load (DL) and the Battery basic Energy Storage System BESS.

In this chapter, we have presented two methods to control the frequency of a hybrid system (PID & Fuzzy Logic) that works in wind mode only (WO) having as a renewable energy source with a fixed speed wind turbine, battery-based energy storage system, DL loads and consumer loads. To see the frequency stability, we have used some extra load in the network.

### **3.5 The system of WDHS**

This is a specific model of the large penetration with storage system, combined with wind-diesel (Gagnon et al. 2002). This technology was promoted by Hydro-Quebec for a remote northern area to minimize the cost of power electricity. The maximum power from wind turbine in the network depends on availability of the wind.

#### **3.5.1 The operation modes of WDHS system**

Figure 3.1 shows the high penetration system that admits three operating modes: Diesel only (DO), Wind-Diesel (WD) and Wind only (WO) (Sebastián and Quesada, 2015).

In DO mode, the wind speed is low and the diesel generator is needed to supply the load. To satisfy the demand by the load consumers (in this mode wind turbines are off), the diesel generator provides active and reactive power. Regulators that control the diesel generator ensure the stability of voltage and frequency of the system.

In WD mode, the wind turbine generators also provide the active power and reactive power consumed. The same control in Diesel mode only is responsible for controlling the frequency and voltage. As the active power received by the DG can be negative, DL must be added to empty the necessary power to prevent reverse power in diesel generators. A battery energy storage system (BESS) can be used to reduce reserve requirements and provide load to the diesel generator to improve their performance.

In WO mode is possible only if the power generated by the turbine is greater than the power required by the load. During this mode, the diesel generator is switched off, and wind turbines provide active power. Therefore, subsidiary devices are needed to control the frequency and voltage. The voltage is regulated by the balance of the reactive power, which is automatic that means; the reactive power supplied by the device is equal to the absorbed reactive power.

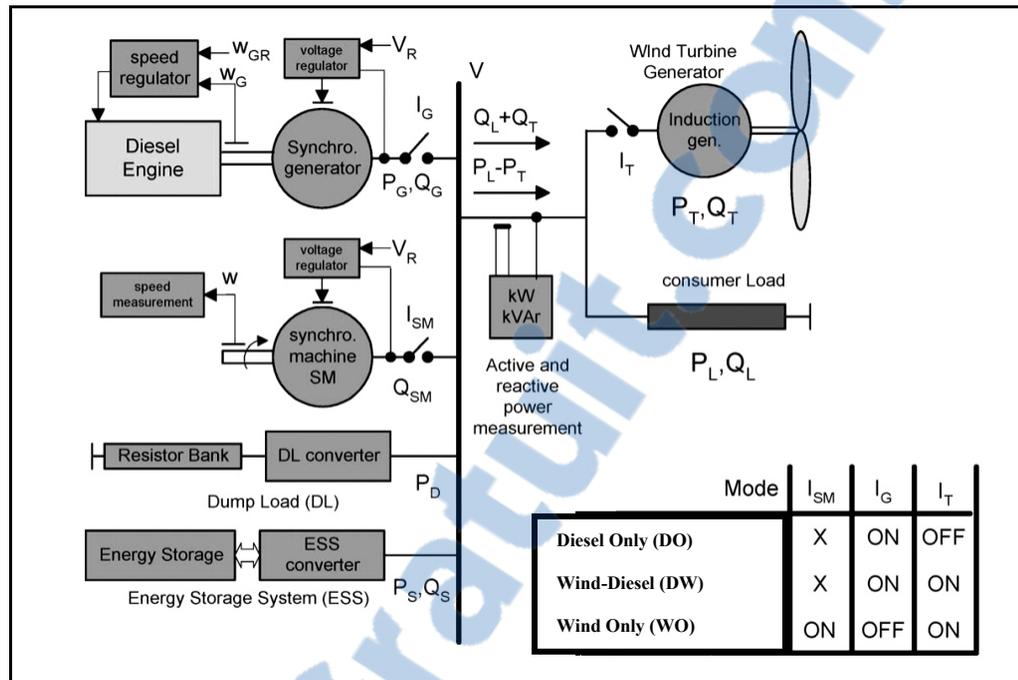


Figure 3.1 Wind generation system diesels with energy storage  
Adapted from (Sebastián and Quesada, 2015)

### 3.5.2 System Combination of WDHS

The system has been shown in Figure 3.1, works for the rest of this thesis in Wind mode Only (WO). Therefore,  $I_G = 0$  and the circuit that represent the diesel engine and its control system is disconnected.

#### 3.5.2.1 The synchronous machine

The synchronous machine (SM) of rated power 300 kVA generates the voltage signal and its regulator control the voltage when the diesel engine is stopped. The synchronous machine of the voltage regulator will control the excitation of the machine so that it provides the reactive power needed to reach a voltage  $V$  at the common bus, where equilibrium reaches the nominal values. Its main role is to provide reactive power to wind DG.

### 3.5.2.2 The wind turbine

The DG block is an asynchronous ASM machine with 2s inertia and 480 kVA power. This block uses the given wind power  $P_{wind}$  and the speed of rotation of the shaft to calculate the mechanical torque that controls the ASM. The DG is considered to be a fixed speed energy generator. Therefore it does not allow controlling its pitch angle. The wind power is an input data  $P_{wind}$  (kW) versus time (s).

### 3.5.2.3 Secondary load system

The Secondary load variable (DL) block consists of eight three-phase resistors connected in series with the GTO switches. The nominal value of power of each three-phase resistors follows a binary progression of 8 bit so that the power consumed by DL can be changed from 0 to 446.25 kW by steps of 1.75kW. GTO thyristors are operated by ideal switches. This DL is used to regulate the frequency of the network by absorbing wind power that exceeds load demand.

### 3.5.2.4 The battery based energy storage system

Figure 3.2 shows, a battery based energy storage system (BESS). It is composed of a battery and a power converter: A bidirectional IGBT transistor bridge of power  $P_{S-NAME} = 150kW$  controlled in current mode. The IGBT performs DC/AC conversion to the battery interface with the isolated network. The battery is high capacity Ni-MH power, rated voltage is 240V, 390Ah capacity. The BESS control allows charging and discharging the battery according to the power requirement for the isolated network. Figure 3.2 shows the model of Current Controlled Inverter (CCI) systems. It is interconnected by an LC filter to reduce current fluctuations. The voltage  $V_{L-L}$  is equal to 120V. The connection of the BESS with the isolated network is ensured through a step-up transformer rated 120V / 480V, 150kVA.

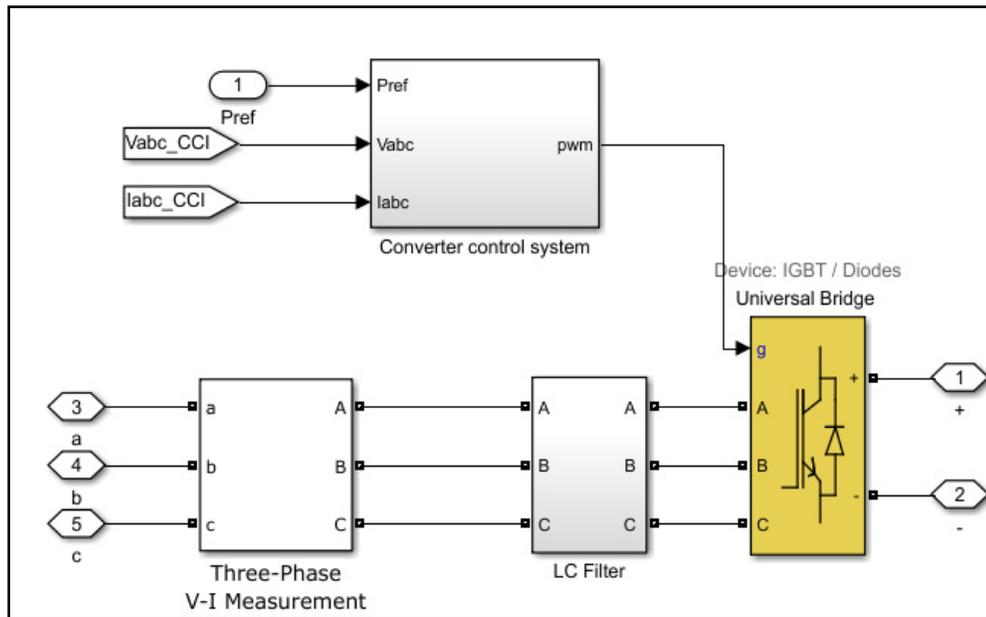


Figure 3.2 Simulink models of Power converter and BESS block

### 3.6 The network controls system of WDHS

To ensure its operation, the WDHS network requires an efficient control system to ensure the optimum operating mode with dynamic stability of the voltages and frequency of the network. Two control systems have to be set up: the first is to ensure network frequency stability while the second is to allow control of the energy requirement via the battery-based storage system (BESS). The principle of instantaneous frequency control through the power flow in the WDHS network which is used in this application is described by the logic diagram in the figure 3.3.



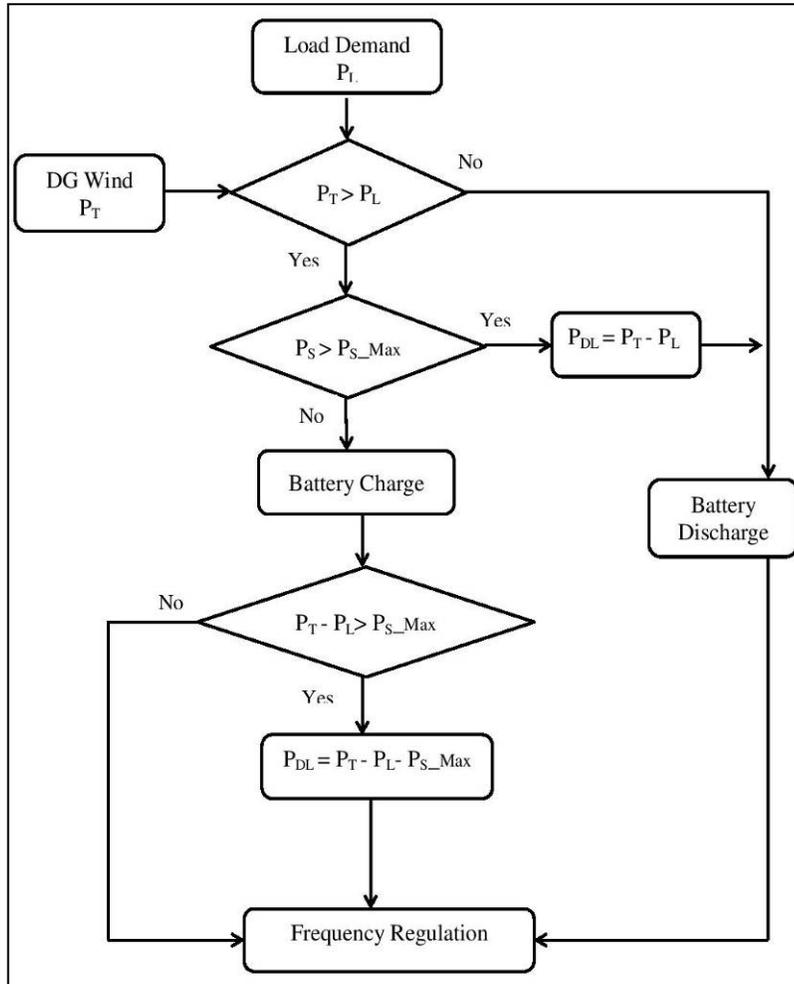


Figure 3.3 Power sharing and the battery charging and discharging conditions of WDHS system Adapted from Oueslati (2014)

### 3.6.1 The frequency control system of WDHS

The frequency is controlled by maintaining an instantaneous balance of the active power consumed and produced. To achieve this balance of active power, the BESS energy storage system and DL store the active power (Sebastián and Quesada, 2015).

The BESS stores the excess power generated by wind: In this case,  $P_S > 0$  and  $P_T > P_L$ .

$P_T$ : The power generated by wind

$P_L$ : The power consumed by the load.

The BESS provides the power for the WDHS network: In this case,  $P_S < 0$  and  $P_T < P_L$ .

Also, the excess wind can be consumed by the DL,  $P_D > 0$ , we can write:

$$P_T - P_L - P_D - P_S = J\omega \frac{d\omega}{dt} \quad (3.1)$$

Where

$P_T$ : The power generated by wind

$P_L$ : The active power consumed by the load (in any wind mode, most of the time  $P_T > P_L$ )

$J$  is the system inertia,

$$\omega = 2\pi f / p \quad (3.2)$$

$\omega$ : The speed of the shaft of the synchronous machine (MS) in rad / s,

$p$ : The number of pairs pole of SM.

In equation 3.1, losses are not taken into account. This means that;  $P_D < P_{D\_NOM}$  and  $P_S < P_{S\_NOM}$  (nominal value of each associated converter).

To maintain the constant synchronous speed, we can write:

$$\frac{d\omega}{dt} = 0 \quad (3.3)$$

The regulator of DL and the BESS energy storage system must be synchronized to extract any excess wind power that cannot be stored. So, the equation 3.1 becomes:

$$P_T - P_L = P_D + P_S \quad (3.4)$$

Figure 3.4 and 3.5 respectively represent the principle of the frequency control system and the method of power sharing between the loads DL and the BESS. The frequency regulator receives the frequency error (the difference between the network frequency and the reference frequency 60 Hz) and delivers the reference power  $P_{REF}$  for the energy storage system

(BESS) and the control blocks of DL. Under normal conditions, the power at the BESS node approaches its nominal power.

$$\begin{aligned} P_{REF} &= P_{S-REF} + P_{D-REF} & (3.5) \\ P_{D-REF} &= 0 \text{ if } P_{REF} < P_{S-NOM} \end{aligned}$$

Equation 3.5 became  $P_{REF} = P_{D-REF}$  when the battery is fully charged ( $P_{S-REF}$ ). DL is used when  $P_{REF}$  exceeds the nominal power of BESS. This ensures the power storage by the DL that the battery cannot be extracted. With a positive power limit signal PPL,  $P_{S-MAX}$  which varies between 0 and  $P_{S-NOM}$ , the power sharing between the loads DL and the energy storage system will ensure that the DL will absorb the excess power that battery cannot store.

However:

$$\begin{aligned} P_{S-REF} &= P_{REF} \text{ if } P_{REF} \leq 0 & (3.6) \\ P_{S-REF} &= P_{S-MAX} \text{ if } P_{REF} > 0 \end{aligned}$$

In the DL's:

$$\begin{aligned} P_{D-REF} &= P_{REF} - P_{S-MAX} \text{ if } P_{REF} > 0 & (3.7) \\ P_{D-REF} &= 0 \text{ if } P_{REF} \leq 0 \end{aligned}$$

- The sharing of power ensures that the DL can only absorb the excess wind energy that the BESS cannot store. To make this possible, the DL and BESS controllers must know the reference power  $P_{REF}$  with the same accuracy at the same time. Three modes of control could be performed;
- For the load DL only (BESS is fully charged  $P_S = 0$ ,  $P_T - P_L > P_{S-MAX}$ );
- By the load DL and BESS, when  $P_T - P_L > 0$  ( $P_{REF} > 0$ );
- By the BESS only ( $P_D = 0$ ) when  $|P_T - P_L| \leq P_{S-NOM}$

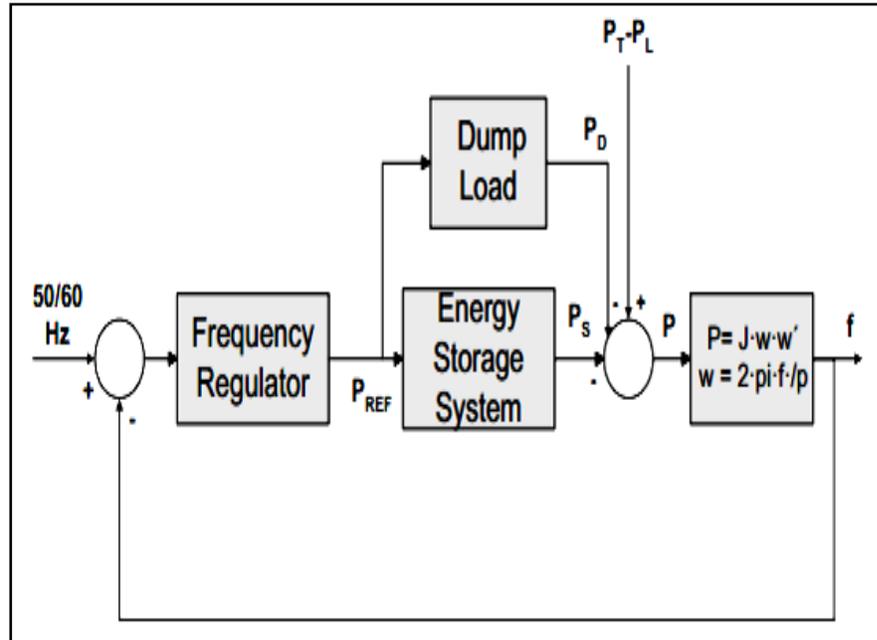


Figure 3.4 Block diagram of the frequency control system  
Adapted from (Sebastián and Quesada, 2015)

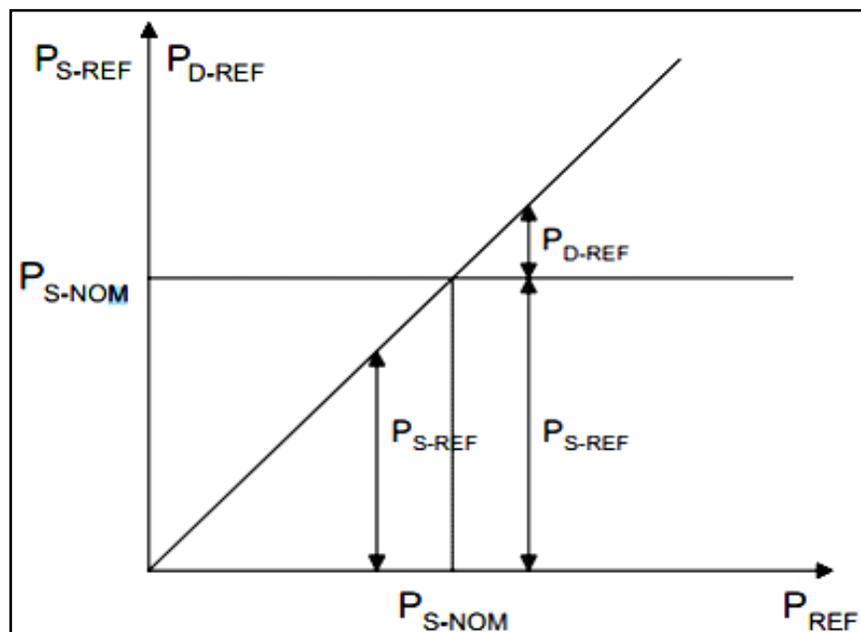


Figure 3.5 Frequency control system using power sharing  
Adapted from (Sebastián and Quesada, 2015)

### 3.3.2 The control of BESS

The control system of BESS operates in two modes (Sebastián and Quesada, 2015):

Rectifier mode: The battery absorbs energy  $P_s > 0$  and consequently it charges and the current passes from the autonomous network to the battery. Generally, under this condition the wind speed is quite large and the power supplied by the wind DG is not absorbed by the consumer load. Therefore, the excess energy is absorbed by the battery for subsequent use;

Inverter mode: The battery provides energy  $P_s < 0$  and therefore it discharges and current flows to the autonomous network from the battery in order to supply the energy requirements to supply the load. Generally, under this condition the wind speed is limited and the power supplied by the wind DG is not sufficient to supply the energy to the consumer.

### 3.4 Case study: connecting a wind turbine to the power grid with storage system

In this case study, we will observe the frequency behavior with storage system (battery) in the network and according to scenarios; we will try to improve the frequency quality response using storage system and controllers (PID and Fuzzy). For this study, a model has been taken which is developed for the High Penetration, No Storage of Wind-Diesel system (HPNSWD). This strategy was promoted by Hydro-Quebec for a remote area to minimize the cost of power electricity. The maximum power from wind in the network depends on attainable wind resource and cost of fuel. Mott and Saulnier (2014) show the first commercial application of HPNSWD technology. For this case study a 480 V, 275 kVA wind turbine based on induction generator, a 480 V, 300 kVA synchronous generators, a variable secondary load (0 to 446.25 kW), battery (240 V, 390Ah) and a 230 kW consumer load is used according to the scenarios. Matlab (2015).

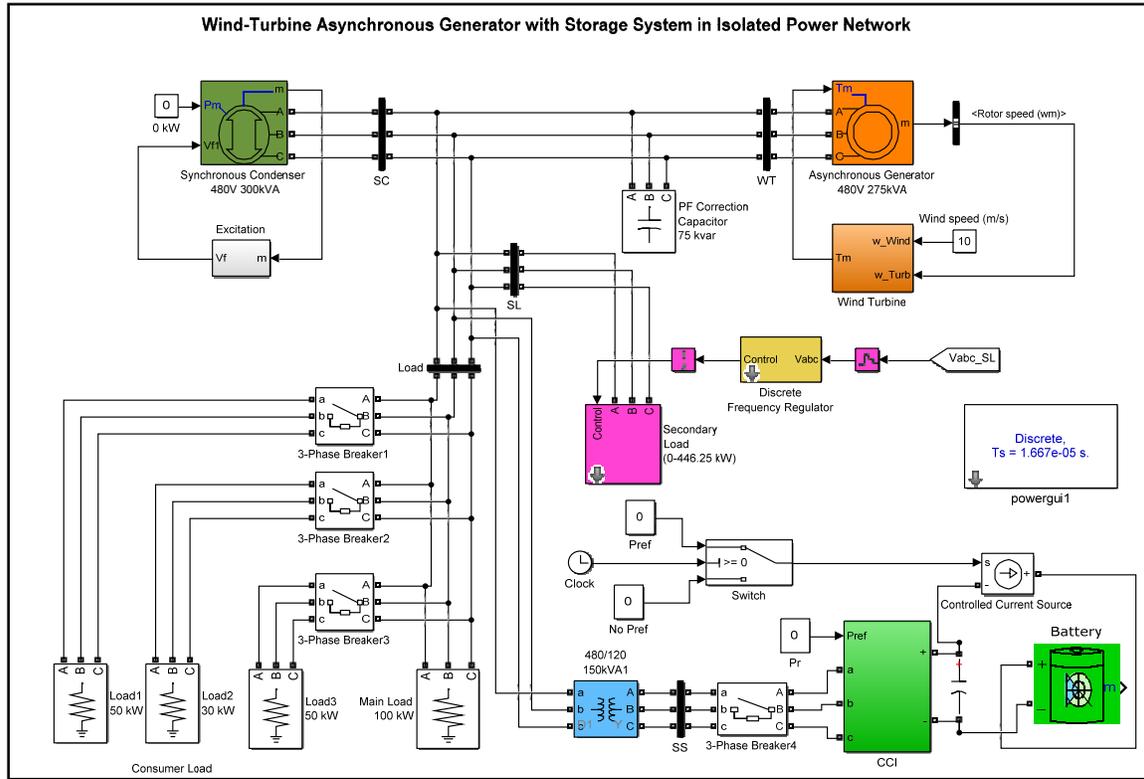


Figure 3.6 Simulink model of hybrid network with BESS in an isolated area wind mode only

Table 3.1 A hybrid network with BESS systems parameters

Network	Synchronous Generator : 480 V, 300 kVA
Turbine	480 V, 275 kVA induction generator P <sub>nom</sub> = 200 kW Wind speed V <sub>wind_nom</sub> = 10 m/s Pitch angle = 0 deg, P=P <sub>nom</sub> and V=V <sub>nom</sub>
Buses	1. Synchronous Condenser Bus (SC) 2. Wind Turbine Bus (WT) 3. Secondary/Dump Load Bus (SL) 4. Main Load Bus (Load) 5. Storage System
Load	Main Load 100 kW Extra Load 50 kW + 30 kW + 50 kW Secondary/Dump Load vary 0 to 446.25 kW by step of 1.75 kW
Transformer	480 kV / 120 kV, 150 kVA
Storage System (Battery)	240 V, 390Ah and SOC:50%

In this case study, we will observe three types of scenarios of power system to control the frequency:

**Scenario 1:** When wind power ( $P_T$ ) > Total load ( $P_L$ ). Where, battery ( $P_S$ ) fully charged;

**Scenario 2:** When wind power ( $P_T$ ) > Total load ( $P_L$ ). Where, battery ( $P_S$ ) is charged;

**Scenario 3:** When wind power ( $P_T$ ) < Total load ( $P_L$ ). Where, battery ( $P_S$ ) is discharged.

In these scenarios, PID and Fuzzy logic controller has been used to see the frequency stability in the network

### 3.5 Simulation: Scenario 1

#### 3.5.1 Frequency control by PID, When ( $P_T > P_L$ ) where, $P_S$ fully charged

Here, wind speed (10 m/s) is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 3.7 (a). Figure 3.7 (b) shows, the consumer (main) load is 100 kW. At 0.5 sec, an extra 50kW has been added. The secondary load absorbs 50 kW to regulate a 60 Hz frequency shown in figure 3.7 (c).

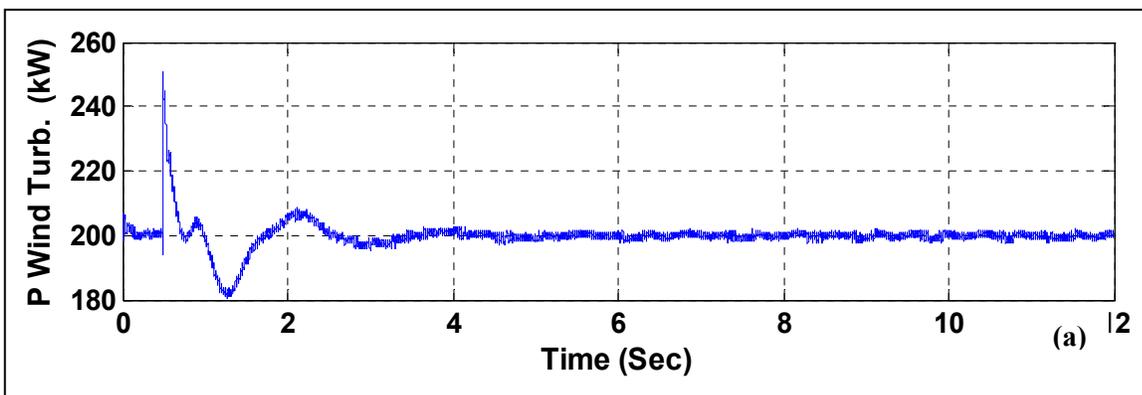


Figure 3.7 (a) Power from wind turbine, using PID controller

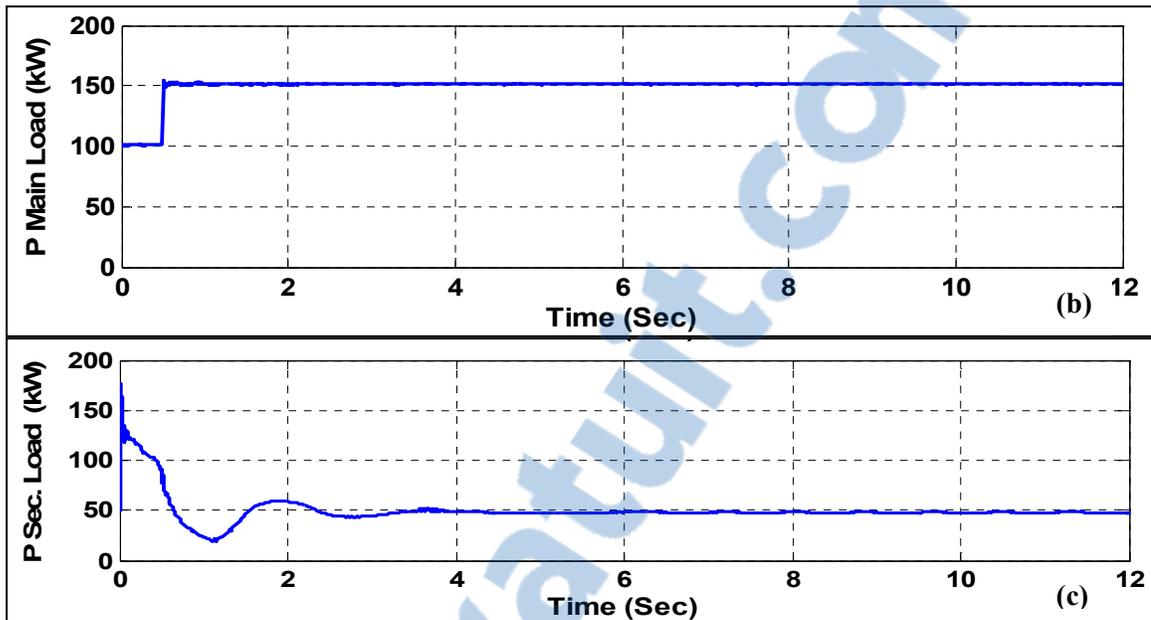


Figure 3.7 (b) Power absorbed by Secondary load and (c) Power absorbed by the main load, using PID controller

Figure 3.8 shows, the frequency are controlled by discrete frequency regulator. To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). The frequency error is then integrated to obtain a phase error. The phase error is applied to the Proportional-Derivative (PD) controller to generate an output signal to get the required secondary load power. Here the simulation has been run for 12s.

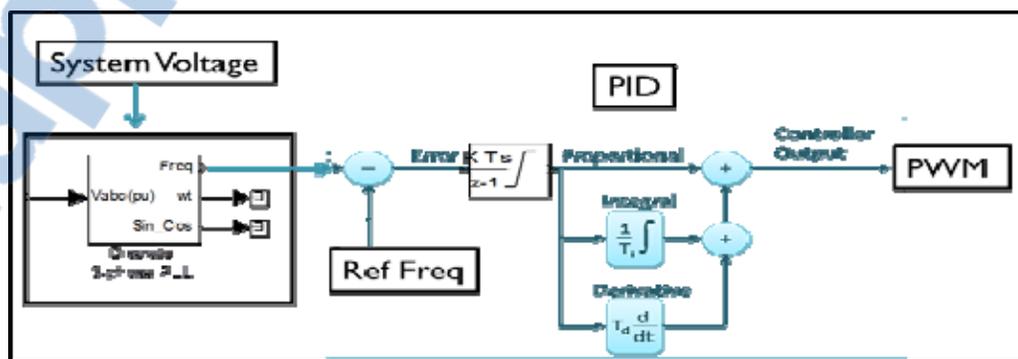


Figure 3.8 Operational block diagram of frequency control using PID controller

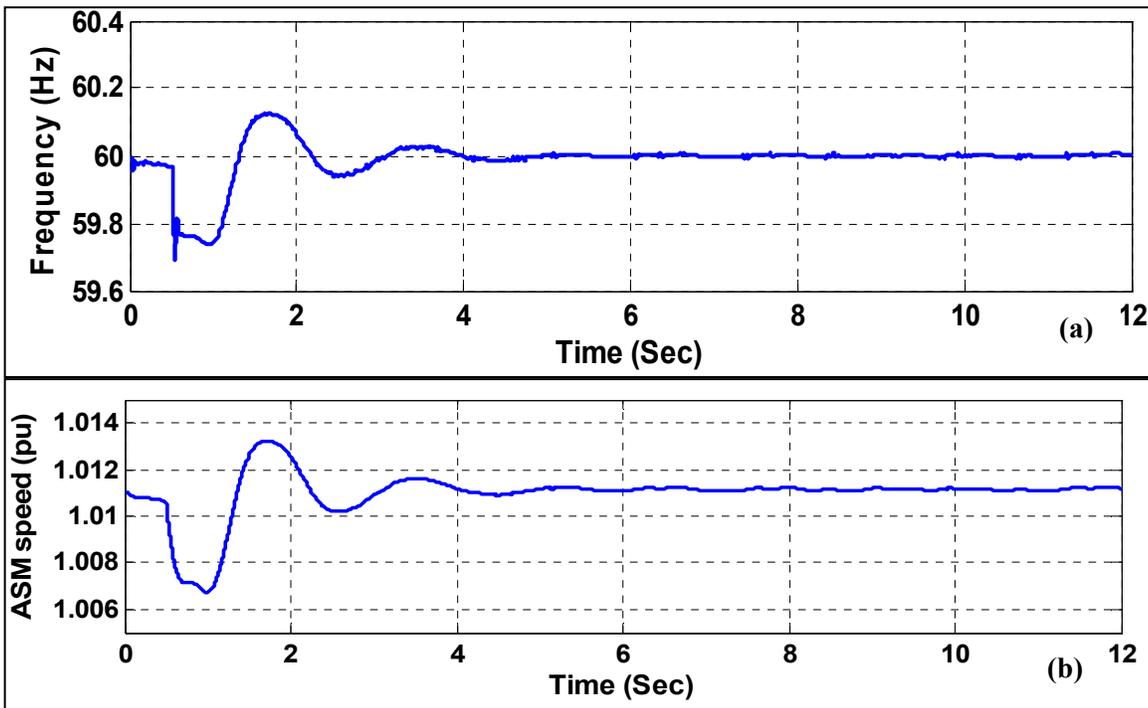


Figure 3.9 (a) Frequency at load bus and (b) Speed generated by asynchronous generator, using PID controller

Figure 3.9 (a) shows, after 12s simulation, the frequency drops to 59.68 Hz at 0.5s due to extra load of 50kW.. Figure 3.9 (b) shows, the speed of the asynchronous machine is above (1.011 pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when turbine runs at 10 m/s wind speed. Due to some asynchronous machine losses, the wind turbine generates 200 kW.

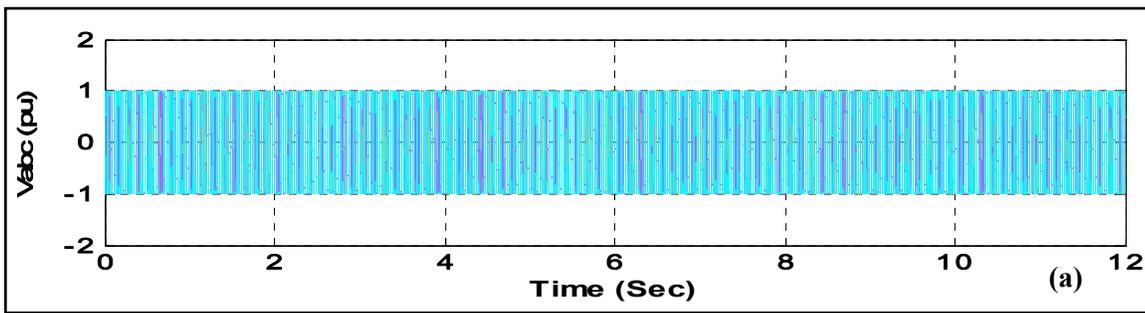


Figure 3.10 (a) Voltage at load bus, using PID controller

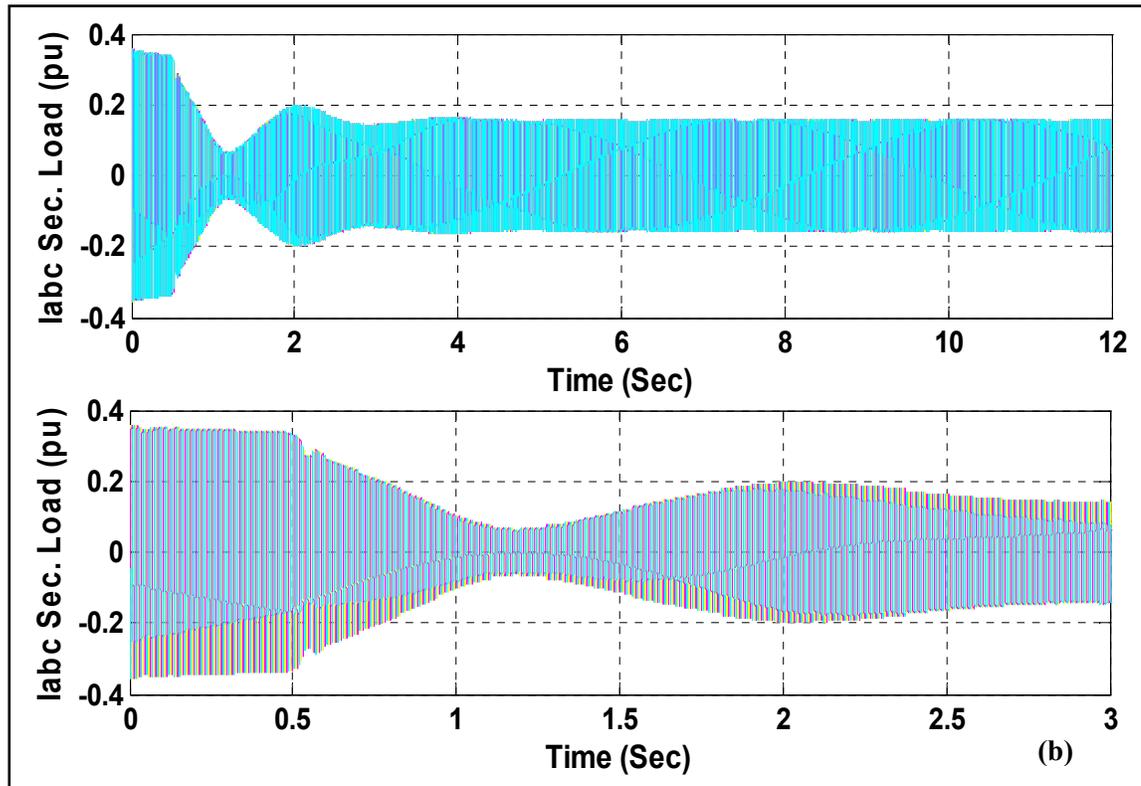


Figure 3.10 (b) Current at secondary loads, using PID controller

Figure 3.10 (a) shows, load voltage remains at 1 (pu) and no flicker is seen. Figure 3.10 (b) shows, the secondary load current decrease at 0.5s due to extra load of 50kW and remains 0.15 (pu) until simulation. To see more visible we took data from 0s to 3s.

### 3.5.2 Fuzzy logic controller

#### 3.5.2.1 Introduction

Boolean logic is a logical approach that based on true or false condition. On the opposite, fuzzy logic allows the truth to be located between 0 and 1. In this case, we talk about 'degree of truth'. The fuzzy logic controller has four main operational parts shown in figure 3.11: (a) Fuzzification interface, (b) Rule base interface matrix, (c) Fuzzy inference engine and (d)

Defuzzification interface (Ross et al., 2010). Fuzzification interface mainly involves with inputs parameters. The input parameters are fuzzified to determine the pre-defined input function (membership functions). It can have various shapes like triangular, sinusoidal, trapezoidal and exponential. The membership functions are defined by setting a selected input on X axis and quantity of classes of membership input variable on Y axis. The membership function should vary within zero and one. The rule-base interface matrix is used to determine the fuzzy sets and operation as a conditional function. For a fuzzy system, a rule can be written as follows:

If x is A and y is B, then z is C

Where, A and B = Set of conditions that must be satisfied and z = Set of outcomes can be deduced. Defuzzification interface converts the fuzzy value into the crisp value. There are several methods of defuzzification interface: max-membership, centroid, bisector mean and weight average (Ross et al., 2010).

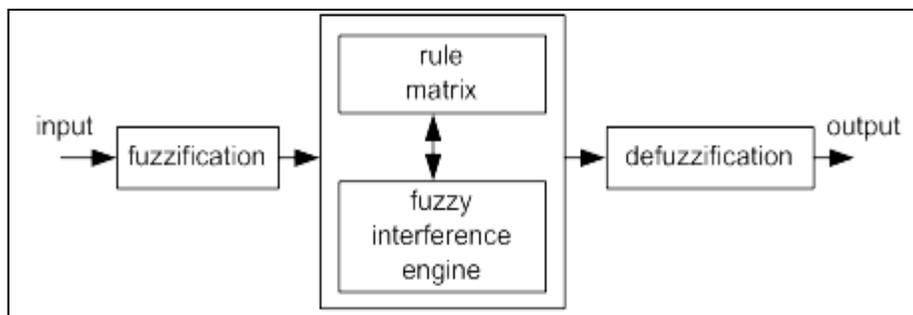


Figure 3.11 Operation of fuzzy logic controller  
Adapted from Fullér et al. (1996)

### 3.5.2.2 Fuzzy logic membership function and rules

**Step 1:** First, input and output of fuzzy logic controller and its variable range should be determined. As a base rule, input signal should be in IF section and the output signal in the THEN section.

**Step 2:** Second, the sets of fuzzy and membership functions should be determined. Then the degree of membership function connected every input variable. Here output signal is discerned.

**Step 3:** Fuzzy inference engine should be narrated. Here, the fuzzy rules are converted into control rules and run the systems according to these rules.

**Step 4:** Finally, defuzzification interface process the rules and converts the fuzzy values into the crisp values.

Here, fuzzifier converts two inputs signal. One is frequency error signal ( $\Delta\omega$ ) as a main signal and another is derivative of frequency error (Change of rate) signal  $\Delta(\Delta\omega)$ . Defuzzification converts one output signal (PWM signal).

In this system the first input is frequency error signal (input 1) which has three membership functions. The range of input variable is -1 to +1. The membership functions of this input where the domain is divided into three linguistic zones denoted by ‘Negative Error’ (-1 -1 0), ‘Zero Error’ (-1 0 1) and ‘Positive Error’ (0 1 1). The shape of all membership function is associated with a triangular based membership function. The membership function for each linguistic variable is shown in Figure 3.12 (a).

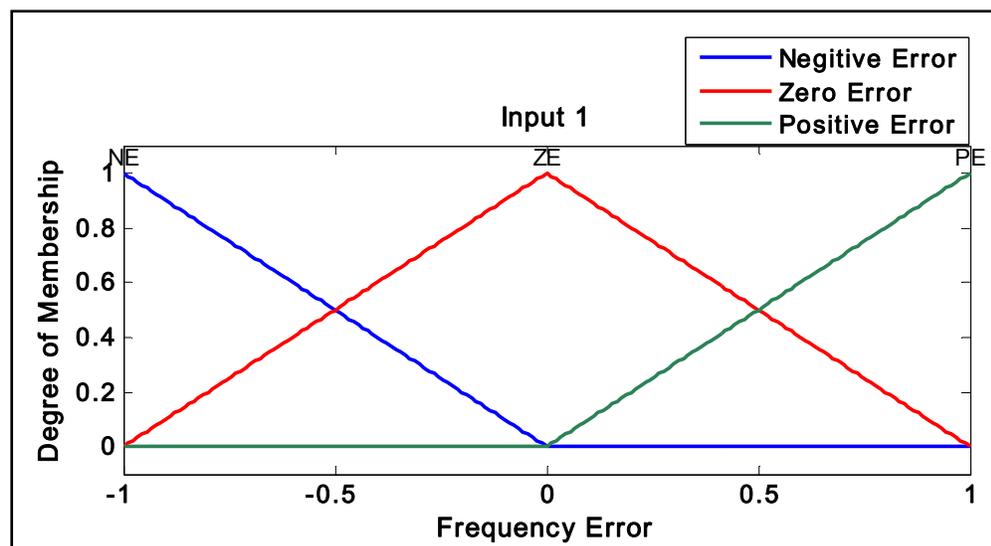


Figure 3.12 (a) Membership function, Input variable 1

The second input is derivative of frequency error (rate of change signal) which has three membership functions. The range of input variable is -1 to +1. The membership functions of this input where the domain is divided into three linguistic zones denoted by ‘Negative Error’ (-1 -1 0), ‘Zero Error’ (-1 0 1) and ‘Positive Error’ (0 1 1). The shape of all membership function is associated with a triangular based membership function and they overlap each other. The membership function for each linguistic variable is shown in Figure 3.12 (b)

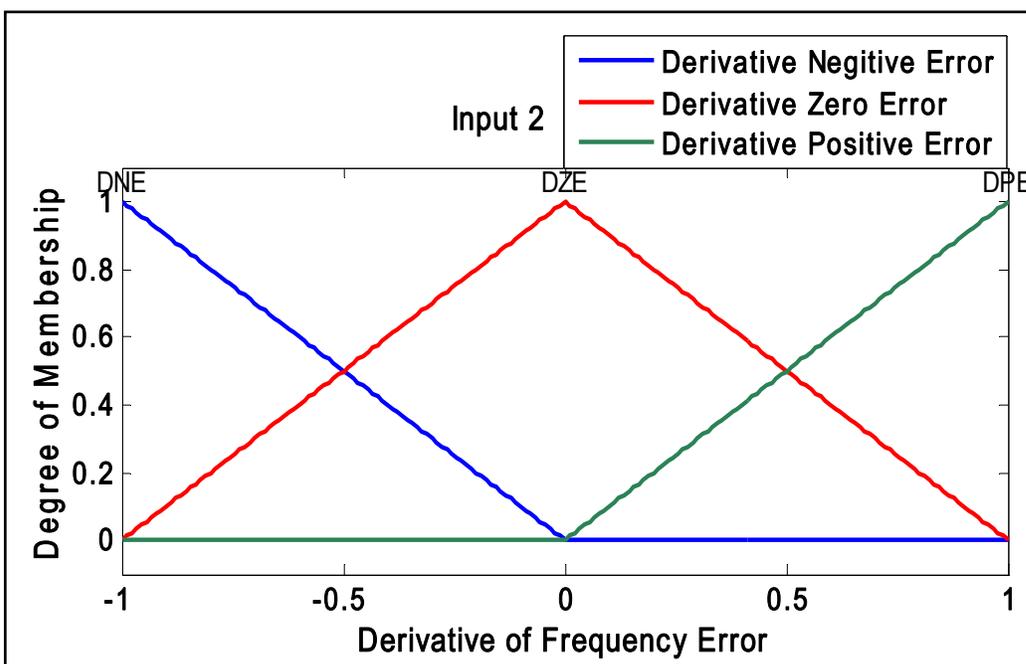


Figure 3.12 (b) Membership function, Input variable 2

The output of membership function is based on PWM signal which has five membership functions. The range of input variable is -1 to +1. The membership functions of this output where the domain is divided into five linguistic zones denoted by ‘Negative Large’ (-1 -1 -1), ‘Negative Small’ (-0.5 -0.5 -0.5), ‘Zero’ (0 0 0), ‘Positive Small’ (0.5 0.5 0.5) and ‘Positive Large’ (1 1 1). The shape of all membership function is associated with a triangular based membership function. The membership function for each linguistic variable is shown in Figure 3.13.

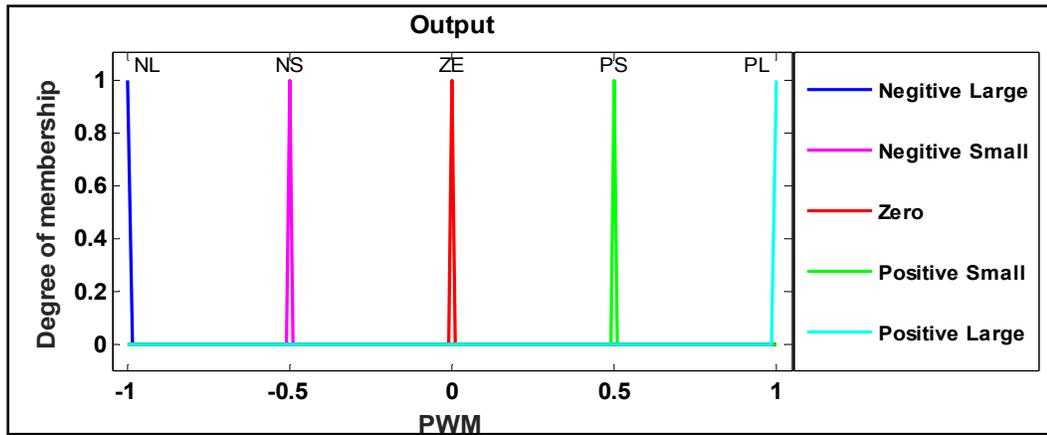


Figure 3.13 Membership function of output variable

The main part of fuzzy logic is the rules and the inference mechanism. The rules are normally arranged in a set of fuzzy linguistic algorithm, with each rule triggered with varying belief to support the input and output of membership function. In this system, a set of nine rules are determined in this study as follows. For each and every fuzzy set, triangular membership function has been used.

Table 3.2 Fuzzy logic operational rules

1.	<b>If (Frequency Error is NE) and (Derivative of Frequency Error is NdE) then (PWM is NL)</b>
2.	<b>If (Frequency Error is NE) and (Derivative of Frequency Error is ZdE) then (PWM is NS)</b>
3.	<b>If (Frequency Error is NE) and (Derivative of Frequency Error is PdE) then (PWM is ZE)</b>
4.	<b>If (Frequency Error is ZE) and (Derivative of Frequency Error is NdE) then (PWM is NS)</b>
5.	<b>If (Frequency Error is ZE) and (Derivative of Frequency Error is ZdE) then (PWM is ZE)</b>
6.	<b>If (Frequency Error is ZE) and (Derivative of Frequency Error is PdE) then (PWM is PS)</b>
7.	<b>If (Frequency Error is PE) and (Derivative of Frequency Error is NdE) then (PWM is ZE)</b>
8.	<b>If (Frequency Error is PE) and (Derivative of Frequency Error is ZdE) then (PWM is PS)</b>
9.	<b>If (Frequency Error is PE) and (Derivative of Frequency Error is PdE) then (PWM is PL)</b>

### 3.5.3 Frequency control using Fuzzy logic controller, When ( $P_T > P_L$ ) where, $P_S$ fully charged

The wind speed (10 m/s) is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 3.14 (a). Figure 3.14 (b) shows, the consumer (main) load is 100 kW. At 0.5 sec, an extra 50kW has been added. The secondary load absorbs 50 kW to regulate a 60 Hz frequency shown in figure 3.14 (c).

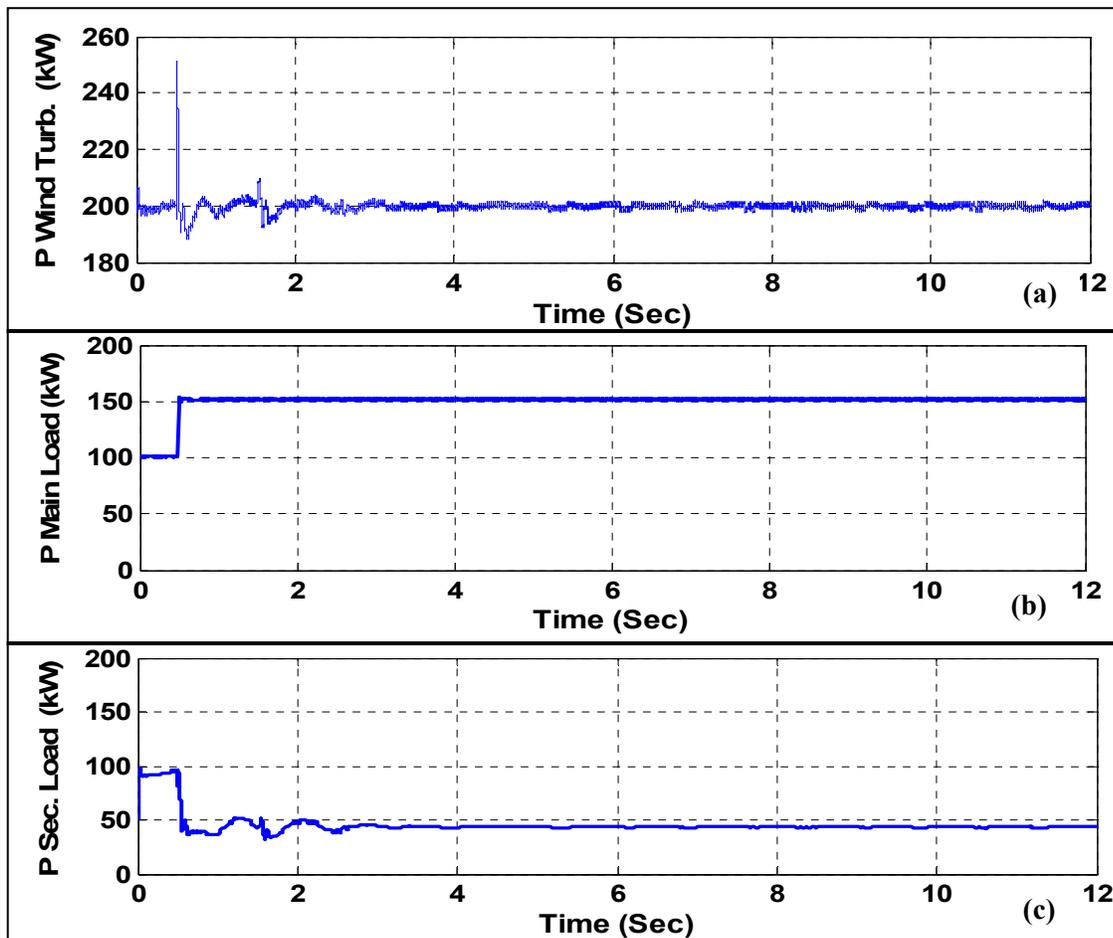


Figure 3.14 (a) Power from wind turbine, (b) Power absorbed by secondary load and (c) Power absorbed by the main load, using Fuzzy logic controller

Figure 3.15 shows, the frequency are controlled by discrete frequency regulator. To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). Finally, the frequency error and derivative of frequency error signal are applied to the fuzzy logic controller to generate an output signal to get the required secondary load power. The simulation has been run for 12s.

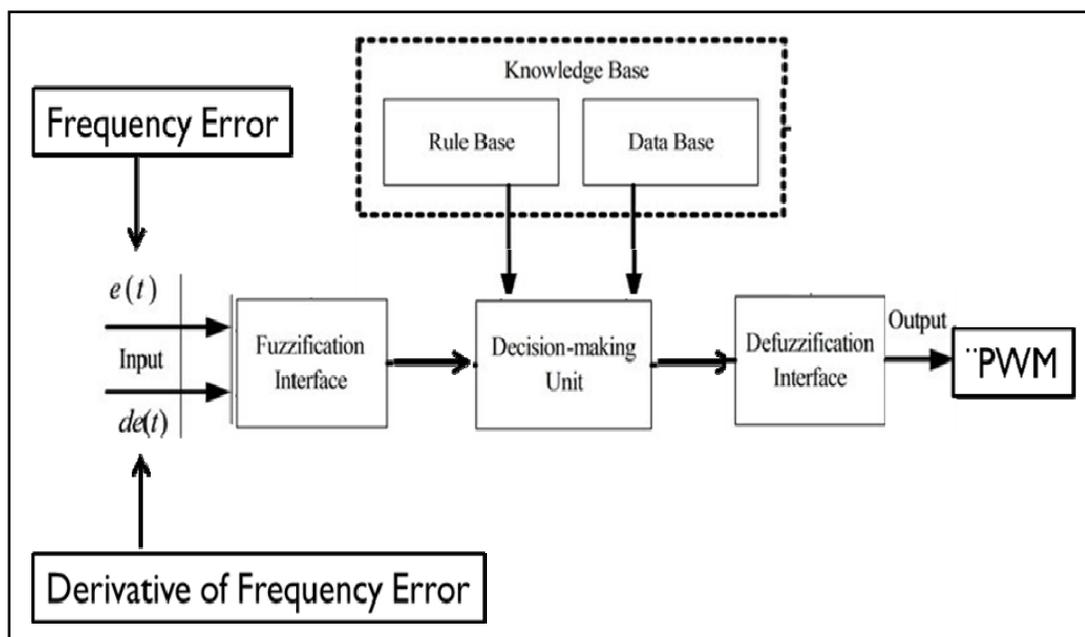


Figure 3.15 Simulink block diagram of fuzzy logic controller

Figure 3.16 (a) shows, after 12s simulation, the frequency drops to 59.72 Hz at 0.5s due to extra load of 50kW. Figure 3.16 (b) shows, the speed of the asynchronous machine is above (1.011 pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when turbine runs at 10 m/s wind speed. Due to some asynchronous machine losses, the wind turbine generates 200 kW.

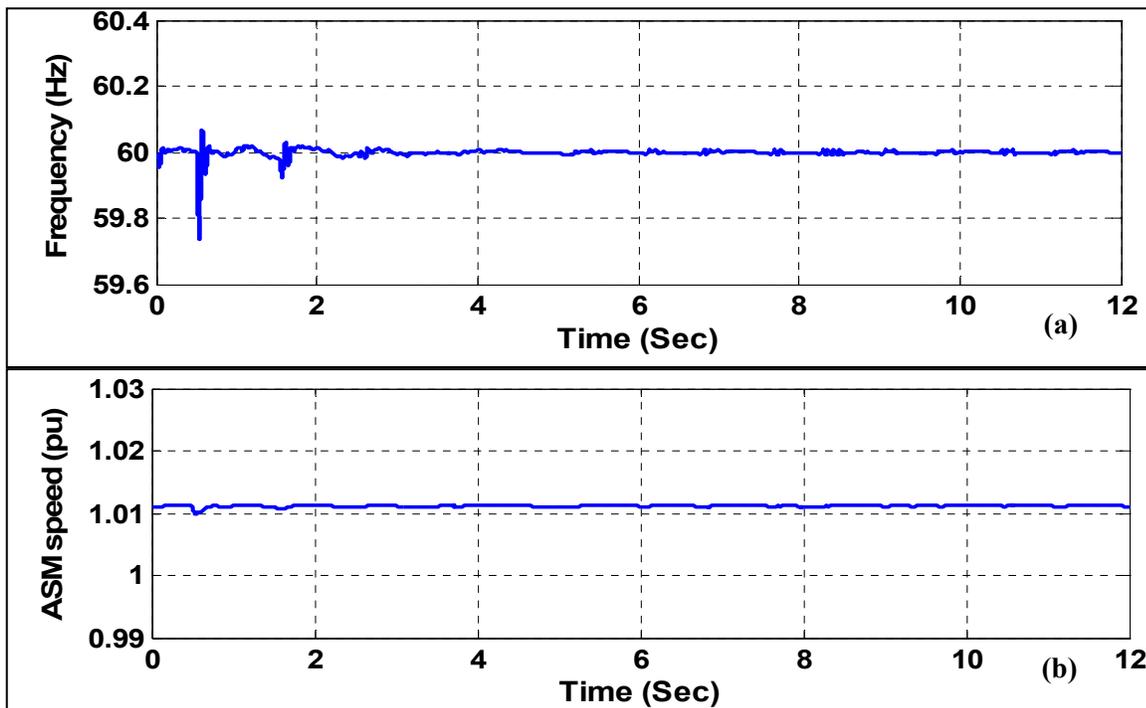


Figure 3.16 (a) Frequency at load bus and (b) Speed generated by asynchronous generator, using Fuzzy logic controller

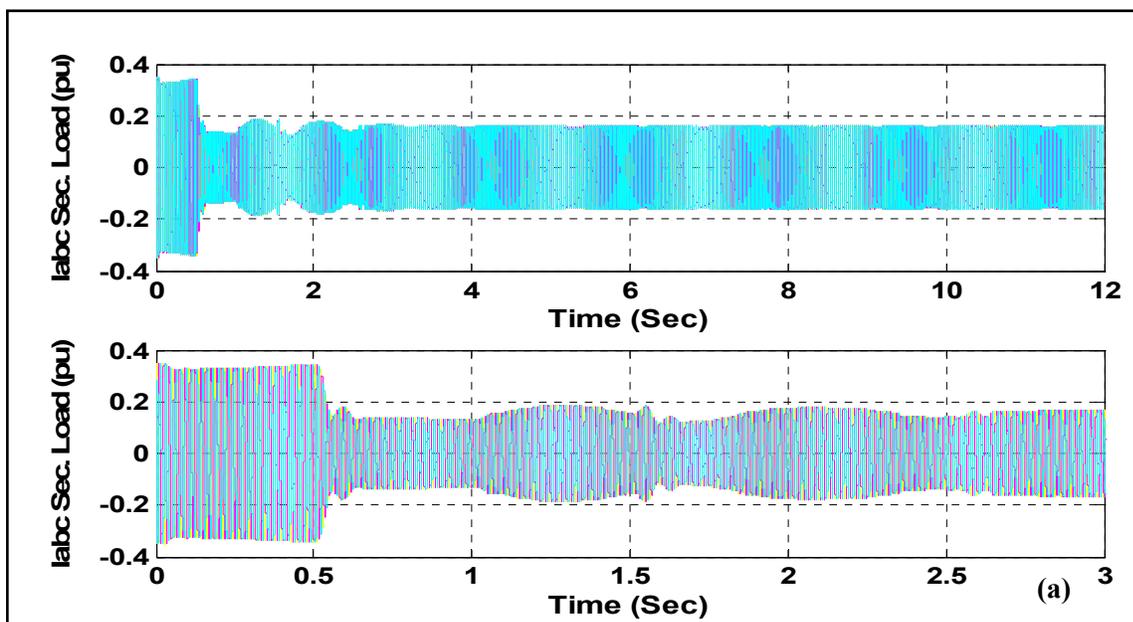


Figure 3.17 (a) Current at secondary loads, using Fuzzy logic controller

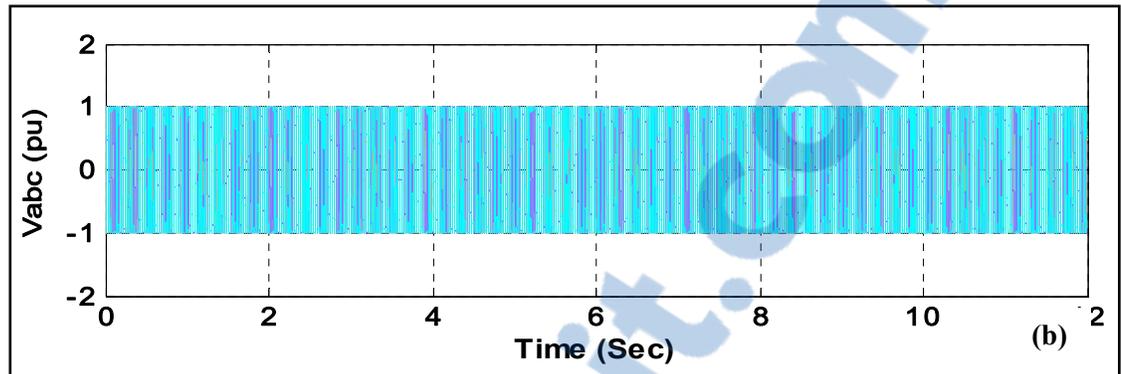


Figure 3.17 (b) Voltage at load bus, using PID controller

Figure 3.17 (a) shows, the secondary load current decrease at 0.5s due to extra load of 50kW and remains 0.15 (pu) until end of simulation. To see more visible we took data from 0s to 3s. Figure 3.17 (b) shows, load voltage remains at 1 (pu) and no flicker is seen.

### 3.5.4 Comparison between PID and fuzzy logic controller to control the frequency, when ( $P_T > P_L$ ) where, $P_S$ fully charged

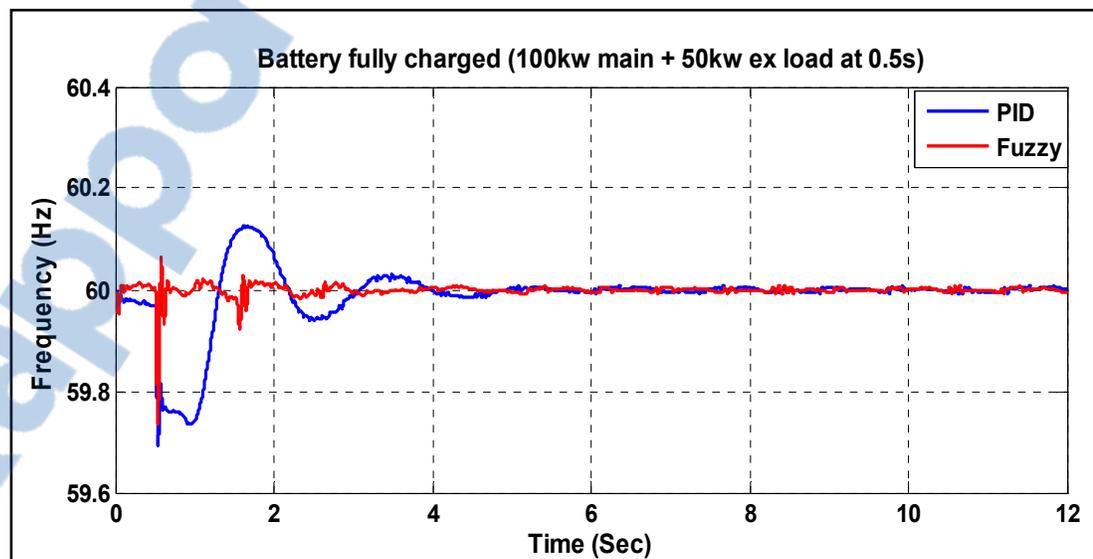


Figure 3.18 Fluctuation observations of frequency compare between PID controller and Fuzzy logic controllers when battery fully charged

From figure 3.18, we observed that the fluctuation behavior of frequency with PID controller is higher than a fuzzy logic controller. The convergence time with fuzzy controller is also faster than PID controller. In PID, frequency drops 59.68 Hz at 0.5s due to extra load of 50kW. But using fuzzy logic controller, frequency drops 59.72 Hz at 0.5s due to extra load of 50kW. Using PID, fluctuation of frequency transient time is from 0s to 4.5s while in the Fuzzy logic controller it is from 0s to 2s. So, it is clear from above graphs that the frequency takes more time to become stable in PID rather than fuzzy logic controller.

To observe frequency fluctuation on this same system now we will study the scenario 2 and scenario 3 to see which controller can give much more stability in the network to control the frequency and can reduce the transient time for the fluctuation of frequency.

In scenario 1, we observed that the power produce from wind turbine is 200kW and total consumer load is 150kW (100kW as a main load and 50kW are added at 0.5s of simulation). So we have 50kW surplus power from wind turbine. Here, battery is fully charged that's why we had to dump 50kW power in the secondary/dump load (DL), which is not a good idea. It's better to use the power or charge the battery when we have surplus power so that we can use it to maintain the higher load demand or any power crisis (shown in scenario 3).

### **3.6 Simulation: Scenario 2**

#### **3.6.1 Frequency control by PID, When ( $P_T > P_L$ ) where, $P_s$ is charged**

Here, wind speed (10 m/s) is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 3.19 (a). Figure 3.19 (b) shows, the consumer (main) load is 100 kW. At 0.5s, an extra 50kW has been added. Figure 3.19 (c) shows, the battery is charging (rate of 30 kW) at 3s. So the secondary load absorbs 20 kW to regulate a 60 Hz frequency shown in figure 3.19 (d).

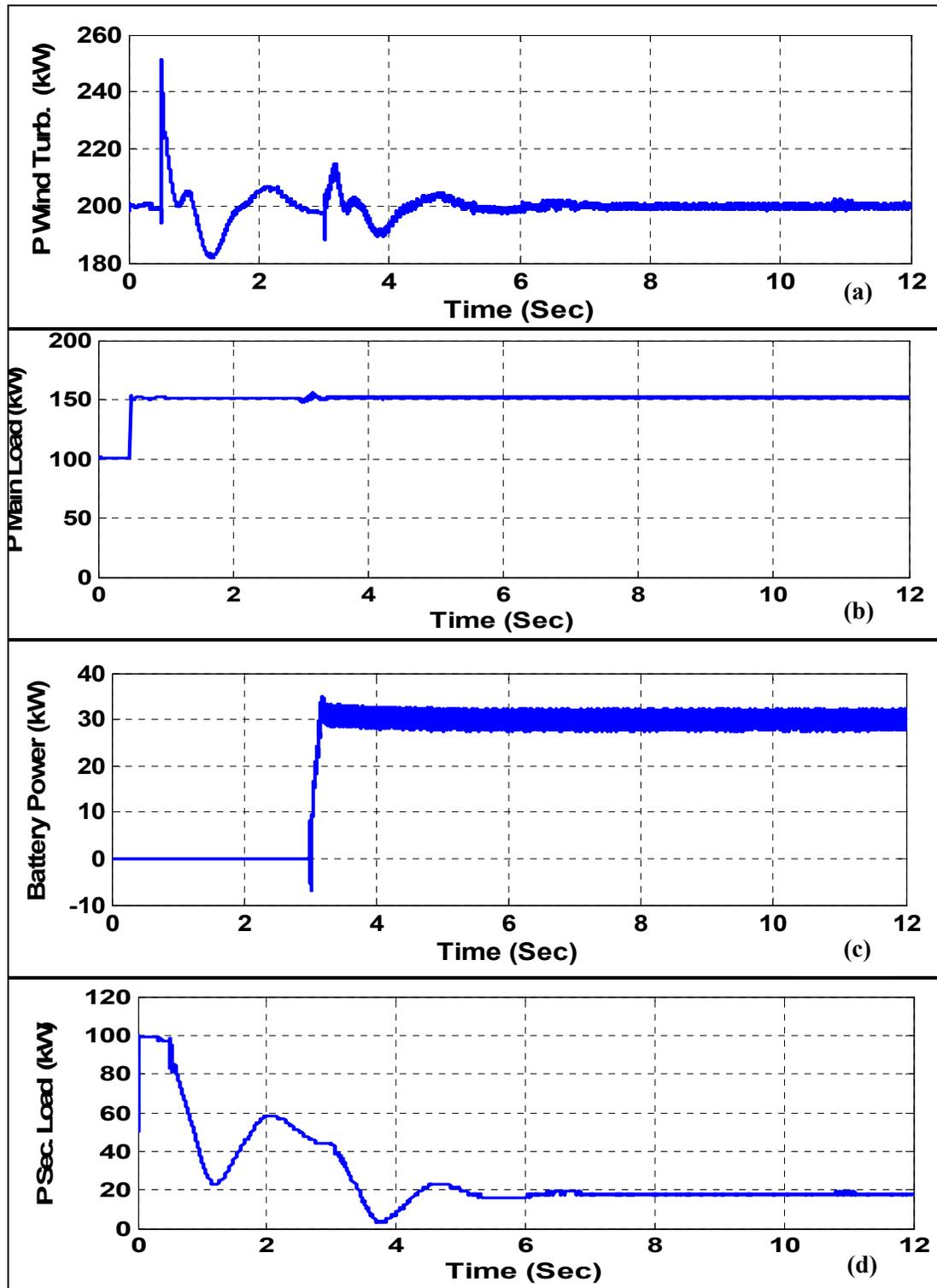


Figure 3.19 (a) Power from wind turbine, (b) Power absorbed by main load, (c) Power from battery and (d) Power absorbed by Secondary load, using PID controller

Figure 3.20 (a) shows, State of charge (SOC) of battery (50%), where battery is charging at 3s. Until end of simulation the battery is charged 47.9% to 48.02%. Figure 3.20 (b) shows, the battery current situation. Before 3s, the current of battery was zero. But after 3s, battery has -200 A to charge itself with a rate of 30kW. Figure 3.20 (c) shows, the voltage is increasing at 3s and remain 262 V until end of simulation.

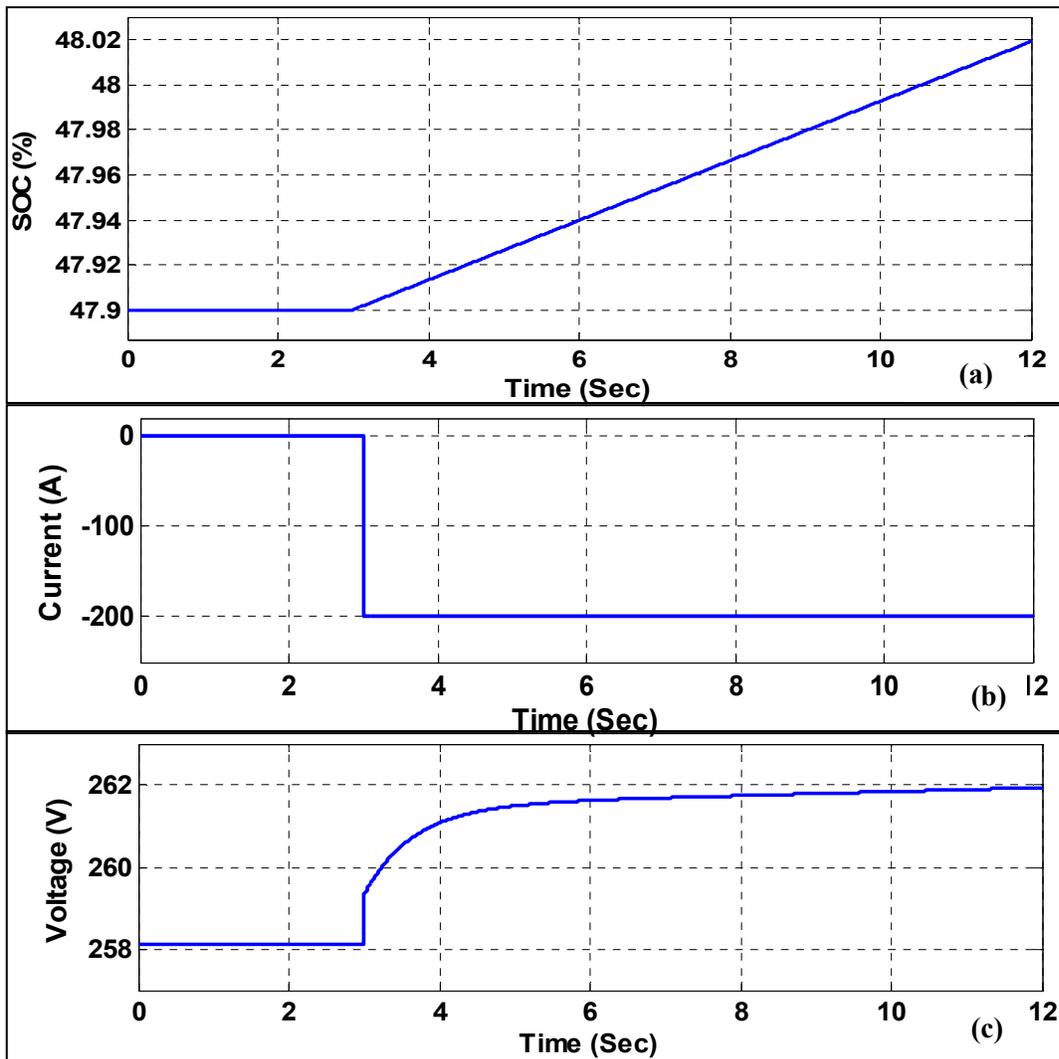


Figure 3.20 (a) State of charge (SOC) of battery, (b) Current in the battery and (c) Voltage in the battery, when battery is charging

To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). The frequency error is then integrated to obtain a phase error. The phase error is applied to the Proportional-Derivative (PD) controller to generate an output signal to get the required secondary load power. Here the simulation has been run for 12s

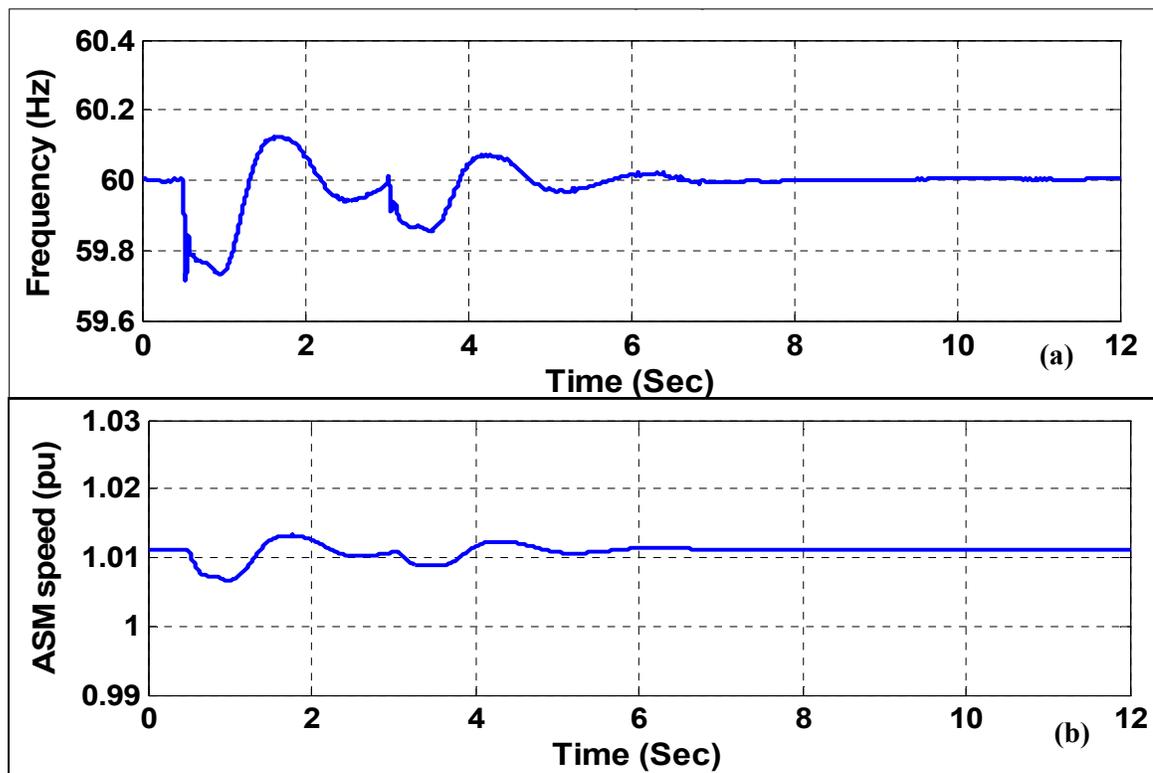


Figure 3.21 (a) Frequency at load bus and (b) Speed generated by asynchronous generator, using PID controller

Figure 3.21 (a) shows, after 12s simulation, the frequency drops to 59.68 Hz at 0.5s due to extra load of 50kW. At 3s battery is started to charge (rate of 30kW) and for that reason frequency drops to 59.82 Hz. Figure 3.21 (b) shows, the speed of the asynchronous machine is above (1.011 pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when turbine runs at 10 m/s wind speed. Due to some asynchronous machine losses, the wind turbine generates 200 kW.

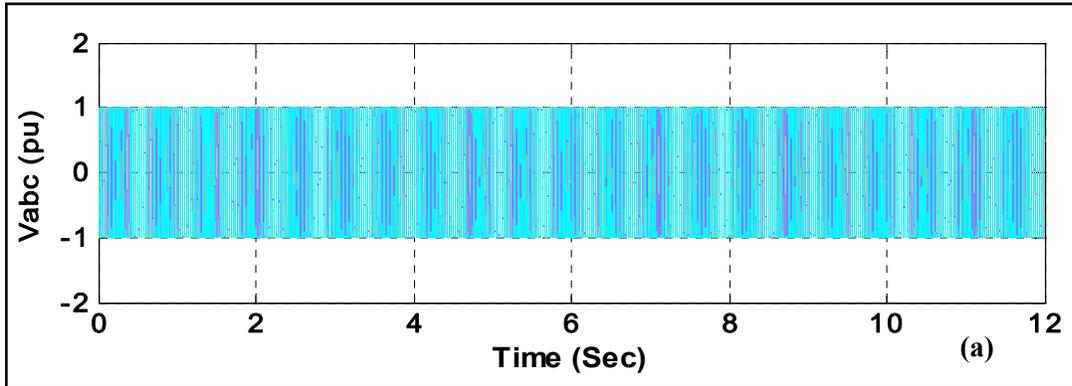


Figure 3.22 (a) Voltage at load bus, using PID controller

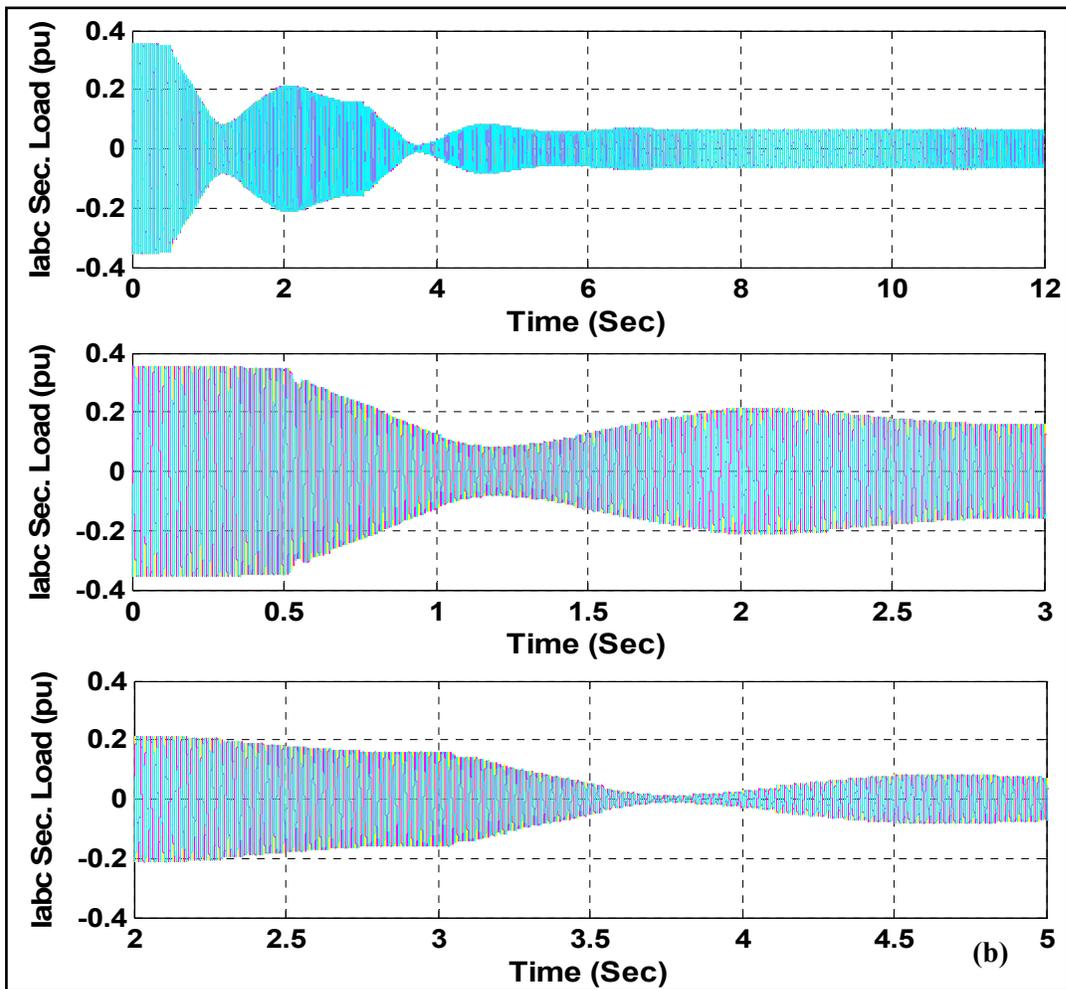


Figure 3.22 (b) Current at secondary loads, using PID controller

Figure 3.22 (a) shows, load voltage remains at 1 (pu) and no flicker is seen. Figure 3.22 (b) shows, the secondary load current decrease at 0.5s due to extra load of 50kW and at 3s due to charging condition of battery (rate of 30kW). Current remain 0.1 (pu) until end of simulation. To see more visible we took data from 0s to 3s and 2s to 5s.

### 3.6.2 Frequency control using Fuzzy logic controller, When ( $P_T > P_L$ ) where, $P_S$ is charged

The wind speed (10 m/s) is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 3.23 (a). Figure 3.23 (b) shows, the consumer (main) load is 100 kW. At 0.5s, an extra 50kW has been added. Figure 3.23 (c) shows, the battery is charging (rate of 30 kW) at 3s. So the secondary load absorbs 20 kW to regulate a 60 Hz frequency shown in figure 3.23 (d).

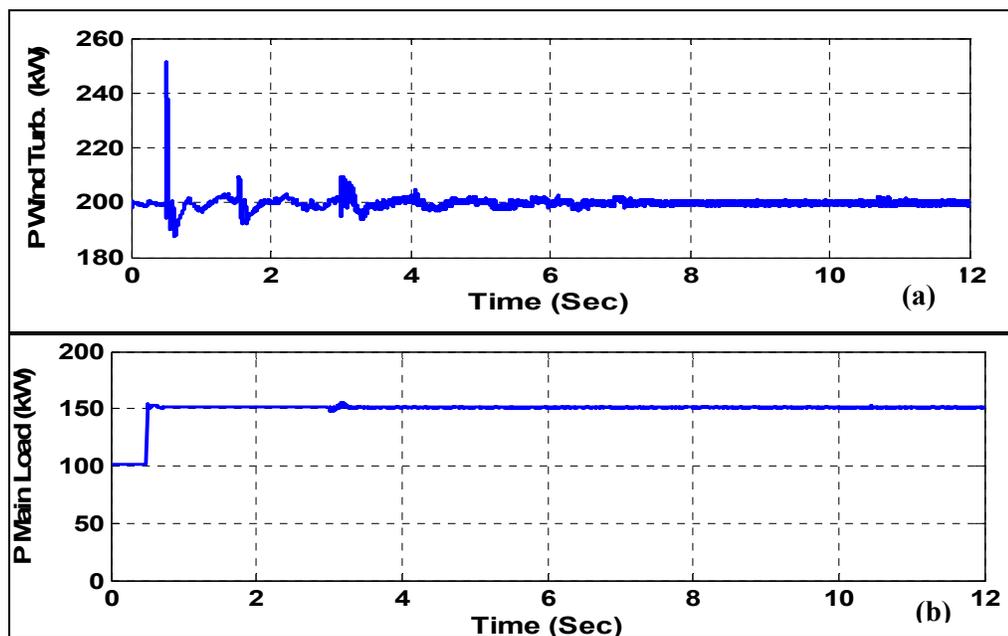


Figure 3.23 (a) Power from wind turbine, (b) Power absorbed by main load using Fuzzy logic controller

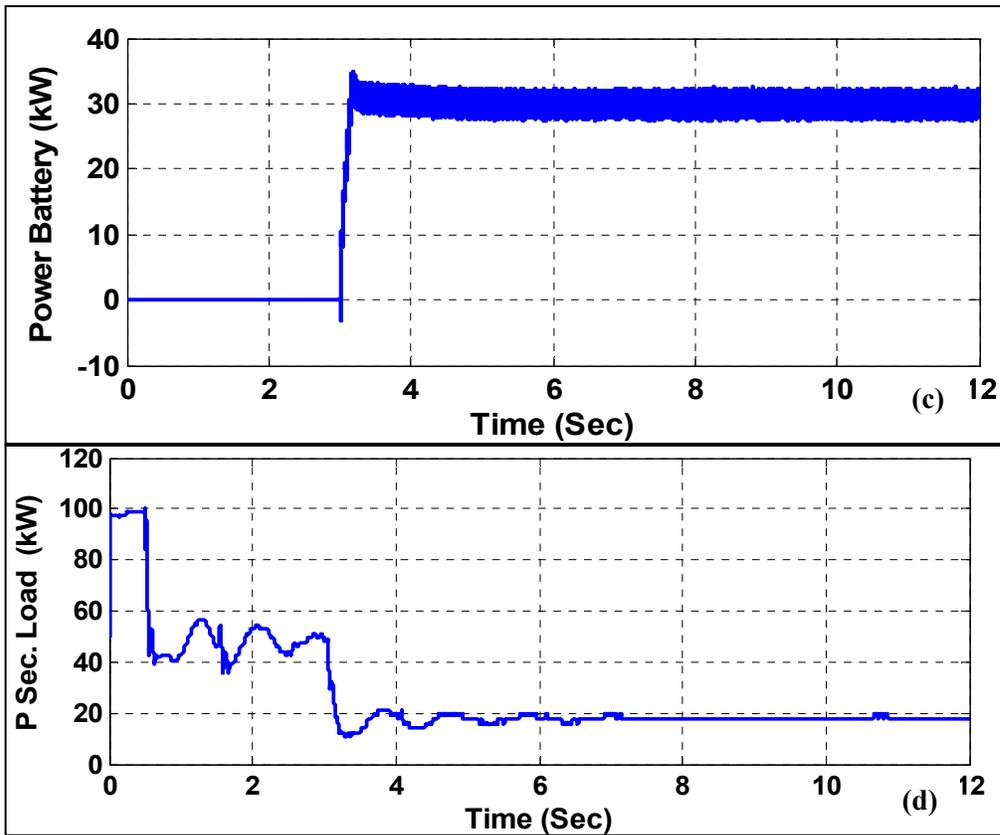


Figure 3.23 (c) Power from battery and (d) Power absorbed by Secondary load, using Fuzzy logic controller

Figure 3.24 (a) shows, State of charge (SOC) of battery (50%), where battery is charging at 3s. Until end of simulation the battery is charged 47.9% to 48.02%. Figure 3.24 (b) shows, the battery current situation. Before 3s, the current of battery was zero. But after 3s, battery has -200 A to charge itself at a rate of 30kW. Figure 3.24 (c) shows, the voltage is increasing at 3s and remain 262 V until end of simulation.

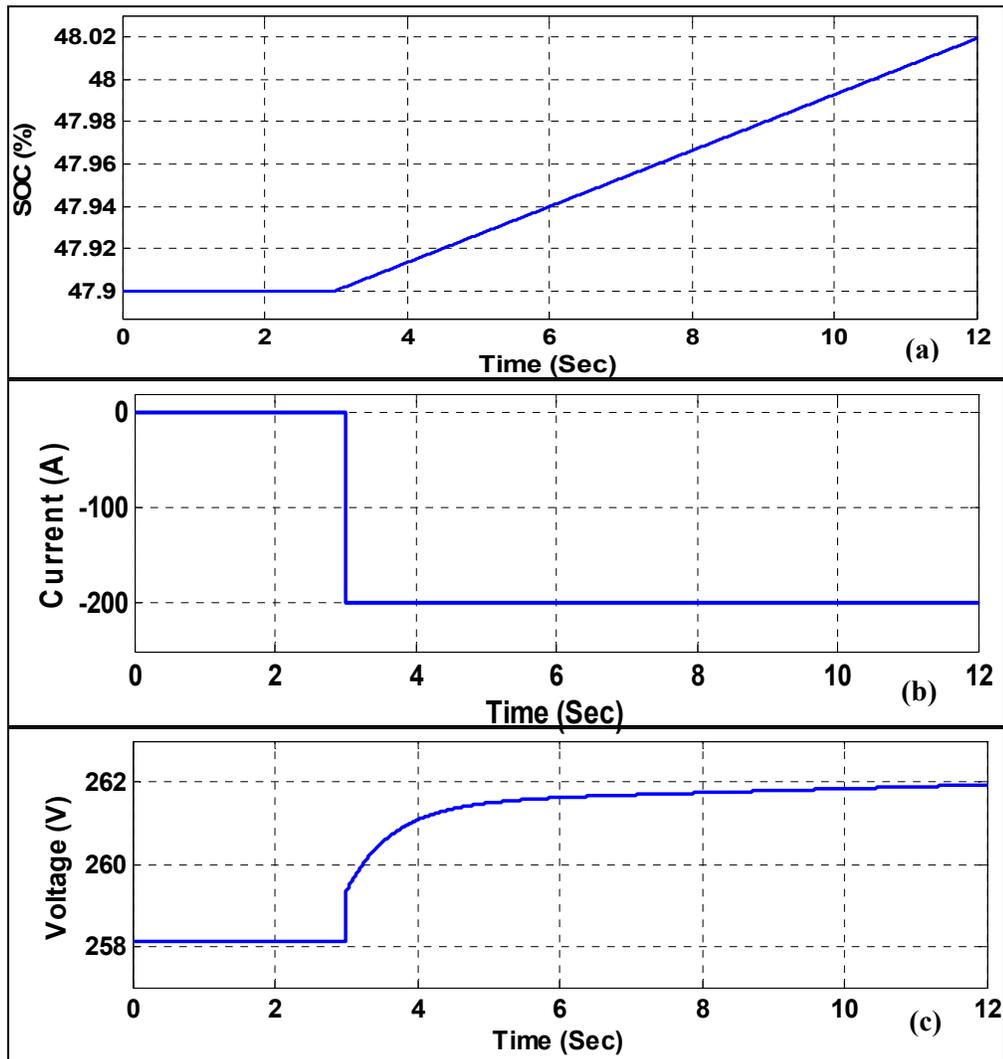


Figure 3.24 (a) State of charge (SOC) of battery, (b) Current in the battery and (c) Voltage in the battery, when battery is charging

To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). Finally, the frequency error and derivative of frequency error signal are applied to the fuzzy logic controller to generate an output signal to get the required secondary load power. The simulation has been run for 12s.

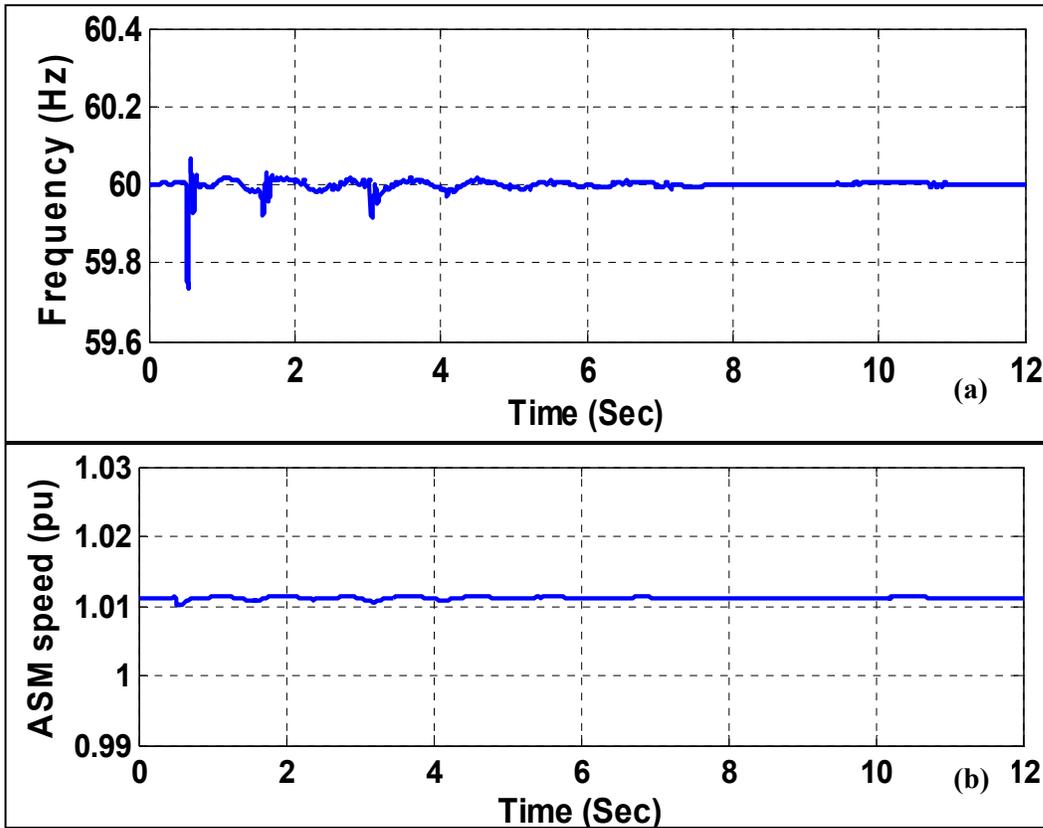


Figure 3.25 (a) Frequency at load bus and (b) Speed generated by asynchronous generator, using Fuzzy logic controller

Figure 3.25 (a) shows, after 12s simulation, the frequency drops to 59.72 Hz at 0.5s due to extra load of 50kW. At 3s battery is started to charge (rate of 30kW) and for that reason frequency drops to 59.92 Hz. Figure 3.25 (b) shows, the speed of the asynchronous machine is above (1.011 pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when turbine runs at 10 m/s wind speed. Due to some asynchronous machine losses, the wind turbine generates 200 kW.

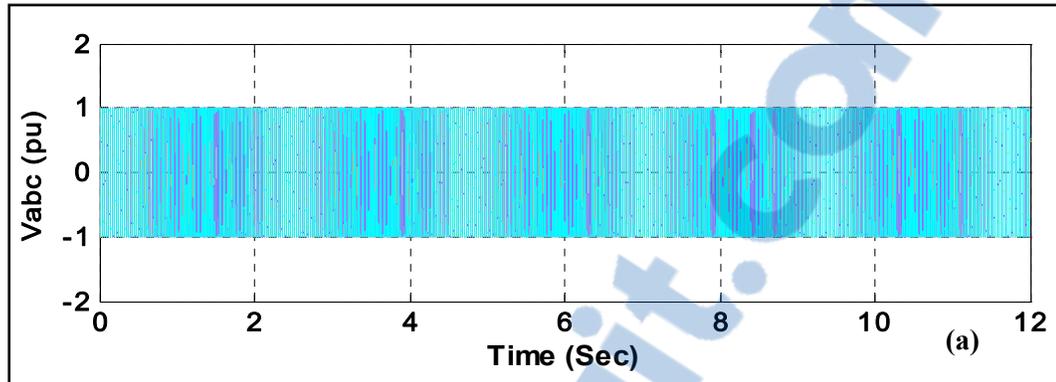


Figure 3.26 (a) Voltage at load bus, using Fuzzy logic controller

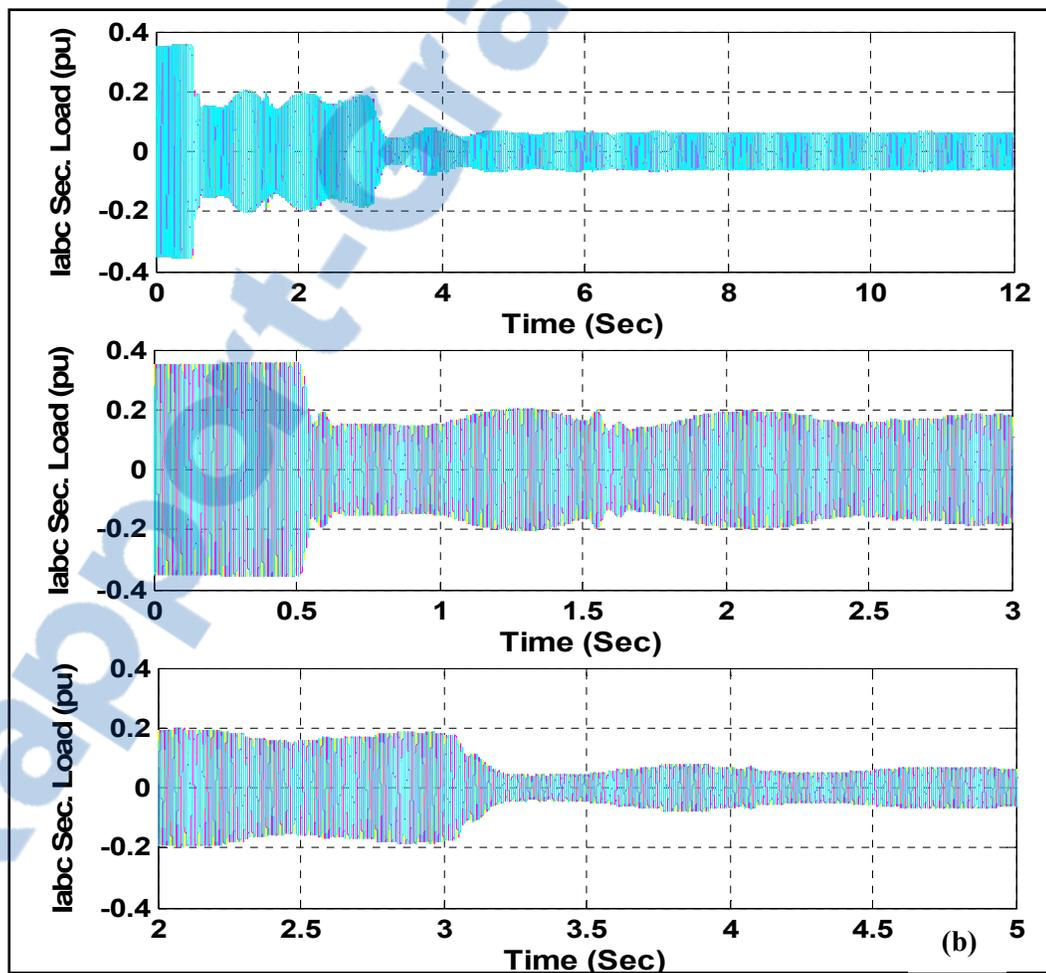


Figure 3.26 (b) Current at secondary loads, using Fuzzy logic controller

Figure 3.26 (a) shows, load voltage remains at 1 (pu) and no flicker is seen. Figure 3.26 (b) shows, the secondary load current decrease at 0.5s due to extra load of 50kW and at 3s due to charging condition of battery (rate of 30kW). Current remain 0.1 (pu) until end of simulation. To see more visible we took data from 0s to 3s and 2s to 5s.

### 3.6.3 Comparison between PID and fuzzy logic controller to control the frequency, when ( $P_T > P_L$ ) where, $P_S$ is charged

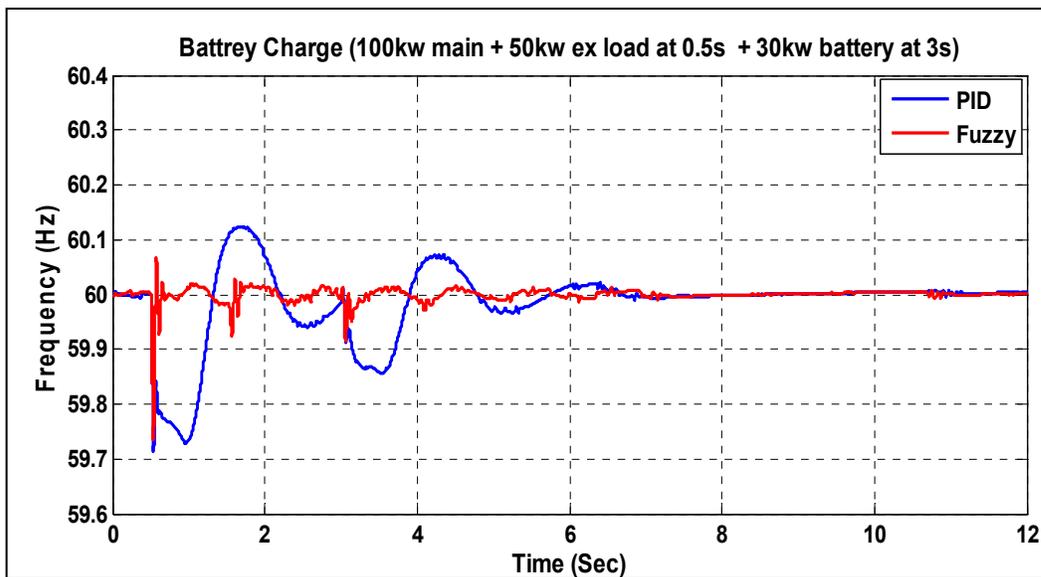


Figure 3.27 Fluctuation observations of frequency compare between PID controller and Fuzzy logic controllers when battery is charging

From figure 3.27, we observed that the fluctuation behavior of frequency with PID controller is higher than a fuzzy logic controller. The convergence time with fuzzy controller is also faster than PID controller. In PID, frequency drops 59.68 Hz at 0.5s due to extra load of 50kW and drops 59.82 Hz at 3s due to battery charging condition. But using fuzzy logic controller, frequency drops 59.72 Hz at 0.5s due to extra load of 50kW and drops 59.92 Hz at 3s due to battery charging condition. Using PID, fluctuation of frequency transient time is from 0s to 7s while in the Fuzzy logic controller it is from 0s to 3s. So, it is clear from above

graphs that the frequency takes more time to become stable in PID rather than fuzzy logic controller.

In scenario 2, we observed that the power produce from wind turbine is 200kW. Total consumer load is 150kW (100kW as a main load and 50kW are added at 0.5s of simulation) and battery is charged at 3s with rate of 30kW. So, 20kW absorbed by secondary/dump load (DL) to regulate the network frequency (in this power system, secondary/dump load should have some rooms to control the frequency. i.e. DL cannot be zero).

### 3.7 Simulation: Scenario 3

#### 3.7.1 Frequency control by PID, When ( $P_T < P_L$ ) where, $P_S$ is discharged

The wind speed (10 m/s) is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 3.28 (a). Figure 3.28 (b) shows, the consumer (main) load is 100 kW. At 0.5s, 3s and 7.5s an extra load of 50kW, 30kW and 50kW has been added respectively. So, the total load in the system is 230kW. Figure 3.28 (c) shows, the battery is discharging (rate of 50 kW) at 4.5s. Therefore, the secondary load absorbs 20 kW to regulate a 60 Hz frequency shown in figure 3.28 (d).

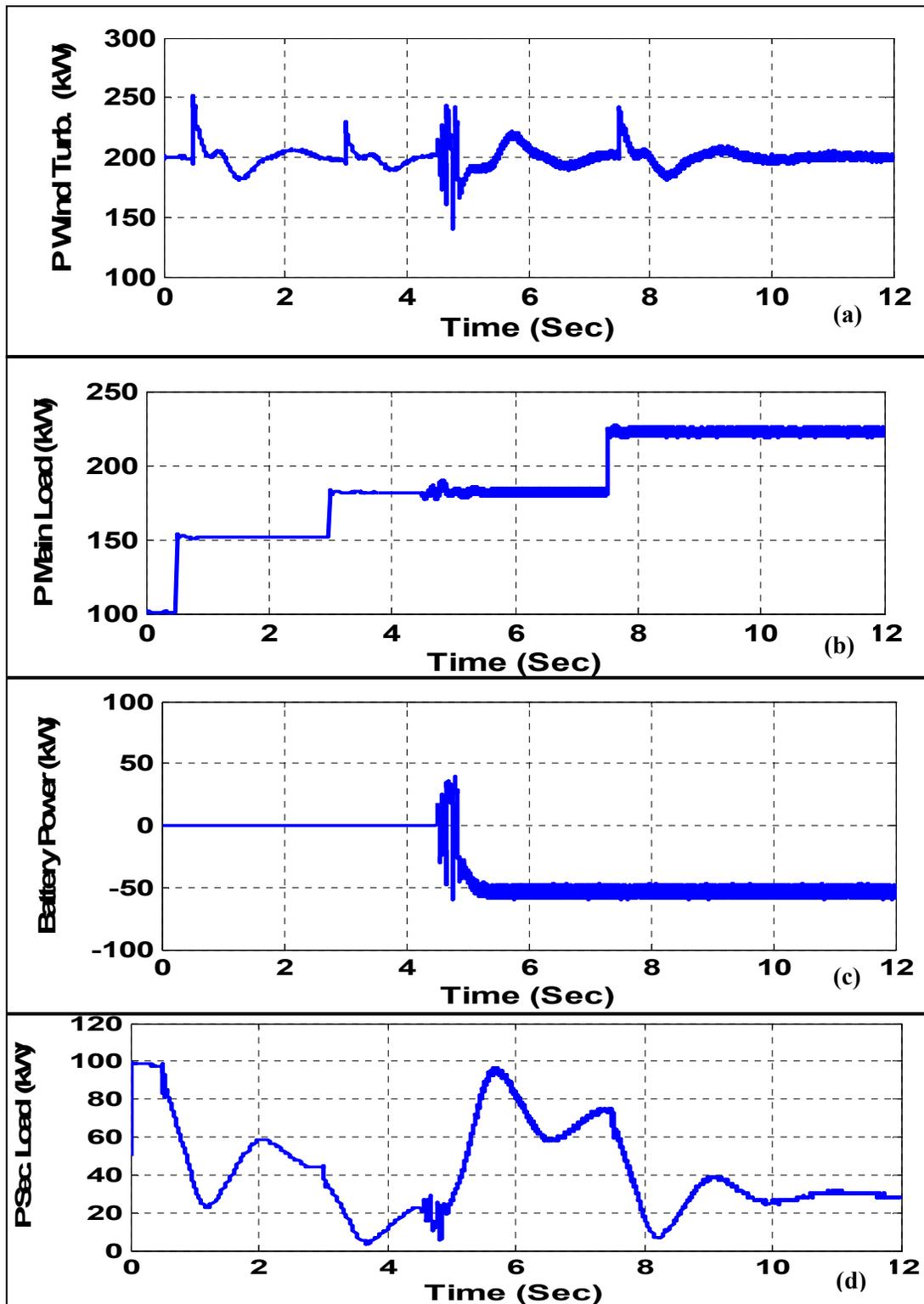


Figure 3.28 (a) Power from wind turbine, (b) Power absorbed by main load, (c) Power from battery and (d) Power absorbed by secondary load, using PID controller

Figure 3.29 (a) shows, State of charge (SOC) of battery (50%), where battery is discharging at 4.5s. Until end of simulation the battery is discharged 47.90% to 47.80%. Figure 3.29 (b) shows, the battery current situation. Before 4.5s, the current of battery was zero. But after 4.5s, battery has 200 A to discharge itself with a rate of 50kW. Figure 3.29 (c) shows, the voltage is decreasing at 4.5s and remain 254 V until end of simulation.

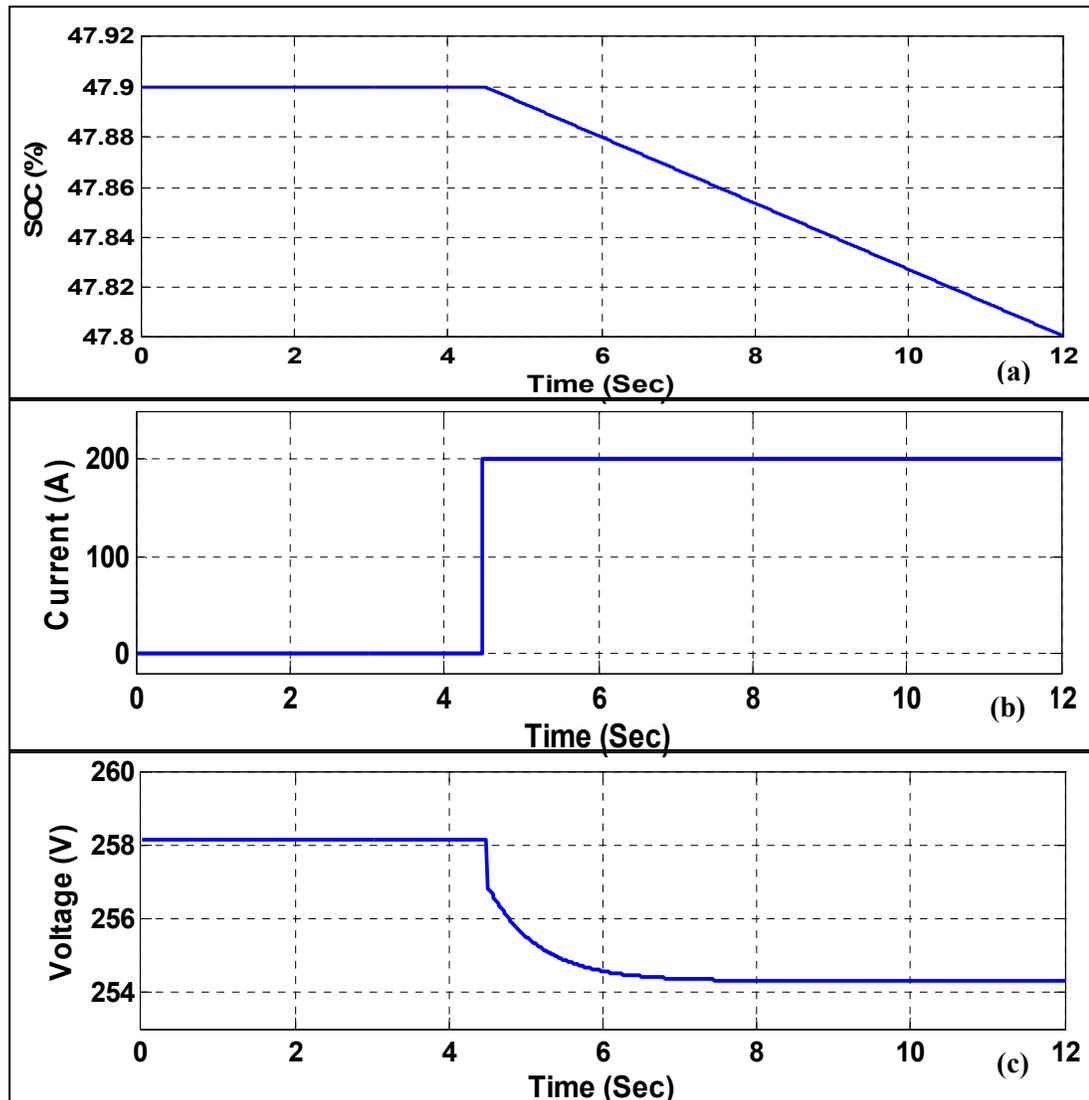


Figure 3.29 (a) State of charge (SOC) of battery, (b) Current in the battery and (c) Voltage in the battery, when battery is discharging

To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). The frequency error is then integrated to obtain a phase error. The phase error is applied to the Proportional-Derivative (PD) controller to generate an output signal to get the required secondary load power. Here the simulation has been run for 12s

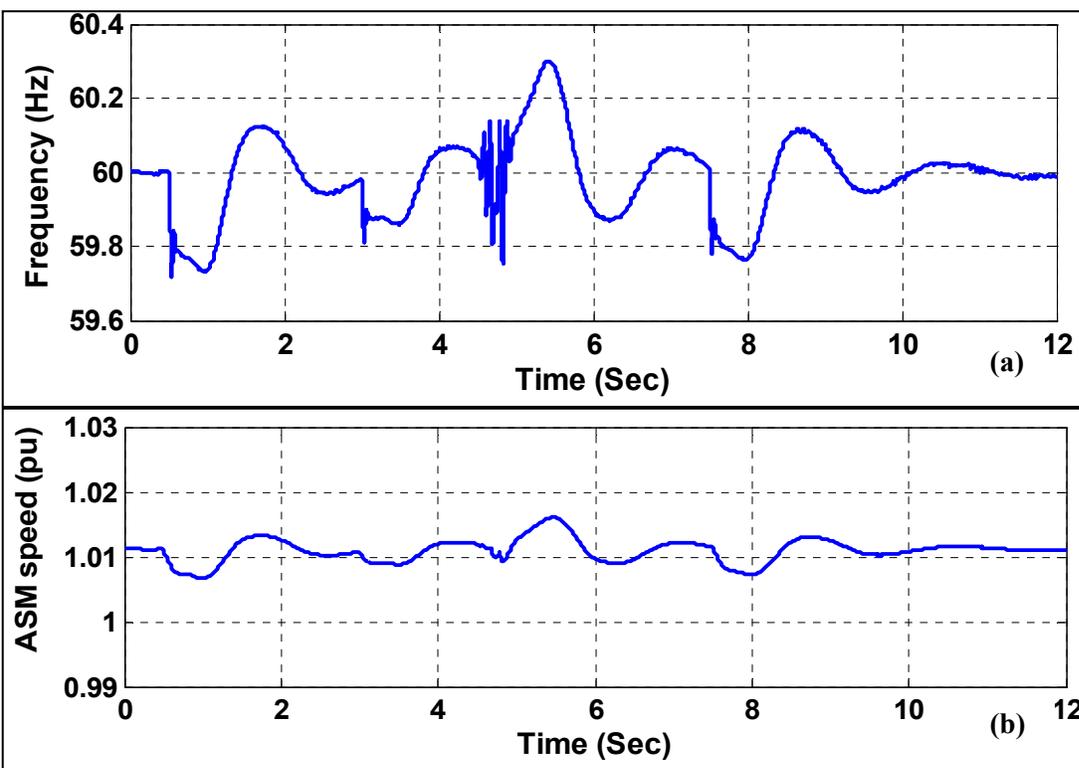


Figure 3.30 (a) Frequency at load bus and (b) Speed generated by asynchronous generator, using PID controller

Figure 3.30 (a) shows, after 12s simulation, the frequency drops to 59.68 Hz, 59.80Hz and 59.77 Hz at 0.5s, 3s and 7.5s due to extra load of 50kW, 30kW and 50kW respectively. At 4.5s battery is started to discharge (rate of 50kW) to maintain the high load demand and for that reason frequency drops to 59.75 Hz. Figure 3.30 (b) shows, the speed of the asynchronous machine is above (1.011 pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when

turbine runs at 10 m/s wind speed. Due to some asynchronous machine losses, the wind turbine generates 200 kW.

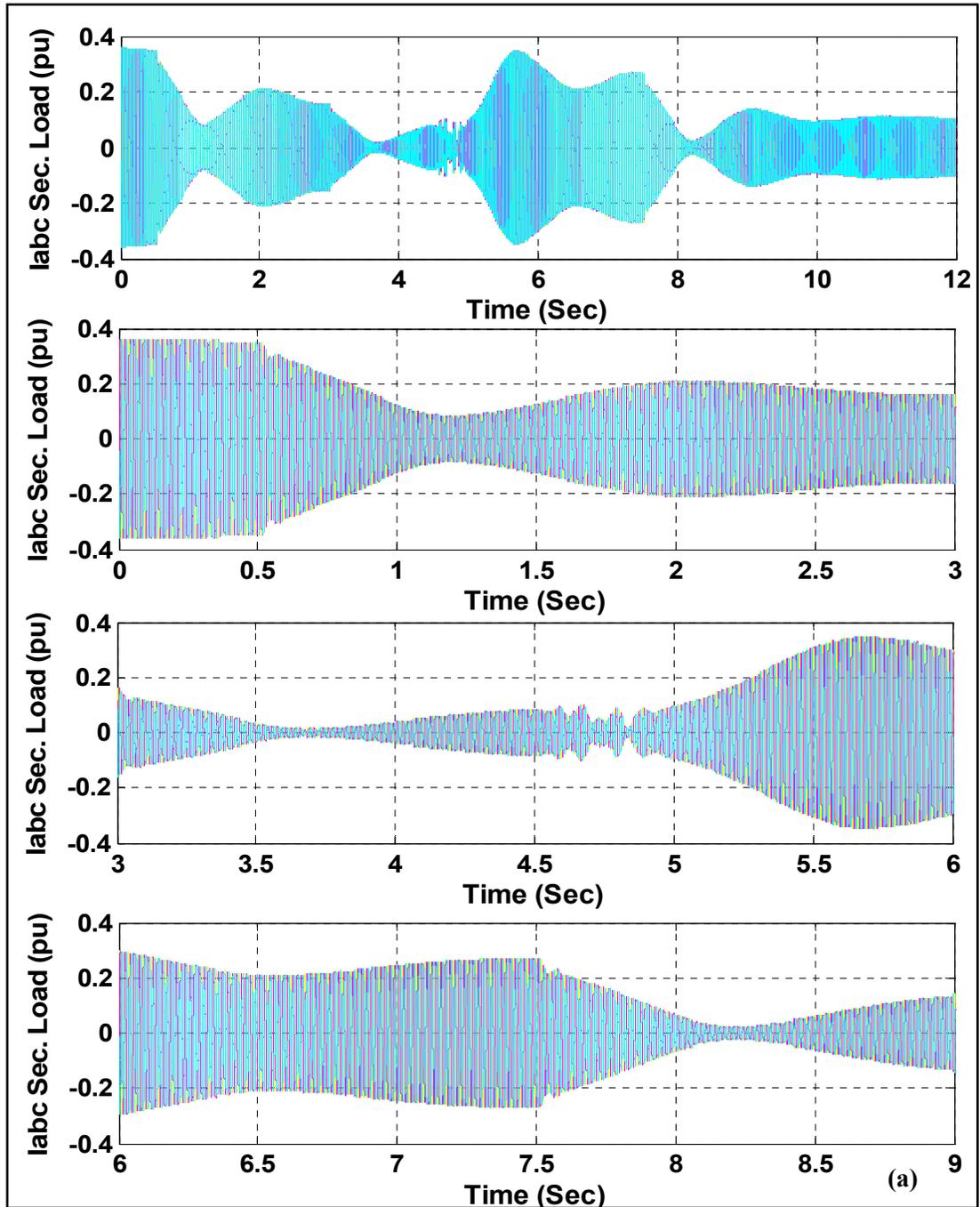


Figure 3.31 (a) Current at secondary loads, using PID controller

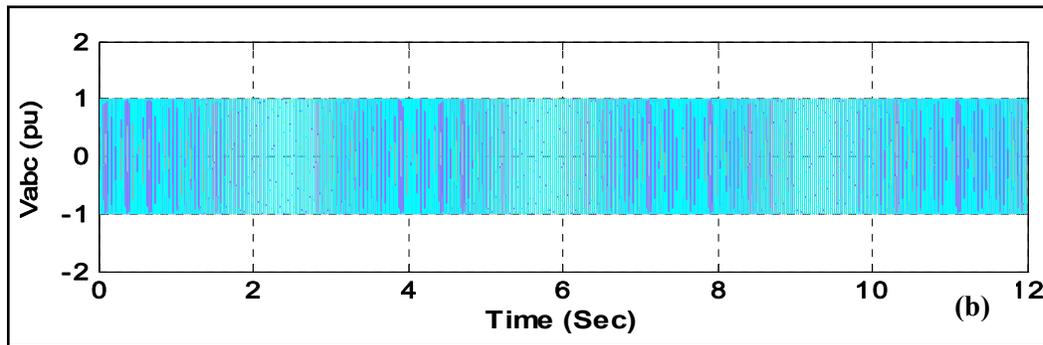


Figure 3.31 (b) Voltage at load bus, using PID controller

Figure 3.31 (a) shows, the secondary load current decrease at 0.5s, 3s and 7.5s due to extra load of 50kW, 30kW and 50kW respectively. At 4.5s current also decrease due to discharging condition of battery (rate of 50kW). Current remain 0.1 (pu) until end of simulation. To see more visible we took data from 0s to 3s, 3s to 6s and 6s to 9s. Figure 3.31 (b) shows, load voltage remains at 1 (pu) and no flicker is seen.

### 3.7.2 Frequency control using Fuzzy logic controller, When ( $P_T < P_L$ ) where, $P_S$ is discharged

Here, wind speed (10 m/s) is maintained in wind turbine to generate sufficient power to supply the load and the diesel generator is stopped. When synchronous machine mechanical power ( $P_m$ ) set at zero as an input, the synchronous machine runs as a synchronous condenser. Due to some asynchronous machine losses, the wind turbine generates 200 kW shown in figure 3.32 (a). Figure 3.32 (b) shows, the consumer (main) load is 100 kW. At 0.5s, 3s and 7.5s an extra load of 50kW, 30kW and 50kW has been added respectively. So, the total load in the system is 230kW. Figure 3.32 (c) shows, the battery is discharging (rate of 50 kW) at 4.5s. Therefore, the secondary load absorbs 20 kW to regulate a 60 Hz frequency shown in figure 3.32 (d).

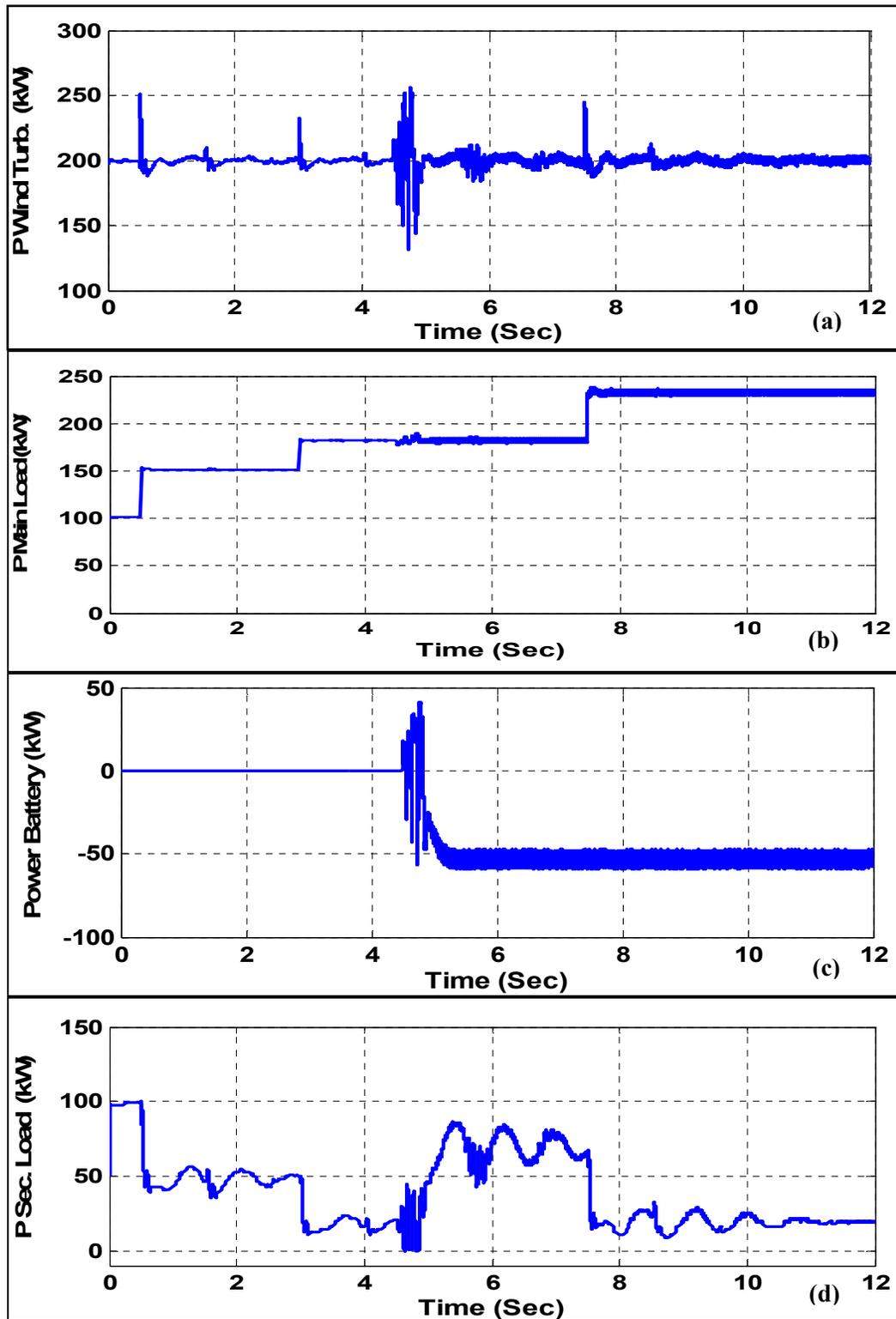


Figure 3.32 (a) Power from wind turbine, (b) Power absorbed by main load, (c) Power from battery and (d) Power absorbed by secondary load, using Fuzzy logic controller

Figure 3.33 (a) shows, State of charge (SOC) of battery (50%), where battery is discharging at 4.5s. Until end of simulation the battery is discharged 47.90% to 47.80%. Figure 3.33 (b) shows, the battery current situation. Before 4.5s, the current of battery was zero. But after 4.5s, battery has 200 A to discharge itself with a rate of 50kW. Figure 3.33 (c) shows, the voltage is decreasing at 4.5s and remain 254 V until end of simulation.

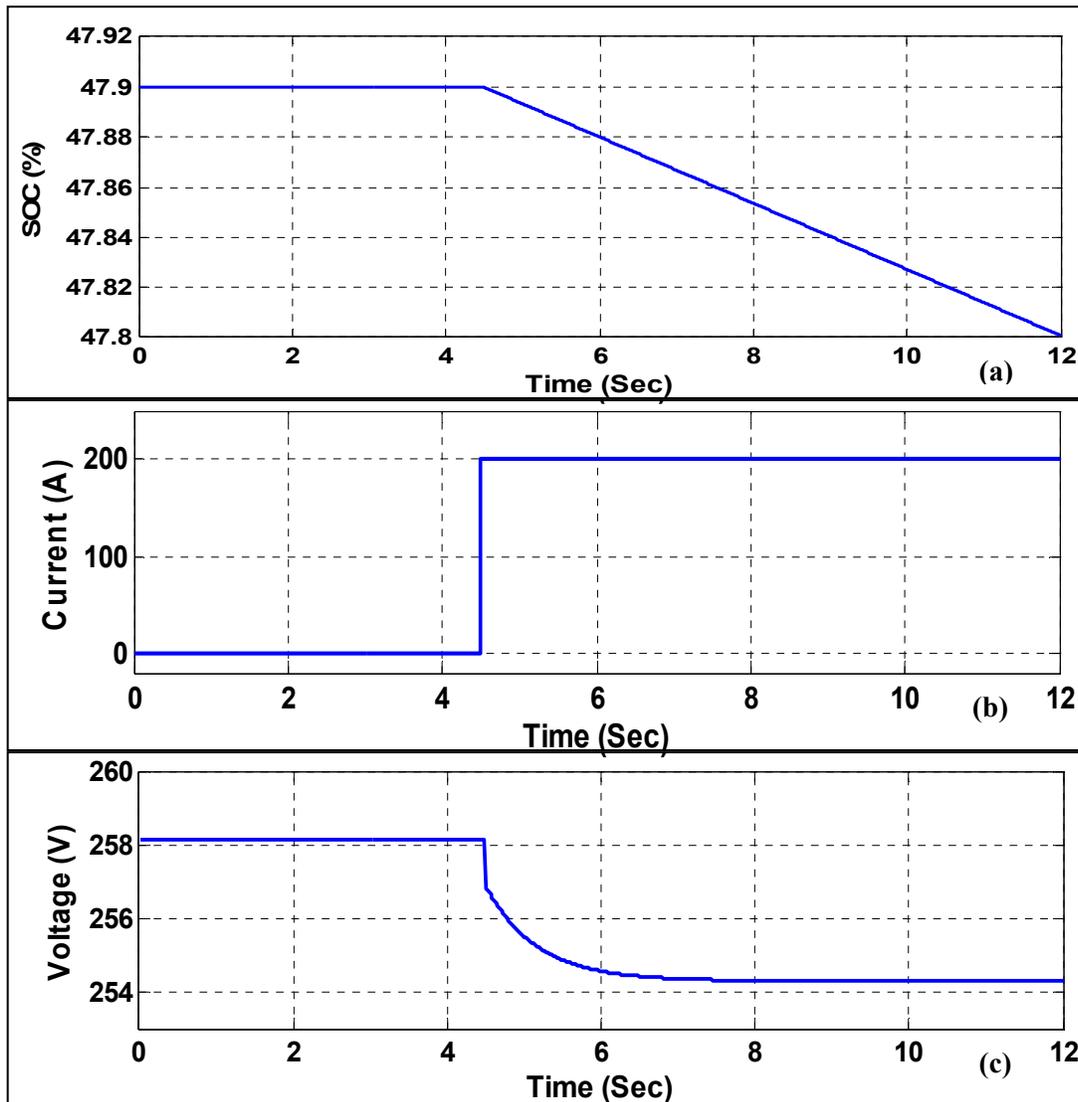


Figure 3.33 (a) State of charge (SOC) of battery, (b) Current in the battery and (c) Voltage in the battery, when battery is discharging

To measure the network frequency a three-phase Phase Locked Loop (PLL) system is used. As an input of PLL, the system voltage is applied. To get a frequency error, the network frequency is compared with the reference frequency (60 Hz). Finally, the frequency error and derivative of frequency error signal are applied to the fuzzy logic controller to generate an output signal to get the required secondary load power. The simulation has been run for 12s.

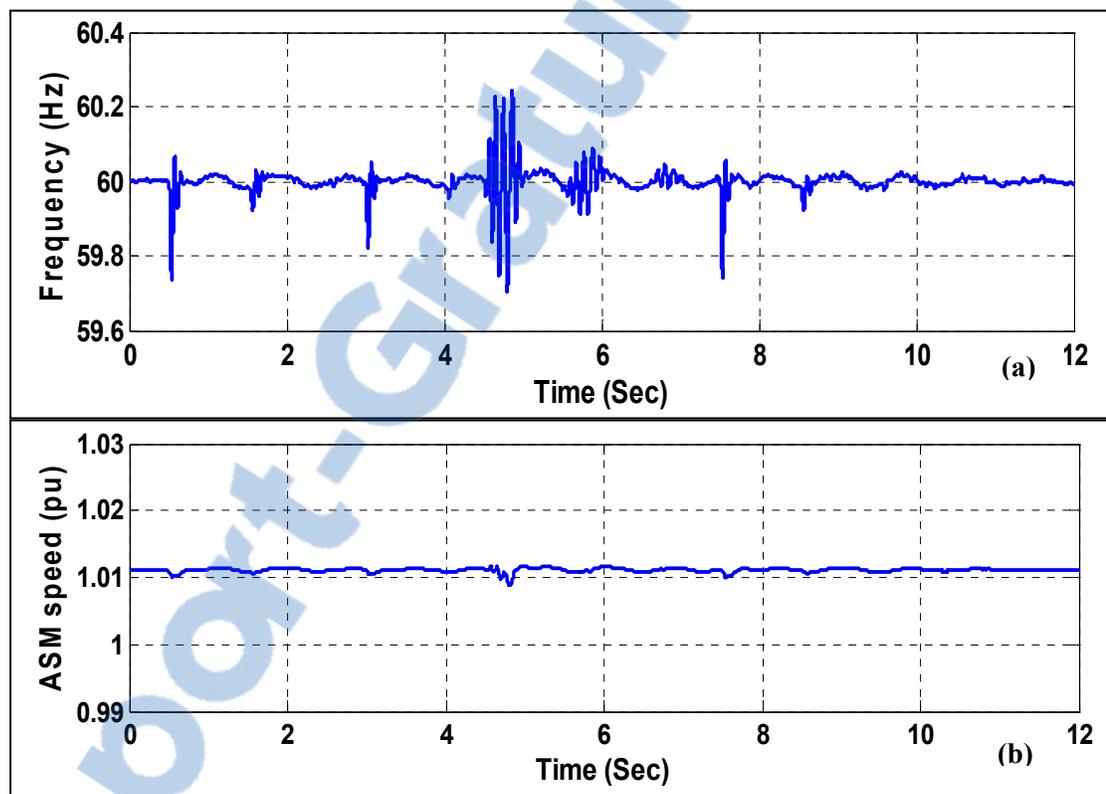


Figure 3.34 (a) Frequency at load bus and (b) Speed generated by asynchronous generator, using Fuzzy logic controller

Figure 3.34 (a) shows, after 12s simulation, the frequency drops to 59.72 Hz, 59.82 Hz and 59.78 Hz at 0.5s, 3s and 7.5s due to extra load of 50kW, 30kW and 50kW respectively. At 4.5s battery is started to discharge (rate of 50kW) to maintain the high load demand and for that reason frequency drops to 59.75 Hz. Figure 3.34 (b) shows, the speed of the asynchronous machine is above (1.011 pu) and it operates in generator mode. According to the characteristics of the turbine, we will receive output power 0.75 pu (206kW) when

turbine runs at 10 m/s wind speed. Due to some asynchronous machine losses, the wind turbine generates 200 kW.

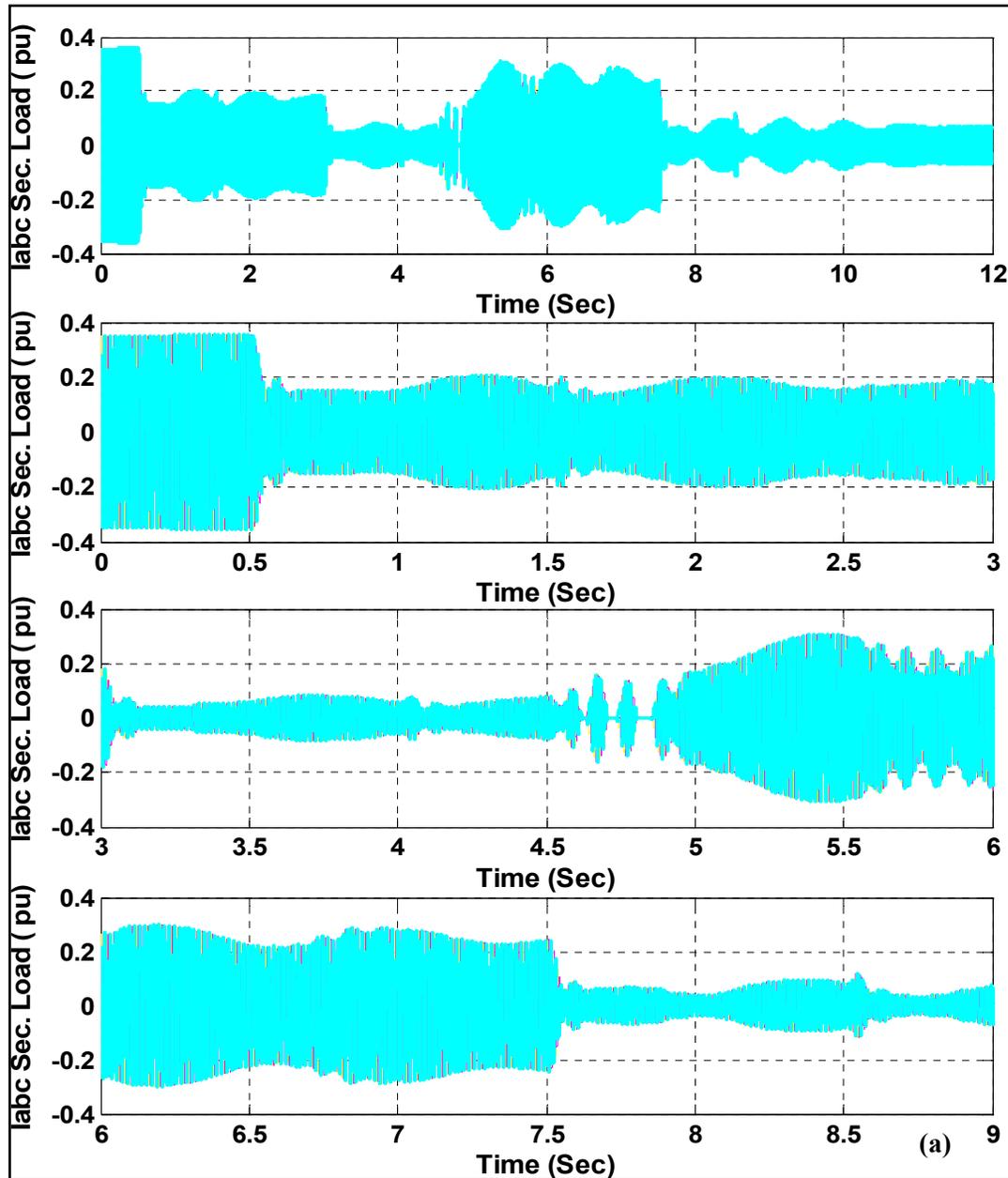


Figure 3.35 (a) Current at secondary loads, using Fuzzy logic controller

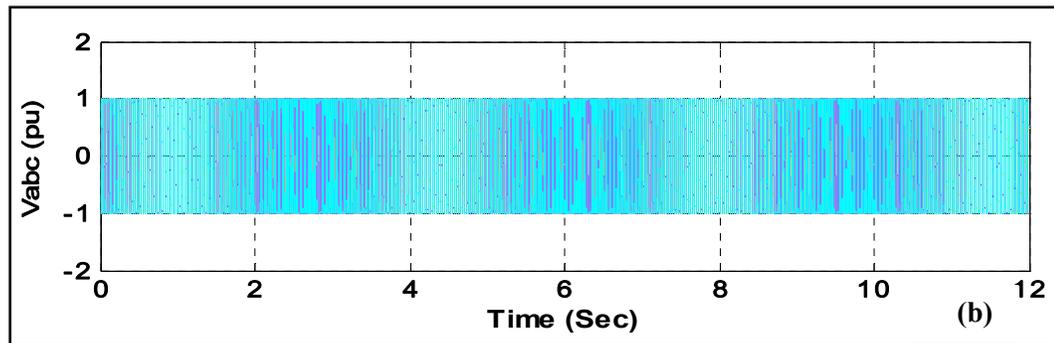


Figure 3.35 (b) Voltage at load bus, using Fuzzy logic controller

Figure 3.35 (a) shows, the secondary load current decrease at 0.5s, 3s and 7.5s due to extra load of 50kW, 30kW and 50kW respectively. At 4.5s current also decrease due to discharging condition of battery (rate of 50kW). Current remain 0.1 (pu) until end of simulation. To see more visible we took data from 0s to 3s, 3s to 6s and 6s to 9s. Figure 3.35 (b) shows, load voltage remains at 1 (pu) and no flicker is seen.

### 3.7.3 Comparison between PID and fuzzy logic controller to control the frequency, when ( $P_T < P_L$ ) where, $P_S$ is discharged

Finally, we observed (Figure 3.36) that the fluctuation behavior of frequency with PID controller is higher than a fuzzy logic controller. The convergence time with fuzzy controller is also faster than PID controller. In PID, frequency drops to 59.68 Hz, 59.80Hz and 59.77Hz at 0.5s, 3s and 7.5s due to extra load of 50kW, 30kW and 50kW respectively and drops 59.75 Hz at 4.5s due to battery discharging condition. But using fuzzy logic controller, frequency drops to 59.72 Hz, 59.82 Hz and 59.78 Hz at 0.5s, 3s and 7.5s due to extra load of 50kW, 30kW and 50kW respectively and drops 59.75 Hz at 4.5s due to battery discharging condition. Using PID, fluctuation of frequency transient time is from 0s to 11s while in the Fuzzy logic controller it is from 4.5s to 7s only. So, it is clear from above graphs that the frequency takes more time to become stable in PID rather than fuzzy logic controller.

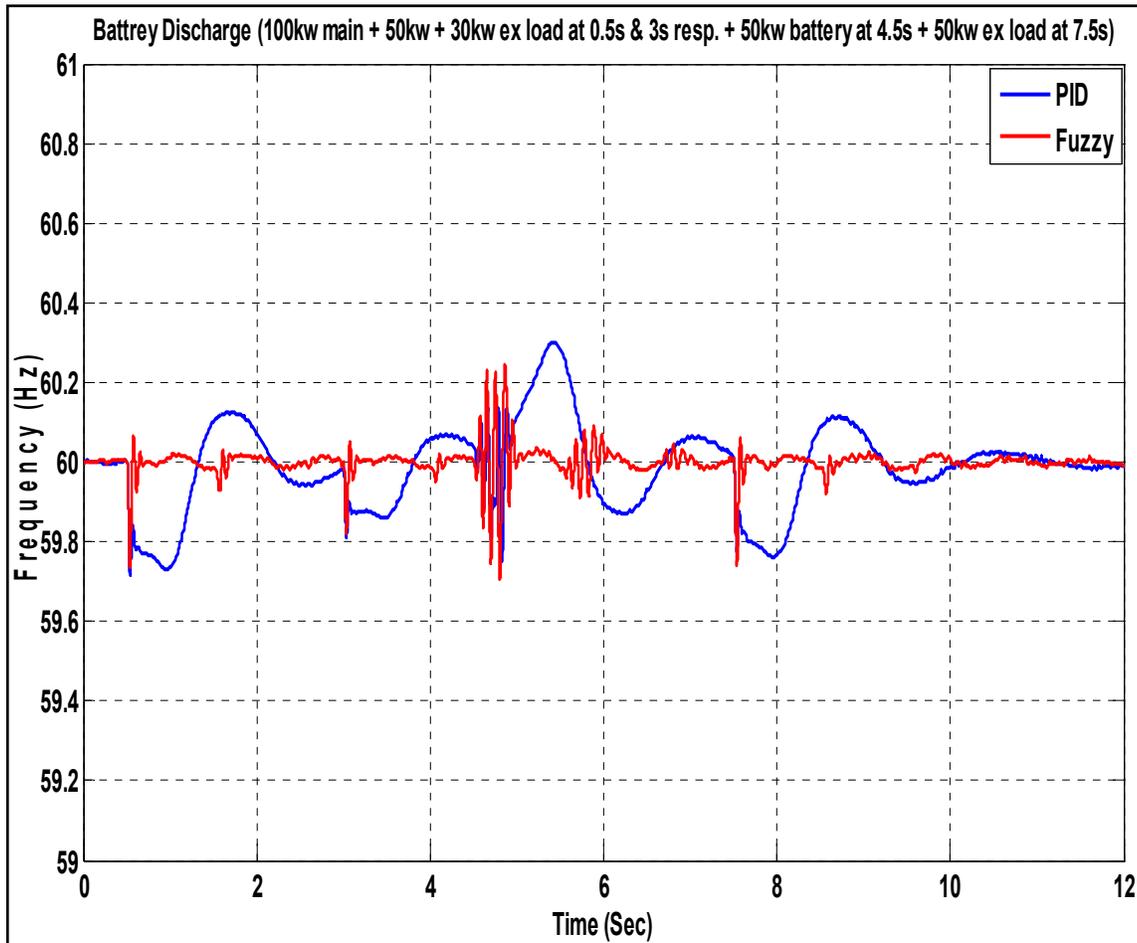


Figure 3.36 Fluctuation observations of frequency compare between PID controller and Fuzzy logic controllers when battery is discharging

In scenario 3, we observed that the power produce from wind turbine is 200kW. The total consumer load is 230kW (100kW as a main load and 50kW, 30kW and 50kW are added at 0.5s, 3s and 7.5s respectively of simulation). Therefore, battery is discharged at 4.5s with rate of 50kW to maintain the high load demand. Here, 20kW absorbed by secondary/dump load (DL) to regulate the network frequency (in this power system, secondary/dump load should have some rooms to control the frequency. i.e. DL cannot be zero).

## CONCLUSION

In this thesis, the technology of DG and the fluctuation behavior of frequency in the presence of wind turbine are identified and simulated. The methods of frequency control were briefly presented, as well as the inputs acquired by the energy storage use by increasing the penetration rate of the wind turbine.

The WO mode frequency control system presented in this thesis which consists of four nodes: the first is used to measure the speed of the SM shaft, followed by a PID controller generating a control signal  $P_{REF}$ . The second node is connected to the consumer load. Other two nodes are respectively the energy storage system and the DL. Storage system is charged and discharged according to the situation of the power system. The performance of the PID and fuzzy logic control system has been tested by simulation.

However, for low wind power, the frequency control is performed by the battery only (BESS). The fluctuation behavior of frequency in the load bus is observed using both PID and fuzzy logic control. In addition, we also observed the fuzzy logic controller gives us more performing frequency (less transient time) compared to the PID controller. Here, the response of battery, dependent on its dynamics, can be slow (depending on the technology used) and can generate a large variation in frequency. The simulation was done in chapter 03 with to show the variation of extra load to see the frequency stability with both controllers (PID and Fuzzy logic). Globally, fuzzy logic control has shown better performance than PID control.



## **RECOMMENDATIONS**

To improve the system's operation, the WD (wind-diesel) mode is necessary to share the load supply with the battery especially when the wind speed drops or the load increases. Also, the battery selection for applications is highly important in order to overcome the problems of dynamic instability of the electrical network based on such an energy storage system. As well, filters play a very important role in reducing the harmonics generated by the power electronics converter. For the future works, a larger power network could be developed using same technologies. To get more flexible results, fuzzy logic rules could be modified. The capacity of the battery could be increased with respect to the network load demand.



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