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# Nomenclature and Abbreviations as used by the Author

| Term                   | Abbreviation | Explanation  |
|------------------------|--------------|--|
| Hydrotalcite           | HT           | The layered double hydroxide of                            |
|                        |              | composition $Mg_6AI_2(OH)_{16}CO_3.4H_2O$ .                |
| Layered double         | LDH          | Anionic clay minerals consisting of                        |
| hydroxide              |              | $Mg(OH)_2$ like layers which contains both                 |
|                        |              | divalent and trivalent cations in different                |
|                        |              | ratios.  |
| Interlayer             |              | The region between the two hydroxide                       |
|                        |              | layers in which the charge balancing                       |
|                        |              | anions and crystal water lie.                              |
| Sand-rose morphology   |              | Particles consisting of many intergrown                    |
|                        |              | smaller particulates which reduce the                      |
|                        |              | surface area.  |
| Intercalation          |              | Process in which atoms, ions or                            |
|                        |              | molecules are trapped between layers in                    |
|                        |              | a crystal lattice without the formation of                 |
|                        |              | a formal chemical bond [1].                                |
| Intercalate (verb)     |              | Diffusion of atoms, ions or molecules                      |
|                        |              | into the interlayer region of a layered                    |
|                        |              | compound.  |
| Intercalate (noun) or  |              | A compound in which atoms, ions or                         |
| Intercalation compound |              | molecules are trapped between layers in                    |
|                        |              | a crystal lattice [1].                                     |
| Adsorption             |              | Formation of (a) layer(s) of gaseous,                      |
|                        |              | liquid or solid molecules on the surface                   |
|                        |              | of a molecule, held by chemical or                         |
|                        |              | physical forces [1].                                       |
| Stearic acid           | SA           | A solid saturated fatty acid,                              |
|                        |              | CH <sub>3</sub> (CH <sub>2</sub> ) <sub>16</sub> COOH [1]. |
| Carboxylic acid        |              | Organic compounds containing the                           |
|                        |              | group –COOH [1].   |



| Fatty acid              | FA                  | An organic compound consisting of a        |
|-------------------------|---------------------|--|
|                         |                     | hydrocarbon chain and a terminal           |
|                         |                     | carboxyl group [1].                        |
| lon exchange            |                     | The exchange of ions of the same           |
|                         |                     | charge between a solution and a solid in   |
|                         |                     | contact with it [1].                       |
| Anionic exchange        | AEC                 | The amount of exchangeable anions          |
| capacity                |                     | available within the crystal structure of  |
|                         |                     | an adsorbent material, expressed in        |
|                         |                     | mmol/g or mmol/100 g adsorbent.            |
| Brønsted acid/base      |                     | A Brønsted-Lowry acid is a substance       |
|                         |                     | that donates a proton and a Brønsted-      |
|                         |                     | Lowry base is a substance that accepts     |
|                         |                     | a proton [2].                              |
| Lewis acid/base         |                     | A Lewis acid is a substance that accepts   |
|                         |                     | an electron pair, and a Lewis base is a    |
|                         |                     | substance that donates an electron pair    |
|                         |                     | [2].                                       |
| Carbonate layered       | LDH-CO <sub>3</sub> | A layered double hydroxide into which      |
| double hydroxide        |                     | the carbonate anion has intercalated.      |
| Chloride layered double | LDH-CI              | A layered double hydroxide into which      |
| hydroxide               |                     | the chloride anion has intercalated.       |
| Stearate layered double | LDH-SA              | A layered double hydroxide into which      |
| hydroxide               |                     | the stearate anion has intercalated.       |
| Emulsion                |                     | A kinetically stable dispersion of two     |
|                         |                     | immiscible liquids, stabilized by the      |
|                         |                     | presence of a surfactant at the interface. |
| Emulsifier              |                     | A surfactant that resides at the interface |
|                         |                     | of two immiscible liquids in order to      |
|                         |                     | stabilize the mixture of the two liquids.  |

| Micro-emulsion         |     | A thermodynamically stable mixture of<br>two immiscible liquids, stabilized by a<br>high concentration of surfactant and a<br>co-surfactant.  |
|------------------------|-----|---|
| Surfactant             |     | Molecules with both hydrophilic and   |
|                        |     | hydrophobic parts.  |
| Sodium dodecyl sulfate | SDS | An anionic surfactant, CH <sub>3</sub> (CH <sub>2</sub> ) <sub>11</sub> SO <sub>4</sub> Na  |
| Calcine                |     | Heat a substance to an elevated<br>temperature to facilitate a reaction, for<br>example decomposition reaction. In the<br>case of the LDHs used in this study, the<br>calcination facilitates the dehydration,<br>decarbonation and dehydroxilation |
|                        |     | reactions which can collectively be   |
|                        |     | described as decomposition reactions.   |
| Reconstruction         |     | Rehydration of a calcined LDH in the  |
|                        |     | presence of an aqueous solution of an   |
|                        |     | anion.  |
| Layered double oxide   | LDO | Calcined LDH.   |
| Poly(sodium            | PVS | The sodium salt of a polymer consisting   |
| vinylsulfonate)        |     | of vinyl sulfonic acid monomeric units.   |
| Polyanion or anionic   |     | A polymer consisting of anionic   |
| polymer                |     | (negatively charged) monomeric units.   |
| Polyelectrolyte        |     | A polymer consisting of positively or negatively charged monomers   |
| Cross linkage          |     | A short side chain of atoms (or a charged moiety) linking two longer chains in a polymeric material [1].  |
| Sodium alginate        |     | The sodium salt of alginic acid, a polysaccharide occurring in the cell walls of brown algae [1].   |



| Dextrin            | An intermediate polysaccharide resulting from the hydrolysis of starch by amylase enzymes or acids [1].                                       |
|--------------------|---|
| Polysaccharide     | Polymers consisting of long chains of<br>monosaccharide(simple-sugar)molecules [1].   |
| Plasticizer        | Materials incorporated into plastic resins<br>to change workability, flexibility, flow and<br>impact resistance [3], for example<br>glycerol. |
| Glycerol           | 1,2,3-trihydroxypropane, used as a plasticizer in thermoplastic starch [3].   |
| Defoamer           | A substance (usually petroleum oil based) that prevents a surfactant from creating foam in a mixture.   |
| Filler             | Solid inert material added to a polymeric<br>matrix to change its physical properties<br>or to dilute it for economy [1].                     |
| Composite material | A material consisting of two or more substances.  |
| Nanocomposite      | A composite material in which one of the constituents have at least one dimension which is lower than 100 nm.                                 |
| Foliate            | With regard to polymer chains or layered<br>compounds, whereby polymer chains<br>line up or the individual layers are<br>stacked together.    |
| Exfoliate          | Polymer chains or individual inorganic<br>layers that are dispersed randomly<br>within a composite.   |

| are pushed apart into a random pattern.   Viscosity A measure of the resistance to flow that   a fluid offers when it is subjected to shear stress [1].   Water vapour WVP   The mass of water vapour that moves permeability   through a film of certain thickness per unit time, unit area and unit difference in water vapour pressure.   Young's modulus Synonym for the modulus of elasticity, namely the ratio of the unit stress to the unit strain [4].   Tensile strength Synonym for ultimate strength, namely the maximum ordinate to the stress-strain curve [4].   Percentage strain The increase in length of the gage after (elongation) at break   Retrogradation A process which happens during the ageing of starch in which the starch chains lose water and form intermolecular hydrogen bonds.   Crystalline Used to indicate that a chemical species has long-range structure.   Amorphous Used to indicate that a chemical species does not have long-range structure.   X-ray diffraction XRD Diffraction of X-rays by a crystal due to the comparable size of the wavelengths of X-rays and the distances between atoms in crystals [1].   | Exfoliation           |     | Process whereby polymer chains that were aligned or stacked inorganic layers |  |
|---|-----------------------|-----|--|--|
| Viscosity A measure of the resistance to flow that   a fluid offers when it is subjected to shear stress [1].   Water vapour WVP   The mass of water vapour that moves permeability   through a film of certain thickness per unit time, unit area and unit difference in water vapour pressure.   Young's modulus Synonym for the modulus of elasticity, namely the ratio of the unit stress to the unit strain [4].   Tensile strength Synonym for ultimate strength, namely the maximum ordinate to the stress-strain curve [4].   Percentage strain The increase in length of the gage after (elongation) at break   Retrogradation A process which happens during the ageing of starch in which the starch chains lose water and form intermolecular hydrogen bonds.   Crystalline Used to indicate that a chemical species has long-range structure.   Amorphous Used to indicate that a chemical species does not have long-range structure.   X-ray diffraction XRD Diffraction of X-rays by a crystal due to the comparable size of the wavelengths of X-rays and the distances between atoms in crystals [1].   |                       |     | are pushed apart into a random pattern.                                      |  |
| a fluid offers when it is subjected to<br>shear stress [1].   Water vapour WVP   The mass of water vapour that moves<br>permeability   through a film of certain thickness per<br>unit time, unit area and unit difference in<br>water vapour pressure.   Young's modulus Synonym for the modulus of elasticity,<br>namely the ratio of the unit stress to the<br>unit strain [4].   Tensile strength Synonym for ultimate strength, namely<br>the maximum ordinate to the stress-<br>strain curve [4].   Percentage strain The increase in length of the gage after<br>fracture divided by the initial gage length<br>and multiplied by 100 [4].   Retrogradation A process which happens during the<br>ageing of starch in which the starch<br>chains lose water and form<br>intermolecular hydrogen bonds.   Crystalline Used to indicate that a chemical species<br>has long-range structure.   Amorphous Used to indicate that a chemical species<br>does not have long-range structure. This<br>does, however, not preclude the<br>existence of short-range structure.   X-ray diffraction XRD Diffraction of X-rays by a crystal due to<br>the comparable size of the wavelengths<br>of X-rays and the distances between<br>atoms in crystals [1]. | Viscosity             |     | A measure of the resistance to flow that                                     |  |
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| X-ray diffraction XRD Diffraction of X-rays by a crystal due to<br>the comparable size of the wavelengths<br>of X-rays and the distances between<br>atoms in crystals [1].  |                       |     | existence of short-range structure.  |  |
| the comparable size of the wavelengths<br>of X-rays and the distances between<br>atoms in crystals [1].   | X-ray diffraction     | XRD | Diffraction of X-rays by a crystal due to                                    |  |
| of X-rays and the distances between atoms in crystals [1].  |                       |     | the comparable size of the wavelengths                                       |  |
| atoms in crystals [1].  |                       |     | of X-rays and the distances between  |  |
|   |                       |     | atoms in crystals [1].   |  |

| X-ray fluorescence    | XRF  | The emission of X-rays from excited          |
|-----------------------|------|--|
|                       |      | atoms produced by the impact of high-        |
|                       |      | energy electrons, particles or a primary     |
|                       |      | beam of X-rays. The wavelengths of the       |
|                       |      | fluorescent X-rays are measured by an        |
|                       |      | X-ray spectrometer as a means of             |
|                       |      | chemical analysis [1].                       |
| Scanning electron     | SEM  | A beam of primary electrons scans the        |
| microscopy            |      | specimen surface and those that are          |
|                       |      | reflected, together with secondary           |
|                       |      | electrons emitted, are collected to form a   |
|                       |      | visual image [1].                            |
| Transmission electron | TEM  | A sharply focused electron beam passes       |
| microscopy            |      | through a thin section of metal-coated       |
|                       |      | specimen onto a fluorescent screen to        |
|                       |      | form a visual image [1].                     |
| Freeze drying         |      | A process used to dehydrate heat             |
|                       |      | sensitive substances whereby the             |
|                       |      | product is deep-frozen and the ice is        |
|                       |      | sublimed by reducing the pressure [1].       |
| Freeze fracturing     |      | A process whereby a material is              |
|                       |      | embrittled by freezing it in liquid nitrogen |
|                       |      | and broken to obtain a clean surface         |
|                       |      | without smearing.                            |
| Microscopic structure |      | The shape of a particle as observed with     |
|                       |      | a microscope, using either an optical or     |
|                       |      | an electron microscope.                      |
| Fourier Transform     | FTIR | Fourier transformations are done on          |
| infrared spectroscopy |      | infrared spectroscopic data by a             |
|                       |      | computer to enable the intensity against     |
|                       |      | wave number to be plotted with high          |
|                       |      | sensitivity [1].                             |

| Thermogravimetry        | TG  | The mass of a sample in a controlled   |  |
|-------------------------|-----|--|--|
|                         |     | atmosphere is recorded continuously as |  |
|                         |     | a function of temperature or time [5]. |  |
| Derivative of the       | DTG | Derivative of the thermogravimetric    |  |
| thermogravimetric trace |     | curve                                  |  |

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#### Preface

The research done for this PhD study is joined in this book in the form of 3 extended self-contained articles (Chapters 2-4) featuring different aspects of the research. Chapter 1 is an introduction to the general concepts dealt with in this research as well as an outline of the aims and importance of this research. Chapter 5 is a general concluding chapter, with some ideas on future research in this field. The abbreviated versions of the articles were submitted to different journals. A list of publications, patents and conference proceedings emanating from this research are given in Appendix A.

# Chapter 1

# Introduction

Some general, overall aims and objectives of this study, as well as some introductory topics are described. More specific aims and introductions are stated within each draft article, which forms the chapters of this thesis.

#### 1.1. The evolution of this project

The first and foremost aim of this project was to use the cheaper carbonate layered double hydroxide (LDH-CO<sub>3</sub>) as a starting reagent in producing fatty acid intercalated LDHs, in stead of the more expensive and cumbersome to prepare chloride LDH. Ion exchange between the highly charged  $CO_3^{2-}$  and the sodium salt of a carboxylic (fatty) acid is not a viable process [1,2]. The fatty acid was used as starting reagent in stead of its salt. The pK<sub>a</sub> values of carbonic acid are 6,35 and 10,33 at 25 °C respectively for the two protonation steps [3,4], which are higher than that of the fatty acid because an acid will donate a proton to the conjugate base of any acid with a higher pK<sub>a</sub> [6]. CO<sub>2</sub> gas will subsequently be released. Hibino *et al.* [7] found that in LDHs with Mg/Al ratio of 2, no leaching of Mg<sup>2+</sup> cations took place in acideous aqueous paramolybdate solutions, whereas substantial leaching of Mg<sup>2+</sup> took place for LDHs with Mg:Al ratios of 3 and 4. Therefore one does not expect Mg<sup>2+</sup> ions to leach during the intercalation reaction involving stearic acid and the LDH Mg<sub>4</sub>Al<sub>2</sub>(OH)<sub>12</sub>CO<sub>3</sub> '3H<sub>2</sub>O.

In the current study the intercalation reaction between stearic acid and the LDH was hampered by lump formation. Surfactants (such as SDS) were consequently added to adsorb onto the LDH surface and to emulsify the stearic acid. The performance of polymeric surfactants or polyelectrolytes such as poly(vinyl sulfonate) was tested and led to the discovery of a new route to intercalate

polymers into the LDHs. Finally, the biodegradable film forming polyelectrolyte sodium alginate was used in the role of surfactant for the intercalation reaction. This led to the development of films with desirable physical and water vapour barrier properties.

#### 1.2. The aims of this research

- To develop new techniques for intercalating organic anions (especially fatty acid anions, such as stearate) into LDH-CO<sub>3</sub> and to compare the new techniques to existing techniques in literature. The new technique should not use calcination steps or N<sub>2</sub> atmosphere.
- To develop new techniques for intercalating anionic polymers into LDH-CO<sub>3</sub> in order to produce nanocomposites.
- To use the modified LDH as a filler in thermoplastic starch composites in order to reduce the water vapour permeability of starch.

Chapter 2 describes the intercalation method we used in comparison to existing literature methods. Chapters 3 and 4 describe some applications of these stearate intercalated LDHs, namely as a starting reagent to easily intercalate anionic polymers and as a filler in starch-based composites.



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# Chapter 2

# Stearate intercalated layered double hydroxides: a comparison of methods

Expanded version of article submitted to Journal of Materials Science.

#### Abstract

Calcined and uncalcined layered double hydroxides (LDH-CO<sub>3</sub>) of the composition  $Mg_4Al_2(OH)_{12}CO_3 \cdot 3H_2O$  were intercalated with stearate anions. Molten stearic acid (SA) in water was reacted with the carbonate anions of the interlayer. The presence of a surfactant, used to emulsify the SA and to disperse the LDH, did not significantly enhance the efficiency of intercalation, but prevented lump formation and facilitated the purification of the stearate intercalated LDH (LDH-SA) by removing unreacted SA during washing with water. Glycerol caused the removal of more carbonate anions possibly through intercalation of glycerolate anions, without facilitating stearate intercalation. Melting SA with LDH-CO<sub>3</sub> formed less LDH-SA than when the reaction took place in an aqueous medium. Reconstruction of calcined LDH in the presence of aqueous sodium stearate led to monolayer intercalation, whereas the methods entailing molten SA in aqueous media with LDH-CO<sub>3</sub> led to bilayer intercalation. Thermogravimetry was used for the first time to quantify the LDH-SA phase. The % mass loss in the temperature region 400-430 °C had a linear relationship to the relative amount of intercalated phase as determined by the internal standard method of XRD ( $I_{50A}/I_{9,3}$  Å).

Keywords: layered double hydroxide, hydrotalcite, intercalation, stearic acid, glycerol, surfactant, calcinations, reconstruction, melt intercalation, infrared spectroscopy, thermogravimetry, X-ray diffraction

#### 2.1. Introduction

Hydrotalcite is an anionic clay mineral with the composition  $Mg_6Al_2(OH)_{16}CO_3.4H_2O$ , and the layered structure of brucite  $[Mg(OH)_2]$ , in which some of the  $Mg^{2+}$  ions are substituted by  $Al^{3+}$  ions. The presence of the  $Al^{3+}$  ions leads to a residual positive charge in the layers. This positive charge is balanced by anions such as  $CO_3^{2-}$ ,  $Cl^-$  and  $NO_3^-$  or organic anions in the interlayer [1]. For the  $CO_3^{2-}$  containing structure, the d-spacing of the (003) and (006) planes are 7,8 Å and 3,9 Å respectively [2]. A range of compositions are possible in terms of bivalent and trivalent cations and of their relative amounts. These types of compounds are generally referred to as layered double hydroxides (LDHs). They will be referred to as LDH-CO\_3, LDH-Cl or LDH-SA (stearic acid), depending upon the anions residing in the interlayer region. Carlino [3] reviewed the different methods that are employed to intercalate carboxylic acids into LDHs. The relevant methods will be highlighted in the following paragraphs.

Due to the strong electrostatic and hydrogen-bond interactions, the carbonate anions in the interlayer are difficult to ion exchange. When the LDH-CO<sub>3</sub> is dehydroxylated and decarbonated at 400 - 500°C to form a layered double oxide (LDO) and subsequently reconstructed in an aqueous solution of a carboxylic acid (or its salt) or anionic surfactant, intercalation of the acid or the surfactant can be achieved. The hydrophobic interaction between the hydrocarbon chains, contribute to the stability of the intercalated product. The mechanism of this intercalation is believed to consist of the fast rehydration of the oxide and intercalation of  $OH^-$  anions, followed by the slow anion exchange of  $OH^-$  anions by the carboxylate anions [4].

Dimotakis *et al.* [5] developed a method of intercalating carboxylic acids or surfactants into LDH-CO<sub>3</sub> in the presence of glycerol as swelling agent, thereby improving the OH<sup>-</sup> exchange in the interlayer.  $[Mg_6Al_2(OH)_{16}](OH)_2 \times H_2O$  can be prepared from  $[Mg_6Al_2(OH)_{16}]CO_3 \times H_2O$  by calcination and reconstruction in pure water (one volume equivalent) under nitrogen atmosphere. Upon addition of two volume equivalents glycerol, extensive swelling occurs. A glycerated phase, with basal spacing in excess of 40 Å, forms. In the presence of carboxylate anions, facile exchange of OH<sup>-</sup> takes place at room temperature. According to Hansen *et al.* [6], LDH-CO<sub>3</sub> can be swollen in glycerol liquid or glycerol vapour resulting in a basal spacing of 9,6 Å or 14,4 Å respectively. Subsequently, the  $CO_3^{2^-}$  can be exchanged by dissolved nitrate, chloride or sulphate anions. It is believed that the glycerol in the interlayer decreases the electrostatic and H-bond forces acting on the carbonate, making the carbonate more exchangeable with other anions. Another possibility is that glycerolate anions (CH<sub>2</sub>OH–CHOH–CH<sub>2</sub>O<sup>-</sup>) are intercalated and exchanged [6].

Carlino *et al.* [7,8] developed a method in which molten sebacic acid (decane-1,10dicarboxylic acid) and phenylphosphonic acid are intercalated into LDH-CO<sub>3</sub> in the absence of any solvents. The intimate mixture of the acid and LDH-CO<sub>3</sub> are heated slowly to above the melting point of the acid and kept there for 8 to 10 hours. Depending upon the molar ratio of acid to LDH, an intercalated phase or a salt (e.g. magnesium salt) of the acid formed. The products were biphasic because of the presence of unreacted LDH-CO<sub>3</sub> together with the intercalated phases [7,8].

Borja *et al.* [9] developed a method in which the Cl<sup>-</sup> anions in LDH-Cl were ionexchanged by the fatty acid anion in ethanolic solutions of lauric, meristic and palmitic acids. Literature procedures for the intercalation of specifically stearate anions into LDHs, mostly involve the anion exchange of Cl<sup>-</sup> anions in LDH-Cl by stearate anions in aqueous solutions of sodium stearate under nitrogen atmosphere [10,11]. Depending on the amount of stearate present and the temperature employed, a monolayer or bilayer of stearate can be intercalated (Fig.1). The interlayer distance is about 32 Å for the monolayer and 52-53 Å for the bilayer [10,11]. Crepaldi *et al.* [12] developed a method of intercalating terephthalate ions into LDH-DS (dodecylsulphate) by salt formation between the intercalated DS<sup>-</sup> and CTA<sup>+</sup> (N-cetyl-N,N,N-trimethylammonium). The salt is extracted into chloroform.





*Figure 2-1* Monolayer (A) and bilayer (B) arrangement of stearate intercalated LDH (LDH-SA).

Organically modified layered compounds or clays such as LDH-SA can be used to form nanocomposites by being exfoliated within polymer matrices [13] or to protect and carry pharmaceuticals or genes [14] into cells due to its membrane-like structure or as stationary phases for chromatography [15]. Therefore, it would be beneficial to develop methods of intercalation that is time and energy efficient as well as environmentally friendly. In these respects, the starting reagent should be LDH-CO<sub>3</sub>, which is easier to produce on large scale than, for example, the LDH-CI. Furthermore, the use of water, in stead of volatile organic solvents, low temperatures (no calcinations) and no  $N_2$  atmosphere would be beneficial. These aspects are explored in this work.

The aim of this work was to intercalate SA into LDH-CO<sub>3</sub> with the formula  $Mg_4AI_2(OH)_{12}CO_3 3H_2O$  by a wide range of methods to form LDH-SA. The methods entailed reacting both LDH-CO<sub>3</sub> and LDO with SA in aqueous or ethanolic media or mixtures thereof. In the aqueous media the acidic SA is envisaged to react with and replace the  $CO_3^{2^-}$  of the interlayer. To the best of our knowledge the use of SA and water to intercalate LDH-CO<sub>3</sub> has not been studied before. The effect of adding sodium dodecylsulphate (SDS) to the water was also tested. This surfactant-mediated method has, to the best of our knowledge, also not been studied previously. The use of 2:1 (v/v) glycerol/water mixtures with molten SA (similar to the method developed by Dimotakis

*et al.* [5] for nonanoic acid) was also tested as well as reacting the LDH-CO<sub>3</sub> with molten SA in the absence of solvents (similar to the method developed by Carlino *et al.* [7,8] for sebacic acid). Reconstruction of the LDO in the presence of aqueous sodium stearate was also performed. This research was aimed at determining the most efficient method for the intercalation of SA into LDH-CO<sub>3</sub> and developing thermogravimetry (TG) as a quick and easy tool for quantifying the LDH-SA phase.

#### 2.2. Experimental procedure

#### 2.2.1. Sample preparation

The layered double hydroxide (LDH) used in this study had the chemical formula  $Mg_4AI_2(OH)_{12}CO_3 \cdot 3H_2O$  (LDH-CO<sub>3</sub>), and was supplied by Chamotte Holdings (Pty) Ltd, South Africa. The amount of crystalline water was determined from TG analysis. The mole ratio of Mg:AI was 2.01:1 as determined by XRF analysis (Appendix B). The particle size distribution as determined by the Mastersizer 2000 (Malvern Instruments) was d(0,1): 0,694 µm; d(0,5): 5,062 µm and d(0,9): 23,925 µm. The theoretical anionic exchange capacity of this LDH-CO<sub>3</sub> was calculated to be 213 meq/100 g.

According to Itoh *et al.* [10] stearate anions can intercalate up to about 225% of the AEC. Therefore, stearic acid (SA, AR, 65-90%, Bio-Zone Chemicals) was used at 200% of the theoretical anionic exchange capacity (AEC) of the LDH. The intercalation of the LDH-CO<sub>3</sub> by SA was performed by 10 different methods (Table 2-1). A reference sample was also prepared in which no reaction took place (mixture of SA and LDH-CO<sub>3</sub> powders). The naming of methods in Table 2-1 are exemplified by the following: A sample or method name of *Calcined-SDS-water* refers to a sample or method in which LDH-CO<sub>3</sub>, calcined at 500 °C, was reacted with SA in the presence of sodium dodecylsulphate (SDS) and water; the sample *Glycerol-water* was prepared by reacting the LDH-CO<sub>3</sub> and SA in the presence of a glycerol-water mixture. SDS was used to adsorb onto LDH surface to disperse it and to emulsify the SA. Deionised water, Glycerol (99%, UNILAB<sup>®</sup>), sodium dodecylsulphate (SDS, Empicol LZ/D, Akulu Marchon), sodium stearate (chemically pure, minimum 40%, UNILAB<sup>®</sup>) and ethanol (96% rectified, Dana Chemicals) were used. In methods where LDO was used 2 g of the

LDH-CO<sub>3</sub> was weighed, calcined at 500 °C for 2 h and the residue was added to the reaction mixtures. The mixtures were heated and stirred with a magnetic heater/stirrer at 70 °C for 2 h, unless specified as reacted for 24 h. All experiments were carried out in air in order to determine the efficiency of intercalation that one could expect under industrial conditions, where N<sub>2</sub> atmospheres would not be viable. Samples were washed with deionised water to remove excess SDS or glycerol; unreacted SA was not washed out. Mass yields of the LDH-SA were not determined because of the mixed nature of the product (containing SA, LDH-CO<sub>3</sub> and LDH-SA). Therefore, the relative amount of LDH-SA formed and unreacted LDH-CO<sub>3</sub> in the different methods was determined by XRD. Samples were filtered, except in the case of *SDS-water* methods in which the product was separated by centrifugation.

#### 2.2.2. Characterization

#### 2.2.2.1. Fourier Transform Infrared spectroscopy (FTIR)

A Perkin Elmer Spectrum RX I FT-IR System was used to scan the infrared transmittance through a KBr (Uvasol, potassium bromide, Merck) pellet 32 times at a resolution of 2 cm<sup>-1</sup>. The averaged spectrum was background-corrected using a pure KBr pellet run under similar conditions. The pellets were prepared with approximately 2 mg of sample and 100 mg of KBr.

#### 2.2.2.2. Thermogravimetry (TG)

15 mg of the powder sample was placed in a 70  $\mu$ l alumina pan. It was heated from 25 °C to 700 °C at a rate of 10 °C/min in air with no lid in a Mettler Toledo STAR<sup>e</sup> System. The first derivatives of the thermogravimetric traces were used because it is more intuitive.



| Table 2-1 Ex | perimental d | etails on t | the intercalation | methods | investigated. |
|--------------|--------------|-------------|-------------------|---------|---------------|
|              |              |             |                   |         |               |

| Method name and details  | Notes                             |  |  |
|--|-----------------------------------|--|--|
| 1. Water. 4,6 g SA, 2 g LDH-CO <sub>3</sub> , 150 ml water.      | Gelation after ca. 20 minutes     |  |  |
| SA is melted but not dissolved.                                  | and later changed into lumpy      |  |  |
| Filter, dry and grind product.                                   | agglomerates.                     |  |  |
| 2. Calcined-Water. 4,6 g SA, LDO*, 150 ml                        | Lumpy agglomerates formed.        |  |  |
| water. SA is melted but not dissolved.                           |                                   |  |  |
| Filter, dry and grind product.                                   |                                   |  |  |
| <b>3. Ethanol.</b> 4,6 g SA, 2 g LDH-CO <sub>3</sub> , 150 ml    | No lumps formed.                  |  |  |
| ethanol. SA is dissolved in ethanol.                             |                                   |  |  |
| Filter and dry product. No washing.                              |                                   |  |  |
| 4. Ethanol-water. 2 g LDH-CO3 reacted with                       | Small globules formed (ca. 1      |  |  |
| 4,6 g SA in a 1:1 v/v water/ethanol mixture.                     | mm diameter).                     |  |  |
| 5. SDS-water**. 4,6 g SA, 2 g LDH-CO <sub>3</sub> , 150 ml       | Well dispersed product.           |  |  |
| water, 2,5 g SDS. SA emulsified by SDS.                          |                                   |  |  |
| Centrifuge, wash and dry product.                                |                                   |  |  |
| 6. Calcined-SDS-water**. 4,6 g SA, LDO*, 150                     | Well dispersed product.           |  |  |
| ml water, 2,5 g SDS. SA emulsified by SDS.                       |                                   |  |  |
| Centrifuge, wash and dry product.                                |                                   |  |  |
| <b>7. Glycerol-water.</b> 4,6 g SA, 2 g LDH-CO <sub>3</sub> , 50 | Spherical soft lumps formed.      |  |  |
| ml water, 100 ml glycerol. SA is melted within                   |                                   |  |  |
| the liquid mixture, not dissolved.                               |                                   |  |  |
| Filter, wash and dry product.                                    |                                   |  |  |
| 8. Calcined-glycerol-water. 4,6g SA, LDO*, 50                    | A soft gel formed and             |  |  |
| ml water, 100 ml glycerol. SA is melted within                   | transformed into soft lumps.      |  |  |
| the liquid mixture, not dissolved.                               |                                   |  |  |
| Filter, wash and dry product.                                    |                                   |  |  |
| 9. Calcined-Na stearate-water**. LDO*                            | No lumps formation.               |  |  |
| reacted with 5,22 g sodium stearate (2 times                     |                                   |  |  |
| AEC) dissolved in 150 ml water. 150 ml hot                       |                                   |  |  |
| deionised water added after reaction and before                  |                                   |  |  |
| centrifugation to retard rate of gelling of sodium               |                                   |  |  |
| stearate. Washed again with hot deionised                        |                                   |  |  |
| water.   |                                   |  |  |
| 10. Carlino melt. 2 g LDH-CO <sub>3</sub> reacted with 4,6       | Soft mixture showing channels     |  |  |
| g molten SA at 70 °C for 8 h. No solvents                        | through which CO <sub>2</sub> gas |  |  |
| present. In air.   | escaped.                          |  |  |
| 11. Reference. No reaction. 2 g LDH-CO <sub>3</sub>              | -                                 |  |  |
| powder mixed with 4,6 g SA powder.                               |                                   |  |  |

\* Residue after 2 g of LDH-CO<sub>3</sub> was calcined at 500 °C in air for 2 h. \*\* 24 h reactions was also performed and denoted, for example, as SDS-water-24 h.



#### 2.2.2.3. Powder X-ray diffraction (XRD)

The XRD analyses were done on a Siemens D500 X-ray system equipped with a 2.2 kW Cu long fine focus tube, variable slit and secondary graphite monochromator (to eliminate  $K_{\beta}$  radiation and reduce fluorescent radiation). The system is computer controlled using SIEMENS DIFFRAC <sup>Plus</sup> software. The goniometer was set to reflection mode. Samples were scanned from 1 to 40° 20 with Cu K<sub>a</sub> radiation (1,5418 Å) at a speed of 0,02° 20, with a recording time of 2 s per step and generator settings of 40 kV and 30 mA. For quantitative XRD analyses the internal standard method [16] was used whereby 20 % m/m talc powder (< 10 micron, Sigma-Aldrich, 3MgO.4SiO<sub>2</sub>.H<sub>2</sub>O) was added to the obtained products. Sample preparation was done in standard sample holders by a single person in a repetitive way. Phases were quantified by determining the ratios of the intensities of the basal reflections to that of the 9,3 Å reflection of the talc.

#### 2.2.2.4. Scanning electron microscopy (SEM)

Small amounts of the powder products or pristine LDH were placed onto carbon tape on a metal sample holder. The excess powder was removed by compressed air. A small piece of the gel-like mixture obtained during the *Calcined-glycerol-water* method was placed onto a carbon stub of approximately 5 mm diameter. It was frozen in a Reichert KF80 plunge freezer (Vienna, Austria). The frozen sample was dried in a custom built high vacuum freeze drier (Pretoria Technicon, South Africa). All samples were coated with chromium in a high resolution ion beam coater, Gatan model 681 (Warrendale, PA, USA) and studied with the JSM-6000F field emission scanning electron microscope (JEOL, Tokyo, Japan).





#### 2.3. Results and discussion

Table 2-1 gives a summary of some of the observations made during the reactions.

#### 2.3.1. Results and discussion of the different intercalation methods

#### 2.3.1.1. Reference sample

During the thermogravimetric (TG) analysis of the reference sample, the stearic acid (SA) melted and intercalated to form the LDH-SA product with decomposition peak around 412 °C (Fig. 2-2). At the higher temperatures (during the temperature program), SA probably also reacted with the hydroxyl groups of the LDH layers, leading to the formation of thermally more stable products (decomposition temperatures of 441 °C and 473 °C, Fig. 2-2). Unreacted SA acid with a decomposition peak around 252 °C was present. The pure SA showed a decomposition peak at around 280 °C. The intercalation mechanism is similar to that of the method developed by Carlino *et al.* [7] in which the LDH and carboxylic acid powders were mixed and the acid allowed to melt. FTIR and XRD analysis showed the presence of only unreacted SA and LDH.



*Figure 2-2* Derivatives of the thermogravimetric traces (DTG) of the LDH-CO<sub>3</sub>, SA and the *Reference* mixture of LDH-CO<sub>3</sub> and SA, showing that SA intercalated during the analysis.

#### 2.3.1.2. Ethanol and Ethanol-water methods

In pure ethanolic solution the intercalation could not take place because the SA was not ionized and, therefore, could not react with the carbonate of the LDH-CO<sub>3</sub> (Fig. 2-3, raw data in Appendix C). The amount of LDH-CO<sub>3</sub> present, were anomalously high with respect to the *Reference* sample (Fig. 2-4) because the SA stayed in solution and was not part of the solid product, leaving only a SA coating on the LDH-CO<sub>3</sub>. The presence of 50% v/v ethanol (*Ethanol-water* method) did not reduce the efficiency of intercalation much (in terms of amount of LDH-SA formed) in comparison to the *Water* method (Fig. 2-3). The presence of the 50% v/v ethanol prevented the agglomeration that took place in the *Water* method. Agglomerated spheres of less than 1 mm diameter formed.





#### Method

*Figure 2-3* Relative amounts of the LDH-SA and LDH-CO<sub>3</sub> phases in the samples of different intercalation methods as determined by the internal standard XRD method. The raw data are given in Appendix C.

\* Reflection in the region of 50 Å.

#### 2.3.1.3. Glycerol-water and Calcined-glycerol-water methods

The relative amount of LDH-CO<sub>3</sub> phase diminished drastically in the presence of glycerol in comparison to the other methods (Fig. 2-3 and Fig. 2-4), and that without any calcination. The carbonate vibration at 1365 cm<sup>-1</sup> was drastically reduced and a small peak at 1384 cm<sup>-1</sup> remained. According to Hansen *et al.* [6] this could be attributed to the weakening of the H-bonds between the water and carbonate in the interlayer region by glycerol or even the intercalation of glycerolate anions. Therefore, one would expect more SA intercalation because of the removal of the carbonate counter-ions. However,



less of the LDH-SA product formed in comparison to most methods (Fig. 2-3), a phenomenon which could be attributed to several factors. First, less SA was in the ionized state because the medium consisted of only about 33 % water. Second, FTIR spectra of these samples (Fig. 2-4) indicated a more amorphous structure (broad, unresolved peaks) in comparison to that of the *Water* method. The amorphous LDH-SA would be undetectable by XRD. The weak peak at 1725 cm<sup>-1</sup> (Fig. 2-4), also seen by Borja *et al.* [9] at 1720 cm<sup>-1</sup>, could be attributed to the intercalation of the acid (COOH) itself.



*Figure 2-4* FTIR spectra of the *Water* and *Glycerol-water* methods, showing that the presence of glycerol caused the removal of carbonate from the LDH (large carbonate vibration at 1365 cm<sup>-1</sup> vs. small one at 1384 cm<sup>-1</sup>) as well as a more amorphous arrangement of the stearate species (broad, overlapping carboxylate asymmetric stretching vibrations around 1550 cm<sup>-1</sup>).



LDH particles usually have sand-rose structures (Fig. 2-5 A). The particles consist of many intergrown smaller particulates which reduce the surface area [17]. This sand-rose structure broke down under the influence of the SA to form plate-like structures of large surface area (approximately 10  $\mu$ m diameter, 200-500 nm thickness, Figs. 5 C and D), and gelling occurred. The thickening or "gelling" of the reaction mixture could be attributed to the house of cards arrangement of the plates (Figs. 5 C and D). The structure of the crystals looked much the same as the LDH-SA obtained by Itoh *et al.* [10] The formation of these gels seemed to depend upon the stirring conditions because in the case of the *Calcined-glycerol-water* method, the gel only formed during a large scale experiment (with overhead stirring) and not during the small scale experiment. When the gel of *Calcined-glycerol-water* was diluted and washed with water, dried and ground, neither the plate-like product, nor the sand-rose morphology of the original LDH persisted (Fig. 2-5 B).





*Figure 2-5* Scanning electron micrographs of the LDH-CO<sub>3</sub> showing the sand-rose microscopic structure (A), the powder product (B) and the gel of *Calcined-glycerol-water* (C and D). The bar in A is 2  $\mu$ m, in B 1  $\mu$ m, in C 10  $\mu$ m and in D 2  $\mu$ m.

#### 2.3.1.4. Water, Calcined-water, SDS-water and Calcined-SDS-water methods

The FTIR spectrum of the LDH-SA obtained from the *SDS-water* method (Fig. 2-6) revealed the following: All the stearic acid reacted because the v(C=O) stretching vibration at 1702 cm<sup>-1</sup> was absent. The carboxylate (COO<sup>-</sup>) asymmetric stretching vibrations were at 1539 cm<sup>-1</sup>, 1555 cm<sup>-1</sup>, 1586 cm<sup>-1</sup> and 1635 cm<sup>-1</sup>, which correlates well with the carboxylate asymmetric stretching vibrations (1542 cm<sup>-1</sup>, 1557 cm<sup>-1</sup>, 1589 cm<sup>-1</sup> and 1637 cm<sup>-1</sup>) obtained by Borja *et al.* [9] for meristate intercalated Mg<sub>3</sub>Al-LDH. The carboxylate asymmetric stretching vibrations are different from that of magnesium stearate (Fig. 2-6). The hydroxyl groups of the layers of the Mg<sub>2</sub>Al-LDH are probably not

strong enough Brønsted bases to react with the SA (due to the Lewis acidity of the Al<sup>3+</sup>). Leaching of Mg<sup>2+</sup> from the Mg<sub>2</sub>Al-LDH used in this study (due to the presence of the acidic SA) is not expected because Hibino *et al.* [18] found that no leaching of Mg<sup>2+</sup> cations took place in LDHs with Mg/Al ratio of 2 when treated with aqueous paramolybdate solutions (low pH), whereas substantial leaching took place in LDHs with Mg/Al ratios of 3 and 4. There is, furthermore, stoichiometrically not enough SA present for the salt (magnesium stearate) to form. The presence of the peak at 1362 cm<sup>-1</sup>, attest to the fact that all the carbonate counter-ions did not react (Fig. 2-6). Longer reaction times and higher SA concentrations might be required for the complete conversion of the carbonate ions. The sulphate peak of SDS (1217 cm<sup>-1</sup>, [19]) was not present, indicating that SDS did not co-intercalate (Fig. 2-6), probably because SDS has a different chain length from SA, the stearate intercalated LDH were more stable, the SDS was present in lower concentration than the SA, the SA alone satisfied the anionic exchange capacity and the SDS was not reactive toward the carbonate.

When LDHs are calcined at temperatures around 400 °C, a Mg-Al oxide with MgO-like structure forms [20]. MgO and SA are used to produce magnesium stearate [21]. Therefore, it was not surprising that the product of *Calcined-water* was similar to magnesium stearate in terms of the carboxylate asymmetric stretching vibrations (around 1575 cm<sup>-1</sup>, Fig. 2-6) and the higher decomposition temperature (446 °C vs. 414 °C for *Water* method, Fig. 2-7). However, when SDS or glycerol was present in the system the products did not resemble magnesium stearate (Fig. 2-8). Therefore, these compounds adsorbed onto the basic sites of the LDO, protecting the carboxylic acid group of the SA from attack by the O<sup>2-</sup> Lewis bases and the LDH-SA intercalates with lower decomposition temperatures formed (Fig. 2-8).




*Figure 2-6* FTIR spectra of SDS, *SDS-water* product, magnesium stearate and *Calcined-water* product, showing that magnesium stearate did not form in *SDS-water* method, that SDS did not co-intercalate and that the product of *Calcined-water* were similar to magnesium stearate in the carboxylate asymmetric stretching vibrations (around 1575 cm<sup>-1</sup>).





*Figure 2-7* DTG traces of magnesium stearate, sample *Water* and sample *Calcined-Water*, showing that *Calcined-water* formed a product similar to magnesium stearate.





*Figure 2-8* DTG traces of *Calcined-water*, *Calcined-SDS-water* and *Calcined-glycerol-water*, showing that the presence of SDS or glycerol protected the LDO from reacting with SA to form an Mg/AI stearate type salt; LDH-SA being the main product.

The reflections at 49,52 Å, 25,43 Å, 17,11 Å and 10,34 Å in Fig. 2-9 can be attributed to the bilayer intercalated LDH-SA. The pattern of the relative intensities of these 4 peaks (high, low, high, and low) is reminiscent of that obtained by Borja *et al.* [9] for the ion exchange of Cl<sup>-</sup> in LDH-Cl by meristic acid in ethanol. Itoh *et al.* [10] attributed the reflection at 53 Å as the basal reflection of stearate intercalated LDH (bilayer) with the chains at approximately a 29° angle from the normal of the layers. This phase was present in the samples of all methods (with varying interlayer distances due to varying angles or degrees of interpenetration of the chains) except the *Ethanol* and *Calcined-Na stearate-water* methods. Monolayer intercalated LDH-SA was also present in sample *Calcined-SDS-water* as a minor phase (reflections at 30,35 Å and 15,43 Å, Fig. 2-9) but in none of the other methods (except *Calcined-Na stearate-water*). For SDS intercalation one would expect reflections at 26 Å, 36 Å or 47 Å depending on the mode of



intercalation [22]. The absence of these reflections (Fig. 2-9) indicates that no SDS intercalated, as was seen by FTIR analyses as well.



*Figure 2-9* X-ray diffractogram of method *Calcined-SDS-water-24 h.* Reflections due to bilayer (49,52 Å, 25,43 Å, 17,11 Å and 10,34 Å) and monolayer (30,35 Å and 15,43 Å) intercalated LDH-SA were present.

\* Reflection of internal standard (talc).

Unreacted SA was removed together with the SDS during washing with water; consequently the product was enriched in the LDH-SA and unreacted LDH-CO<sub>3</sub> phases. This explains why there were (anomalously) somewhat more LDH-CO<sub>3</sub> present than in the reference sample (Fig. 2-3). The relative amount of LDH-CO<sub>3</sub>, however, decreased from  $2,1 \pm 0,3$  to  $1,3 \pm 0,2$  when comparing a 2 h reaction with a 24 h reaction.

In a preliminary study it was found that the amount of surfactant did play a role in the amount of stearate that intercalated. For the same relative amounts of LDH and SA, the higher the SDS concentrations, the higher the yield (mass) of the LDH-SA after thorough washing with water and acetone. The internal standard method of XRD (Fig. 2-3) was not sensitive enough to capture these differences (compare *Water* and *SDS-water*). The correlation between the amount of surfactant and amount of stearate intercalation could possibly be attributed to the droplet size of the molten stearic acid as well as the surfactant adsorbing onto the LDH surface, preventing the side-reaction whereby the stearic acid reacts with the surface OH groups of the LDH.

Gelling occurred after 20 minutes of reaction in the *Water* method (as in *Calcined-glycerol-water* method), but in none of the other methods described in this paper. The gel was, however, too weak to withstand the preparation methods for SEM analysis, but it is believed to have the same microscopic structure as depicted in Figs. 5 C and D. Upon vicious shaking, the gel broke and the mixture could be stirred for the remainder of the time. Lumps of growing size started to form, which made magnetic stirring increasingly difficult (especially around and after 2 h of reaction), which possibly inhibited further diffusion of SA into the interlayer regions.

#### 2.3.1.5. Calcined-Na stearate-water method

The carboxylate asymmetric stretching vibration region of sample *Calcined-Na stearate-water* looked almost identical to that of pure sodium stearate (Fig. 2-10). Therefore, at first it seemed as if no intercalation took place. However, reflections due to monolayer intercalation (31,90 Å and 15,69 Å) as well as a minor reflection at 45-48 Å due to bilayer intercalation were seen in XRD (Fig. 2-11). The decomposition temperature ( $T_{peak}$ ) was lower (334 °C) than that of the bilayer intercalated products (about 420 °C). The reaction mixtures' tendency to gel makes the sodium stearate method less attractive.





*Figure 2-10* FTIR spectra of sodium stearate and sample *Calcined-Na stearate-water*, showing that the carboxylate asymmetric stretching vibrations of sodium stearate did not change much after intercalation (only some broadening seen).





*Figure 2-11* X-ray diffractogram of method *Calcined-Na stearate-water-24 h.* Monolayer intercalation with reflections at 31,90 Å and 15,69 Å were obtained together with a minor phase of near bilayer intercalation (45,90 Å).

\* Reflection of internal standard (talc).

#### 2.3.1.6. Carlino melt method

In the case of the *Carlino melt* method less of the LDH-SA phase seemed to form even though more of the LDH-CO<sub>3</sub> disappeared (Fig. 2-3) with respect to the *Water* and *SDS-water* methods. One would expect, however, that more LDH-CO<sub>3</sub> have reacted because of the longer reaction time (8 h vs. 2 h). The low amount of LDH-SA could possibly be ascribed to the following factors: mixing was not as efficient as in the case of stirring in the presence of a solvent, the SA is less ionized due to the absence of water or the LDH-SA is less crystalline and could mostly not be detected by XRD. FTIR results also attested to the formation of a less crystalline product due to the broad overlapping



carboxylate asymmetric stretching vibrations. (Fig. 2-12) The relative heights of the peaks at 1550 cm<sup>-1</sup> and 1583 cm<sup>-1</sup> differed significantly from that of the other methods described in this work (Figs. 4 and 6, which correlated well with the relative heights seen by Borja *et al.* [9]). This is indicative that the carboxylates were present in different amounts in the different environments in comparison to the methods where water was present. There was also some unreacted SA (1706 cm<sup>-1</sup>) left in the *Carlino melt* sample.



*Figure 2-12* FTIR spectrum of the *Carlino melt* product showing different relative intensities of the carboxylate asymmetric stretching vibrations than the *Water* (Fig. 2-4) and *SDS-water* (Fig. 2-6) methods.

#### 2.3.2. The effect of reaction time

The observed interlayer distances (basal reflections) ranged from 47-54 Å. There are indications that intercalated SA reached approached an equilibrium state with increasing reaction time because the interlayer distances decreased: Compare *SDS-water* with *SDS-water-24 h* as well as *Calcined-SDS-water* with *Calcined-SDS-water-24 h* in Table 2-2. The *Carlino melt* sample (which was reacted for 8 h) had an interlayer distance of only 47,04 Å. The solvents and other constituents may also have an effect on the observed interlayer distances (angle of the chains or extent of interpenetration of the chains). The decomposition peak temperature also increased with time (from about 420°C to about 438-446°C, Table 2-2). The higher decomposition temperatures can be due to the fact that the product reached a state closer to equilibrium (optimum Van der Waals interactions between chains) or reaction with hydroxyl groups might have occurred following the displacement of the carbonate anions by the carboxylates.

#### 2.3.3. Correlation between TG and XRD data

The DTG curves of magnesium stearate and the intercalated LDH-SA phase cross each other at 400 and 430 °C (Fig. 2-7) It was thought that the mass loss between these two temperatures could be a quantitative measure of the amount of LDH-SA because it more or less excludes any Mg stearate like salts that might have formed. The mass loss of the uncalcined samples in the region 400-430 °C was indeed directly proportional to the relative amount of the intercalated LDH-SA phase as determined by the XRD internal standard method ( $R^2 = 0.9923$ , Table 2-3). The correlation was good because the basic LDH structure is unchanged. In Table 2-3 one can also see that the relative amount of LDH-SA that formed was dependent on the amount of water present in the medium. In the light of the time-dependent results given in Table 2-2, it is important to apply the TG quantization method only for samples reacted for the same time (e.g. 2 h) because the decomposition temperature (T<sub>peak</sub>) shifted to temperatures above 430 °C at longer reaction times. When the calcination methods were added to the regression, the correlation coefficient decreased to 0,8563, because the reconstruction of the LDO in the presence of substances such as glycerol or SDS was affected due to adsorption onto the reforming crystals. When the Carlino melt and Calcined-Na stearate-water



methods were added to the equation, the correlation coefficient dropped to 0,7515, probably because the intercalation mechanisms at work are so different.

*Table 2-2* Interlayer distances of samples prepared by different methods and peak temperatures ( $T_{peak}$ ) for the decomposition of the LDH-SA phase.

|                     | Interlayer   | Interlayer    | LDH-SA                            |  |
|---------------------|--------------|---------------|-----------------------------------|--|
| Method              | distance of  | distance of   | decomposition T <sub>peak</sub> / |  |
|                     | bilayer / Å  | monolayer / Å | °C                                |  |
| Water               | 49,96-50,86  | -             | 412-414                           |  |
| Calcined-water      | 48,25-50,37  | -             | 441-446                           |  |
| Ethanol-water       | 49,52        | -             | 418                               |  |
| Ethanol             | -            | -             | -                                 |  |
| SDS-water           | 48,94-50,86  | -             | 418                               |  |
| SDS-water-24 h      | 47,02        | -             | 438                               |  |
| Calcined-SDS-       | 54 48        | 30,74 (minor  | 422                               |  |
| water               | 0-1,-10      | phase)        | TLL                               |  |
| Calcined-SDS-       | 49 52        | 30,35 (minor  | 446                               |  |
| water-24 h          | +0,02        | phase)        |                                   |  |
| Glycerol-water      | 48,25-49,94  | -             | 431-438                           |  |
| Calcined-glycerol-  | 48.25-49.97  | -             | 408-425                           |  |
| water               | ,,           |               |                                   |  |
| Calcined-Na         | 48,25 (minor | 31.90         | 334                               |  |
| stearate-water      | phase)       | 01,00         |                                   |  |
| Calcined-Na         | 45,90 (minor | 31.90         | 328                               |  |
| stearate-water-24 h | phase)       | 01,00         | 020                               |  |
| Carlino melt        | 47,04        | -             | 410                               |  |

*Table 2-3* Correlation between XRD and TG data for the quantization of the LDH-SA phase.

| Method             | I <sub>50 Å</sub> /I <sub>9,3 Å</sub> * | % Mass loss from | Equation    | Correlation                   |
|--------------------|---|------------------|-------------|-------------------------------|
|                    |   | 400-430 °C       |             | coefficient (R <sup>2</sup> ) |
| SDS-water          | 5,0                                     | 28               | y = 4,3661x | 0,9923                        |
|                    |   |                  | + 4,9846    |                               |
| Water (100%        | 4,2                                     | 22               |             |                               |
| water)             |   |                  |             |                               |
| Ethanol-water      | 3,0                                     | 17               |             |                               |
| (50% water)        |   |                  |             |                               |
| Glycerol-water     | 1,1                                     | 10               |             |                               |
| (33% water)        |   |                  |             |                               |
| <i>Ethanol</i> (no | 0                                       | 5                |             |                               |
| water)             |   |                  |             |                               |
| Calcined-SDS-      | 7,5                                     | 30               | y = 3,3693x | 0,8563                        |
| water              |   |                  | + 7,5653    |                               |
| Calcined-          | 2,4                                     | 22               |             |                               |
| glycerol-water     |   |                  |             |                               |
| Calcined -         | 3,2                                     | 15               |             |                               |
| Water              |   |                  |             |                               |
| Carlino melt       | 1,2                                     | 20               | y = 3,3755x | 0,7515                        |
|                    |   |                  | + 7,8328    |                               |
| Calcined -Na       | 0,4                                     | 3                |             |                               |
| stearate           |   |                  |             |                               |

\* Relative amount of LDH-SA phase in region of 50 Å.

#### 2.3.4. Recommendations for future work

It would be interesting to study the effect of varying the ratio of glycerol to water in the *Glycerol-water* method because the more glycerol present, the more carbonate will be removed, but the more water present, the more SA will intercalate due to ionization of the SA. A more thorough study of the time-dependent changes in interlayer distance and



basal reflection intensity should be conducted in future, for all methods described in this work. The shift in decomposition temperature should also be followed with time of reaction to learn more about the intercalation mechanism and product.

#### 2.4. Conclusions

This article described a direct method for intercalating fatty acids into LDH-CO<sub>3</sub>, due to a reaction between the carbonate and the ionized SA in aqueous media. In general, such a direct method of intercalation does not work with anions which are unreactive towards the carbonate. Even though the current experiments were carried out in air, virtually no LDH-CO<sub>3</sub> phase reformed in the cases where LDOs were used (Fig. 2-3). Therefore, the bilayer intercalated stearate anions has greater stability than LDH-CO<sub>3</sub>, probably because of the stabilising effect of hydrophobic interactions between the chains [11,23]. Large scale production of the LDH-SA would, therefore, be easy because a  $N_2$  atmosphere is not necessary.

Interestingly, XRD and FTIR analyses of the samples of these water-based methods remarkably resembled those obtained by Borja *et al.* [9] for the ion exchange of Cl<sup>-</sup> in LDH-Cl and the fatty acid in ethanolic media. Therefore, as concluded by Borja *et al.* [9], the fatty acid intercalated in both the dissociated (COO<sup>-</sup>) and undissociated (COOH) form. Itoh *et al.* [10] also obtained bilayer intercalated LDH-SA by exchanging the Cl<sup>-</sup> in LDH-Cl by stearate in aqueous sodium stearate solutions (24 h, 80 °C). It is clear from Fig. 2-11, however, that reconstruction of the LDO in the presence of aqueous sodium stearate led to the intercalation of a monolayer of stearate. Therefore, when using LDH-CO<sub>3</sub> as a starting reagent, molten SA in aqueous medium should be used to obtain bilayer intercalation.

The reaction mixtures of method *Water* and *Calcined-Water* could not be stirred for 24 h because large lumps (> 1 cm) tended to form, making stirring difficult. The lump formation did not drastically decrease the rate of LDH-SA formation within the first 2 h in comparison to the *SDS-water* and *Calcined-SDS-water* methods and it is unknown whether the rate of reaction is inhibited upon longer stirring times. Sodium dodecyl



sulphate (SDS) not only prevented this agglomeration, but also kept the unreacted SA in emulsion; therefore removing it from the final product. A purer LDH-SA end-product resulted with less effort. The surfactant-mediated methods of intercalation are, therefore, environmentally friendly because the SDS solutions should be recyclable and no volatile or flammable organic solvents (such as ethanol) are needed to free the product from SA. In the case of the Water methods the products were hard lumps, whereas in the surfactant-mediated methods the products were soft and easy to grind to a fine powder. Therefore, the surfactant played a role in terms of ease of stirring and ease of purification and grinding of the product and not in facilitating the reaction. The relative amounts of LDH-SA formed in the SDS-water-24 h, Calcined-SDS-water and Calcined-SDS-water-24 h methods (Fig. 2-3) were similar. The Calcined-SDS-water method was the most time efficient and the amount of LDH-SA formation seemed to have reached a plateau within the 2 hours. The SDS-water method should be tested at more time intervals to determine when a plateau is reached. The thermal history of the LDH-SA (whether it was calcined or not) could have an influence on the performance of the products within a given application and should be tested. When exposing the LDO to aqueous SA, however, a thermally more stable Mg/AI stearate type salt formed and much less of the desired LDH-SA in comparison to Calcined-SDS-water (Fig. 2-3). In the presence of glycerol, the  $CO_3^{2-}$  of the LDH-CO<sub>3</sub> were removed and probably replaced by glycerolate anions, without facilitating the intercalation of SA because the 2:1 glycerol/water does not allow ionization of as much SA as do pure water.

In this study it was found that TG could be used for quantification of the LDH-SA phase (especially for uncalcined samples) because the % mass loss in the region 400-430 °C correlated with the relative amount of LDH-SA phase as determined by XRD (internal standard method). Quantitative XRD needs more sample as well as the addition of an internal standard. Furthermore, sample preparation needs to be done meticulously and repetitively to prevent orientation of the LDH-SA crystals. If preferred orientation occurs, the intensity of the interlayer distance reflection is artificially enhanced [24] and the intensity could, therefore, be subject to erroneous quantification. TG analysis, on the other hand, requires only a few milligrams of sample and no special sample preparation





techniques to prevent preferred orientation of the crystals. The gradient of the linear equation (Table 2-2) indicated that the TG analysis was 3-4 times more sensitive than XRD to the amount of LDH-SA present.

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## Chapter 3

# Poly(vinyl sulfonate) intercalation into stearate intercalated layered double hydroxides

Expanded version of article submitted to *Journal of Colloid and Interface Science*.

#### Abstract

Poly(vinyl sulfonate), PVS, was intercalated into a carbonate layered double hydroxide (LDH-CO<sub>3</sub>), after an intercalative reaction with stearic acid in a one-pot reaction. The intercalated stearate ion exchanged with the PVS to form sodium stearate and LDH-PVS. Within an hour at 78 °C all the carbonate anions reacted. The PVS intercalated material had low crystallinity and features an interlayer distance of 13,91 Å attributed by Oriakhi *et al.* [1] to a bilayer intercalation.

*Keywords*: layered double hydroxides; carbonate hydrotalcite; intercalation; stearate; poly(vinyl sulfonate); ion exchange

#### 3.1. Introduction

Intercalation of polymers into layered inorganic minerals has recently received a lot of attention [2]. The composites display physical properties, due to the molecular level interactions, that cannot be achieved by the polymer or filler alone. For instance, the polymer could be protected from UV degradation, the mineral could act as flame retardant or the thermal stability of the composite could be enhanced above that of the separate constituents [2,3].

Hydrotalcite  $[Mg_6Al_2(OH)_{16}CO_3 H_2O]$  is an anionic clay. It is a member of the family of layered double hydroxides (LDH). LDHs have the same stacked sheet structure as brucite  $[Mg(OH)_2]$  but are distinguished by the partial replacement of  $Mg^{2+}$  with  $Al^{3+}$  ions in the sheets and the presence of charge balancing anions, for example  $CO_3^{2-}$ ,  $Cl^-$ ,  $NO_3^{-}$  or stearate, in the interlayer [4]. The corresponding compounds are referred to as LDH-CO<sub>3</sub>, LDH-CI, LDH-NO<sub>3</sub> or LDH-SA.

Several methods have been employed [1,5,6,7] to intercalate polymers into LDHs and other layered minerals or clays. Anionic polymers such as poly(styrenesulfonate), poly(acrylic acid) and poly(vinylsulfonate) have been intercalated by synthesizing the LDH in the presence of the polymer [1,5]. The products obtained were amorphous but hydrothermal treatment improved the crystallinity [5]. The polymers only intercalated under N<sub>2</sub> atmosphere. When the procedure was attempted in air, the carbonate intercalated LDH (LDH-CO<sub>3</sub>) was obtained [1]. Choy et al. [6] successfully intercalated DNA (deoxyribonucleic acid, an anionic polymer) into  $Mg_2AI-NO_3$  LDH by ion exchange. The key to intercalation into layered species is usually to modify the interlayer region by surfactants with hydrophobic tails [2]. This surfactant-mediated method was successfully used by Kerr et al. [7] to intercalate poly(p-phenylene) into MoO<sub>3</sub>. The polymer chains are preferentially adsorbed into the hydrophobic interlayer region from the polar solution.



Due to the strong electrostatic and hydrogen-bond interactions, the carbonate anions in the interlayer are difficult to ion exchange. When the LDH-CO<sub>3</sub> is dehydroxylated and decarbonated at 400 - 500°C to form a layered double oxide (LDO) and subsequently reconstructed in an aqueous solution of a carboxylic acid (or its salt) or anionic surfactant, intercalation of the acid or the surfactant can be achieved [8]. Fatty acids such as stearic acid, however, can be intercalated into uncalcined LDH-CO<sub>3</sub> (unpublished results). The stearate anions intercalate as a bilayer into the interlayer of the LDH (Fig. 3-1) with an interlayer distance in the region of 50 Å. The aim of this study was to intercalate stearate anions into the interlayer region of Mg<sub>4</sub>Al<sub>2</sub>(OH)<sub>12</sub>CO<sub>3</sub>·3H<sub>2</sub>O (LDH-CO<sub>3</sub>) by using molten stearic acid (SA) emulsified by poly(vinyl sulfonate) in a water-ethanol medium. Possibly the stearate bilayer would facilitate the intercalation of the PVS. This would represent an easy and environmentally friendly method of intercalating an anionic polymer into the cheap LDH-CO<sub>3</sub>, without the need for energy intensive calcination.





#### 3.2. Materials and methods

#### 3.2.1. Materials

The layered double hydroxide used in this study had the chemical composition  $Mg_4Al_2(OH)_{12}CO_3 H_2O$ . The mole ratio of Mg:Al was determined from XRF analysis as 2.01:1 (Appendix B). The LDH was received from the local manufacturer Chamotte Holdings (Pty) Ltd. The particle size distribution as determined by a Mastersizer 2000 (Malvern Instruments) was d(0,1): 0,694 µm; d(0,5): 5,062 µm and d(0,9): 23,925 µm. The theoretical anionic exchange capacity of this LDH-CO<sub>3</sub> was calculated to be 213 meq/100 g.

25% m/m poly(vinyl sulfonate, sodium salt) solution in water (PVS, Mw 70 000, Sigma-Aldrich), stearic acid ( $C_{18}H_{36}O_2$ , Merck, 85% pure) and ethanol (96% rectified, Dana Chemicals) were used. Reactions were carried out in deionized water. Deionized water, tap water or solutions of CaCl<sub>2</sub>.2H<sub>2</sub>O (UNIVAR<sup>®</sup>, Saarchem) in deionized water (20 volume equivalents) were used to dilute the reacted mixtures (1 volume equivalent).

#### 3.2.2. Intercalation method

8 g of the 25% m/m sodium-PVS solution in water was added to 57 ml deionised water to obtain a solution consisting of approximately 2 g of PVS in 60 ml water. This solution was heated to 78 °C. 0,7 g stearic acid (SA) was dissolved in 30 ml ethanol and heated to approximately 60 °C. The SA solution was slowly added to the PVS solution and the temperature allowed to reach 78 °C. 0,34 g of the LDH powder was added to the solution and stirred for 1 h. Itoh *et al.* [9] found that stearate is capable of intercalating up to about 225% of the anionic exchange capacity (AEC) of the LDH and therefore a level of 200% SA in relation to the AEC was used. The reaction mixture will be referred to as the PVS-SA-LDH mixture.

#### 3.2.3. Characterization

#### 3.2.3.1. Fourier Transform Infrared spectroscopy (FTIR)

A Perkin Elmer Spectrum RX I FT-IR System was used to scan the infrared transmittance through a KBr (Uvasol, potassium bromide, Merck) pellet 32 times at a resolution of 2 cm<sup>-1</sup>. The averaged spectrum was background-corrected using a pure KBr pellet run under similar conditions. The pellets were prepared with approximately 2 mg of sample and 100 mg of KBr. The 2 mg powder samples were obtained by diluting the cooled down reaction mixture with a 20-fold excess of deionised or tap water or CaCl<sub>2</sub> solution, in order to release (flocculate) the insoluble reaction products, which were subsequently centrifuged off, washed again (to remove any unreacted PVS or salts), dried and ground.

#### 3.2.3.2. Powder X-ray Diffraction (XRD)

The XRD analyses were performed on a Siemens D500 X-ray system equipped with a 2.2 kW Cu long fine focus tube, variable slit and secondary graphite monochromator (to eliminate  $K_{\beta}$  radiation and reduce fluorescent radiation). The system is computer controlled using SIEMENS DIFFRAC <sup>Plus</sup> software. The goniometer was set to reflection mode. Samples were scanned from 1 to 35° 20 with Cu K<sub>a</sub> radiation (1,5418 Å) at a speed of 0.02° 20, with a recording time of 2 s per step and generator settings of 40 kV and 30 mA. Part of the reacted mixture was cast onto an aluminium sample holder and the solvent was allowed to evaporate. This was repeated a few times to obtain enough material to mask the aluminium. One would expect the intercalated LDH phases to be highly oriented within these holders and the interlayer distances to be preferentially enhanced [10].

#### 3.2.3.3. Scanning Electron Microscopy (SEM)

A small disc of the clear and white parts of the gel was placed onto carbon stubs of approximately 5 mm diameter. It was frozen in a Reichert KF80 plunge freezer (Vienna, Austria). A drop of the gel that was diluted with deionized water was also placed on a stub and was frozen in the same way. The frozen samples were dried in a custom-built high vacuum freeze drier (Pretoria Technicon, South Africa). A drop of the gel that was diluted with deionized water was also allowed to air dry on a stub. These were coated by chromium in a high resolution ion beam coater, Gatan model 681 (Warrendale, PA, USA) and studied with a JSM-6000F field emission scanning electron microscope (JEOL, Tokyo, Japan).

#### 3.2.3.4. Transmission Electron Microscopy (TEM)

The mixture (before onset of gelling) was diluted with deionised or tap water. A droplet of the solution containing white suspended particles was placed onto a carbon coated formvar grid, the excess water was removed by the capillary action of filter paper and it was allowed to dry in air. The Philips EM301 (Eindhoven, Netherlands) Transmission electron microscope was used.

#### 3.3. Results and discussion

#### 3.3.1. General

After the addition of the LDH-CO<sub>3</sub> to the SA-PVS emulsion, CO<sub>2</sub> gas was released. Some particles settled to the bottom after the reaction, but most of the particles were suspended. In time a small amount of clear solution collected at the top. Within a few days both the clear phase and the reaction mixture as a whole had gelled. Upon shaking, the gel broke but reformed in time. Experiments showed that the sodium PVS solutions did not gel in the presence of Mg<sup>2+</sup>, Al<sup>3+</sup>, Ca<sup>2+</sup> or H<sup>+</sup> ions as some other anionic polymers do. The gelling mechanism is, therefore, unknown.

Before the onset of the gelling, some of the mixture was diluted with water. Upon addition of 20 volumes of deionized water, a suspension of white fluffy particles (> 10-20  $\mu$ m, Fig. 3-7E) formed. After centrifuging, the sediment particles went back into suspension upon the least disturbance, probably due to electrostatic repulsion. The white particles have been unchanged and in suspension for more than a year at the time of writing. Upon dilution with tap water, however, the suspension became unstable and the fluffy particles collected at the top. With



time the particles formed heavy white globules, which settled to the bottom. After 2 to 3 months the solution and the sediment became yellow due to oxidation of the PVS (Fig. 3-2).



*Figure 3-2* The reaction mixture diluted with tap water (A) and deionized water (B), showing that the suspension is destabilized by the divalent cations in tap water, leading to PVS release and decomposition.

#### 3.3.2. FTIR results

When PVS was not present in the system, the reaction between LDH-CO<sub>3</sub> and SA could not proceed to completion under the conditions employed (78 °C, 1 h) as evidenced by the presence of unreacted carbonate (1367 cm<sup>-1</sup>) and unreacted carboxylic acid (1703 cm<sup>-1</sup>) in Fig. 3-3A. In the presence of other surfactants, such as sodium dodecyl sulfate (SDS), the reaction also does not go to completion, even in 24 hours. In the presence of PVS, however, the reaction proceeded to completion under the same conditions (only 1 hour). Only a small carbonate vibration peak remained at 1383 cm<sup>-1</sup> (Fig. 3-3B). The LDH platelets



were still intact, because the OH stretching vibration (3440 cm<sup>-1</sup>) and the O-M-O bending vibration (446 cm<sup>-1</sup>) were present (Fig. 3-4) [11]. If the hydroxide layers had reacted to form an Mg/AI type stearate salt, these vibrations would no longer be present. The PVS is intercalated (refer to Section 3.3.3): In spite of extensive washing, the sulfonate peak around 1176-1181 cm<sup>-1</sup> remains (Figs. 3 and 4B).

When heating and melting SA in the presence of PVS, no acid-base reaction can occur because sodium PVS is a weak conjugated base of the strong polyvinyl sulfonic acid. Therefore, one does not expect sodium stearate and polyvinyl sulfonic acid to form. Upon cooling, the SA crystallizes out of the emulsion. When the PVS-SA-LDH reaction product was diluted with tap water or CaCl<sub>2</sub> solution, the observable peaks in the carboxylate asymmetric stretching region were different from when it was diluted with deionized water. The peak at 1558 cm<sup>-1</sup>, which corresponds to that of sodium stearate, decreased in intensity and peaks at 1572 and 1539 cm<sup>-1</sup>, which corresponds to that of calcium stearate, appeared (Figs. 3B and C). Therefore, sodium stearate formed during the PVS-SA-LDH-CO<sub>3</sub> reaction. In comparison, when PVS is absent, the vibration peaks in the carboxylate asymmetric stretching region were typical of stearate intercalated LDHs (Fig. 3-3A and [12]).





*Figure 3-3* FTIR spectra of the LDH-SA (A), PVS-SA-LDH product (B) and the PVS-SA-LDH product isolated from tap water (C), showing that sodium stearate (1558 cm<sup>-1</sup>) formed, which changed to calcium stearate (1572 cm<sup>-1</sup>, 1539 cm<sup>-1</sup>) in tap water in contrast to the typical LDH-SA bands at 1538 cm<sup>-1</sup> and 1581 cm<sup>-1</sup> (A).





*Figure 3-4* FTIR spectra of the PVS-SA-LDH reaction mixture (bottom) and the LDH-CO<sub>3</sub> (top), showing that the PVS intercalated and that the LDH platelets were intact (O-M-O bending vibration at 445 cm<sup>-1</sup>).

It is supposed that the mechanism of intercalation of the PVS into the LDH consists of two steps. First, the acid-base reaction between SA and the interlayer carbonate anions takes place, releasing H<sub>2</sub>CO<sub>3</sub> and eventually CO<sub>2</sub>, with the stearate anions being intercalated as bilayers. Second, the sodium PVS ion exchange with the stearate ions, releasing sodium stearate and the PVS intercalates. The entropy gain due to the release of the bilayer-intercalated stearates is probably larger than the entropy loss due to the intercalation of the PVS. The sodium stearate probably stabilized the suspended particles through electrostatic repulsion, but in tap water calcium stearate formed, which precipitated and, hence, could not stabilize the suspension.

#### 3.3.3. XRD results

The X-ray diffractogram (Fig. 3-5) of the reaction product obtained in the absence of PVS showed the presence unreacted SA (39,20 Å, 13,17 Å, 4,12 Å and 3,11 Å), unreacted LDH-CO<sub>3</sub> (7,60 Å, 3,79 Å and 2,57 Å) and bilayer intercalated LDH-SA (49,52 Å, 25,43 Å, 17,11 Å, 10,29 Å). The product obtained in the presence of PVS was amorphous (broad, low intensity reflections, Fig. 3-6). The reflections at 13.91 Å (and 6.94 Å, second order) are due to intercalation of a bilayer of PVS [1] and it correlates well with the value of 13,1 Å observed by Oriakhi et al. [1]. The reflection at 45,17 Å is probably the remnant of bilayer intercalated LDH-SA which was too stable to allow for exchange with PVS chains because of the high degree of interpenetration of the two stearate layers. There was only a small reflection left at 7.81 Å, indicating that most of the LDH-CO<sub>3</sub> reacted. When stirring the LDH-CO<sub>3</sub> and PVS together under the same conditions but in the absence of SA, the diffractogram of the LDH-CO<sub>3</sub> was unchanged (not shown). This is due to the stability of the LDH-CO<sub>3</sub> and the slow diffusion of the polymer chains [1]. The intercalated stearate anions destabilize the layered structure and allows for the PVS chains to intercalate.





*Figure 3-5* X-ray diffractogram of the LDH-SA product formed in the absence of PVS, showing that it is highly crystalline.





*Figure 3-6* X-ray diffractogram of the dried PVS-SA-LDH reaction mixture, showing that the LDH-SA reflections diminished and LDH-PVS appeared at around 13,91 Å. The peaks are broad and of low intensity, attesting that the products are less crystalline.

#### 3.3.4. SEM results

The FTIR results showed that sodium stearate had formed. It was originally thought that the gelling was caused by formation of sodium stearate within the PVS-SA-LDH mixture. When the microstructures of sodium stearate (Fig. 3-7A) and the clear part of the gel (Fig. 3-7B) are compared, this is clearly not the case. The latter shows a spaghetti-like structure approximately 200 nm in diameter and several micrometers in length. Fig. 3-7C is the SEM micrograph of the white part of the gel, which shows large plate-like structures of the LDH (> 10  $\mu$ m diameter), which are similar to the structures obtained by Itoh et al. [9] for stearate intercalated LDHs. The SA and PVS stabilize this plate-like structure above the usual sand-rose – intergrown particulates – structure of LDH-CO<sub>3</sub> (Fig. 3-7D) [13]. The SEM micrograph (Fig. 3-7E) of the freeze-dried suspension of the mixture diluted with deionized water consisted of large thin plate-like structures (> 20  $\mu$ m diameter). When the diluted mixture was allowed to air dry, the plate-like structures seemed to role up into tubes of diameter  $0.5 - 1 \mu m$  (Fig. 3-7F). When freeze-dried, the rolling up could not take place and the large, thin plates remained in their original state. Dispersing these plate-like structures, of which the thickness is in the sub-micrometre region, into polymer matrices could lead to the formation of nanocomposites.





Figure 3-7 Scanning electron micrographs of

- (A) Freeze-dried sodium stearate gel, bar is 10  $\mu$ m.
- (B) Freeze-dried clear part of the gel of the PVS-SA-LDH reaction mixture, bar is 500 nm.
- (C) Freeze-dried white part of the gel of the PVS-SA-LDH reaction mixture, bar is 5  $\mu$ m.
- (D) The sand-rose microscopic structure of the LDH-CO<sub>3</sub>, bar is 2  $\mu$ m.
- (E) Freeze-dried sample of the diluted PVS-SA-LDH suspension, bar is 10  $\mu$ m.
- (F) Air-dried sample of the diluted PVS-SA-LDH suspension, bar is 1  $\mu$ m.
- (G)

#### 3.3.5. TEM results

The TEM images of the tap and deionized water diluted air-dried samples showed the presence of long fibers or tubes (Figs. 8A and B, > 10  $\mu$ m long and 1  $\mu$ m wide, possibly the same as was seen in Fig. 3-7F), small unreacted particulates (black, less than 1 µm in size) and large plate-like structures (approximately 10 µm diameter, Figs. 8C and D). In the case of diluting with tap water, the fibers looked more etched, as if it reacted (Fig. 3-8B). Upon drying, the plate-like structures seemed to crack (Fig. 3-8C). It might be that this cracking phenomenon led to the formation of the fiber- or tube-like structures; or perhaps the large plates rolled up to form long, thin tubes. The fibers seem to be of the same length as the diameter of the flat layers (10-20  $\mu$ m, Figs. 7C, 7E and 8D). Tube-like and fiber-like features were reported by Leontidis et al. [14,15] for PEO-SDS-acetate-Pb-sulfide containing systems as well as by Ogata et al. [16] for Zn(OH)<sub>2</sub>-carboxylic acid systems, which are both similar to the current system (layered inorganic substances in combination with carboxylic acids). The fact that the plates are so thin attests to the fact that the sand-rose morphology was broken down to a large extent and that the stearate and PVS stabilized the structure at a few layers. It is possible that exfoliation took place some extent as well. Moujahid et al. [5] found that LDH-CI exfoliated in excess polystyrene sulfonate and possibly the same happened for LDH-SA in excess PVS, which also explains the almost featureless X-ray diffractogram (Fig. 3-6).





Figure 3-8 Transmission electron micrographs of

- (A) Deionized water diluted PVS-SA-LDH reaction mixture dried in air, showing smooth fibers or tubes. Bar is 2  $\mu$ m.
- (B) Tap water diluted PVS-SA-LDH reaction mixture dried in air, showing etched (reacted) fibers or tubes. Bar is 2 μm.
- (C) Deionized water diluted PVS-SA-LDH reaction mixture dried in air, showing large, plate-like structures. Bar is 3 μm.
- (D) Deionized water diluted PVS-SA-LDH reaction mixture dried in air, showing cracked plate-like structures. Bar is 10 μm.



#### 3.4. Conclusions

The stearic acid reacted with all of the carbonate in the interlayer (FTIR results). XRD showed that the PVS had intercalated and the amount of LDH-SA had diminished. The stearate and PVS anions exchanged to form sodium stearate. The process might be driven by the increase in entropy due to the disassembly of the stearate bilayer. Calcination was not necessary to successfully intercalate the stearate and PVS into the LDH-CO<sub>3</sub>; therefore the LDH platelets could keep their original crystallinity. No N<sub>2</sub> atmosphere was needed, probably because the LDH-SA is of similar stability than the LDH-CO<sub>3</sub>. The layered mineral or clay is sometimes modified by a surfactant in a separate step before introducing the polymer [2], but in the current system the surfactant modification and polymer incorporation takes place in one pot. In most other instances the polymer intercalated LDHs is prepared by synthesizing (coprecipitating) the LDH in the presence of the polymer; a procedure which requires a N<sub>2</sub> atmosphere. The current process is more environmentally friendly (no calcination, single batch), cheap (LDH-CO<sub>3</sub> starting reagent) and upscalable (no N<sub>2</sub> atmosphere).

The intercalated PVS appears to be stabilized and protected from oxidative or UV degradation (Fig. 3-2). This reaction could possibly be carried out simultaneously with emulsion polymerization of polymers in order to ensure good dispersion of the LDH into the polymers, which could lead to the formation of nanocomposites. The PVS intercalation could also be a model for intercalation of other anionic polymers, like DNA, by the same method.

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## Chapter 4

### Stearate intercalated layered double hydroxides: effect on the physical properties of dextrin-alginate films

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## Abstract

The effect of stearate intercalated layered double hydroxides (LDH-SA) on the water vapour permeability (WVP) and mechanical properties of glycerol plasticized dextrin-alginate films were tested. The LDH Mg<sub>4</sub>Al<sub>2</sub>(OH)<sub>12</sub>CO<sub>3</sub> 3H<sub>2</sub>O and stearic acid (SA) were reacted in different mass ratios within the film solutions. The filler (SA and LDH) concentration was fixed at 16% m/m of the dried films. Infrared spectroscopy verified that the SA did indeed intercalate. WVP measurements showed a broad range of minima around filler compositions of 50-80% SA (and 50-20% LDH). The Young's moduli of the films showed a maximum increase of 213% around the filler composition of 60% SA (40% LDH). From the interlayer distances and intensities of the basal reflections of the LDH-SA (as determined from X-ray diffraction, XRD) and the increased Young's moduli it was concluded that delamination and exfoliation of the LDH-SA took place. A layered and oriented microscopic structure was seen by scanning electron microscopy (SEM).

Keywords: Layered double hydroxides, stearic acid, intercalation, starch, dextrin, alginate, edible films, water vapour permeability, Young's modulus, exfoliation, delamination, cross-linking

# 4.1. Introduction

Edible films are used to protect foodstuff from water vapour and oxygen in their environment and to prevent water moving from one part to another in multicomponent foodstuffs, for example to separate the filling or sauce from the dough of pizzas or pies. Most edible film-forming polymers or hydrocolloids (such as starch, sodium alginate, and sodium caseinate) are hydrophilic and pose no barrier against water vapour, and becomes soggy in contact with water. Lipid films are good barriers against water, but have little structural integrity. This problem has been overcome using laminates of hydrocolloid and wax films and also by making emulsions of the wax or lipid within the hydrocolloid solution. Waxes such as beeswax and stearic acid are emulsified within the surface-active sodium alginate or sodium caseinate and their blends with starch. [1,2,3]

Polymer-layered clay nanocomposites are filled polymers in which at least one of the dimensions of the filler is in the nanometre range (less than 100 nm). Nanocomposites in general have increased modulus, strength and heat resistance, as well as decreased gas permeability and flammability in comparison to the pristine polymer. [4] Studies were done on preparing composites of starch with kaolin [5], Ca<sup>2+</sup> hectorite [6] and kaolinite, hectorite, layered double hydroxide (LDH) and brucite [7]. These studies focused mainly on the mechanical properties and microstructure of the composites as well as determining whether exfoliation took place by means of X-ray diffraction. These platelet fillers, however, can ideally be used to reduce the WVP of hydrophilic polymers such as starch or alginate.

The water vapour permeability (WVP) and also the permeability to large organic molecules (or pharmaceuticals) of sodium alginate and sodium caseinate films can be reduced by cross-linking with polyvalent cations, e.g.  $Ca^{2+}$ . This can be done by immersing films in solutions of  $Ca^{2+}$  salts [3] or by *in situ* leaching  $Ca^{2+}$  ions from insoluble CaCO<sub>3</sub> by acids [8]. This mechanism might play a role in the

current system that is composed of an insoluble layered double hydroxide and stearic acid.

Hydrotalcite anionic clay mineral with composition is the an  $Mg_6Al_2(OH)_{16}CO_3.4H_2O$ . It has the same layered structure as brucite  $[Mg(OH)_2]$ but with some of the Mg<sup>2+</sup> ions substituted by Al<sup>3+</sup> ions. The presence of the Al<sup>3+</sup> ions gives rise to a residual positive charge in the layers. This positive charge is balanced by anions such as  $CO_3^{2^-}$ ,  $CI^-$  and  $NO_3^-$  or organic anions in the interlayer. [9] A range of compositions is possible in terms of bivalent and trivalent cations and of their relative amounts. These types of compounds are more generally referred to as layered double hydroxides (LDHs).

In the present study a combination of an LDH [Mg<sub>4</sub>Al<sub>2</sub>(OH)<sub>12</sub>CO<sub>3</sub>·3H<sub>2</sub>O] and stearic acid (SA) was used to reduce the WVP of glycerol-plasticized dextrinalginate films. Ideally the SA would intercalate into the LDH structure to form LDH-SA during the film solution preparation. Stearate and other surfactant intercalated LDHs have large, plate-like microscopic structures [10,11] and this extended plate-like structures would lower the WVP of the dextrin-alginate films depending on their relative orientation within the films.

# 4.2. Experimental

# 4.2.1. Materials

The materials used, their source of origin, and their respective roles are given in Table 4-1.

Table 4-1 Components of the films and their roles.

| Component name  | From   | Role   |
|---|--|--|
| Dextrin, Stydex 074030  | AfricanProducts(Pty.)Ltd,SouthAfrica.                                      | Biodegradable polymer  |
| Sodium Alginate (E401),<br>Manugel GMB, viscosity of 1%<br>solution is 185 cps.   | Kelco International<br>Limited   | Biodegradable polymer,<br>film former, emulsion<br>stabilizer (due to high<br>viscosity), prevent<br>agglomeration of LDH-<br>SA |
| 99% Glycerol  | Merck, UNILAB <sup>®</sup>   | Plasticizer  |
| 85% Stearic acid  | Merck  | Hydrophobic, intercalate into LDH.   |
| LDH, $Mg_4Al_2(OH)_{12}CO_3 3H_2O$<br>Particle size distribution by<br>Mastersizer 2000 (Malvern<br>Instruments): d(0,1): 0,694 µm;<br>d(0,5): 5,062 µm and d(0,9):<br>23,925 µm. The XRF analysis is<br>given in Appendix B. | Chamotte Holdings<br>(Pty.) Ltd., South<br>Africa                          | Filler, intercalated by SA.  |
| Talc  | Sigma-Aldrich, < 10<br>micron,<br>3MgO.4SiO <sub>2</sub> .H <sub>2</sub> O | Filler, cannot be<br>intercalated by SA.<br>Coated and dispersed<br>by SA.   |
| Bentonite Ocean Clear   | Boland Base<br>Minerals, South<br>Africa                                   | Filler, cannot be<br>intercalated by SA,<br>coated and dispersed by<br>SA.   |
| Foamaster 8034  | Cognis   | Prevent foam formation due to $CO_2$ release.  |
| Deionised water or tap water  |  | Solvent  |
| Ethanol, rectified 96%  | Dana Chemicals   | Solvent  |

#### 4.2.2. Film production procedure

Wu *et al.* [1] attempted to lower the WVP of starch-alginate films by using, amongst others, SA. Their recipe was followed (Table 4-2) except that lecithin (emulsifier) was not used. The LDH,  $Mg_4Al_2(OH)_{12}CO_3 3H_2O$ , was used additionally to the recipe of Wu *et al.* [1]. The ratio of SA and LDH was varied to determine its effect on WVP and Young's modulus. The SA and LDH together are referred to as the filler, which can consist of 100% SA, 100% LDH or any ratio in between. This filler content was kept constant at 16.56% m/m of the dried film, which is similar to the amount used by Wu *et al.* [1]. Films are referred to in terms of the SA content of the filler in the Figures and by annotations such as 60SA/40LDH for a film where the filler consists of 60% SA and 40% LDH by mass.  $CO_2$  is released during the intercalation of stearate into LDH and this necessitated the use of a defoamer.

| Constituent     | Typical amounts / g | % in film solution | % in dried film |
|-----------------|---------------------|--------------------|-----------------|
| Dextrin         | 2,5                 | 2,78               | 41,39           |
| Sodium alginate | 1                   | 1,11               | 16,56           |
| Glycerol        | 1,4                 | 1,55               | 23,18           |
| SA              | 0 - 1               | 0 - 1,11           | 0 - 16,56       |
| LDH             | 1 - 0               | 1,11 - 0           | 16,56 - 0       |
| Defoamer        | 0,14                | 0,16               | 2,32            |
| Water           | 60                  | 66,64              | -               |
| Ethanol         | 24                  | 26,65              | -               |

*Table 4-2* Relative amounts of the different components in the films solutions and dry films.

Dextrin, sodium alginate and the LDH were mixed and crushed in a mortar and pestle. This procedure broke the LDH particles down by shear forces. The presence of the LDH also prevented the alginate from forming lumps during dissolution. The powdered mixture was slowly added to the water, ethanol, glycerol and SA solution at 78°C. A reaction time of one hour was used



throughout. Although the defoamer was effective, the mixtures were ultrasonicated in warm water to ensure release of all trapped bubbles still present. 8 g portions of the solutions were cast into metal rings of approximately 67 mm diameter (Fig. 4-1) to prepare samples for WVP analyses. 45 g portions were cast into 150 mm square metal holders that were placed on a non-stick silicone sheet (Silicone zone<sup>®</sup>). The samples were left to dry at room temperature and then removed by peeling. The films were cut into 45 mm diameter circles for WVP tests or punched into dumbbell shapes (6 mm wide, 35 mm gauge length, 115 mm total length) for tensile testing. Samples were conditioned for two weeks at  $23 \pm 2$  °C, 75 % RH (saturated NaCl solution [12]) prior to analysis.

One film was made with tap water to determine whether the  $Ca^{2+}$  ions would have a negative effect (by reducing the alginate solubility) or a positive effect (by cross-linking the alginate) on the WVP.



Figure 4-1 Casting of film solution into metal rings.

#### 4.2.3. Characterization

# 4.2.3.1. Fourier Transform Infrared spectroscopy (FTIR)

A Perkin Elmer Spectrum RX I FT-IR System was used to scan the infrared transmittance through a KBr (Uvasol, potassium bromide, Merck) pellet 32 times at a resolution of 2 cm<sup>-1</sup>. The averaged spectrum was background-corrected using a pure KBr pellet run under similar conditions. The pellets were prepared with approximately 2 mg of sample and 100 mg of KBr. The 2 mg powder samples were obtained by diluting the film solution with excess deionised water in order to release the insoluble LDH-SA. It was subsequently recovered by centrifugation, dried and ground. This was done in order to enable the observation of carboxylate vibrations of the intercalated stearate, which is otherwise overshadowed by the carboxylate peaks of the sodium alginate.

# 4.2.3.2. X-ray Diffraction (XRD)

The XRD analyses were done on a Siemens D500 X-ray system equipped with a 2.2 kW Cu long fine focus tube, variable slit and secondary graphite monochromator. The system is computer controlled using SIEMENS DIFFRAC <sup>Plus</sup> software. The goniometer was set to reflection mode. The films were placed on a no-background silicon (Si) wafer before placing it onto the aluminium sample holder to prevent aluminium peaks from being seen. Samples were scanned from 1 to 40° 20 with Cu K<sub>a</sub> radiation (1.5418 Å) at a speed of 0.02° 20, with a recording time of 2 s per step and generator settings of 40 kV and 30 mA.

#### 4.2.3.3. Scanning Electron Microscopy (SEM)

The film samples were freeze fractured by dipping into liquid nitrogen and then breaking the brittle film. The broken cross-sections of the films were studied. These were coated with chromium in a high resolution ion beam coater, Gatan model 681 (Warrendale, PA, USA) to prevent charge build-up due to its low conductivity. Samples were then studied with the JSM-6000F field emission scanning electron microscope (JEOL, Tokyo, Japan).



# 4.2.3.4. Optical microscopy

A drop of the film solution was placed between two microscope slides and studied under 40 times magnification with a Leica DME optical microscope with built-in digital camera.

# 4.2.3.5. Water Vapour Permeability (WVP)

The cast and dried films were cut into discs of appropriate size for the WVP cups. A Mitutoyo Digimatic Indicator was used to determine the thickness of each disc at 9 positions. The measured thicknesses varied between 130 and 140  $\mu$ m. Additional films were prepared in order to determine the effect of thickness on WVP of films of differing compositions. In all cases at least four discs per formulation were tested. Film discs were mounted on cups filled with dried silica gel (Fig. 4-2) and placed in a desiccator filled with saturated NaCl solution in contact with excess NaCl to obtain 75% relative humidity (RH) at 23 ± 2 °C [12]. Films derived from emulsions always have a shiny side (bottom) and a dull side due to accumulation of lower density wax (or fatty acid) at the top. Therefore, the measured WVP depended on which side faced which relative humidity. [3] Care was taken to always place the shiny (more hydrophilic) side facing the 0% RH side.

A WVP test of the best performing film was carried out at 38 °C/90 %RH in order to determine its performance (good, moderate or poor) according to the classification scheme of Krochta *et al.* [13]





Figure 4-2 Water vapour permeability test setup.

## 4.2.3.6. Tensile properties

Films were allowed to condition for at least two weeks before testing, so that results would be comparable in terms of the age of the samples. The thickness of the samples were tested at three positions within the middle portion of the dumbbells and averaged. The measured thicknesses ranged from 110 to 130  $\mu$ m. Samples were tested at a strain rate of 1 mm/min on a LRX Plus instrument from Lloyd Instruments, and results were analysed using Nexygen software. The software calculated the Young's moduli. Tests were performed at 25 °C at ambient humidity (30-50% RH). Three samples of each formulation were tested and averaged.

#### 4.3. Results and Discussion

#### 4.3.1. Fourier Transform Infrared spectroscopy (FTIR)

The FTIR spectrum of the LDH-SA intercalates obtained from the 60SA/40LDH film (Fig. 4-3) revealed that all the stearic acid reacted because the v(C=O) stretching vibration at 1702 cm<sup>-1</sup> was absent. The carboxylate (COO-)

asymmetric stretching vibrations were at 1539 cm<sup>-1</sup>, 1554 cm<sup>-1</sup> and 1576 cm<sup>-1</sup>, which correlates well with the carboxylate asymmetric stretching vibrations (1542 cm<sup>-1</sup>, 1557 cm<sup>-1</sup> and 1589 cm<sup>-1</sup>) obtained by Borja *et al.* [14] for meristate intercalated Mg<sub>3</sub>Al-LDH. The weak peak at 1725 cm<sup>-1</sup> was also seen by Borja *et al.* [14] at 1720 cm<sup>-1</sup> and can be attributed to the intercalation of the acid (COOH). Therefore, the same intercalation product was obtained in these aqueous film solutions as was obtained by the ion exchange of the Cl<sup>-</sup> ion in LDH-Cl by fatty acids in ethanol [14], and not the Mg/Al salt of the fatty acid. The presence of a peak at 1366 cm<sup>-1</sup>, attested to the fact that all the carbonate counter-ions did not react. Some unreacted carbonate remained no matter how large an amount of SA was used to react with the carbonate species.



*Figure 4-3* FTIR spectrum of the LDH-SA intercalates isolated from the 60SA/40LDH film solution, indicating complete ionisation and intercalation of SA together with some carbonate anions (1366 cm<sup>-1</sup>).

## 4.3.2. Water Vapour Permeability (WVP)

The water permeability of hydrophilic films depends on the films moisture content. In the WVP experiment the film separates a region of high humidity from one of low humidity. Therefore there is also a gradient in the moisture content across the film. Owing to concentration polarization, this gradient depends on the film thickness. The consequence is that, unlike hydrophobic polymer films, the WVP of hydrophilic films depends on film thickness. This was previously noted by McHugh *et al.* [15].

Fig. 4-4 shows the WVP of several films. The WVP of blank films (only dextrin, alginate and glycerol, no LDH or SA) as well as the films with only SA or only LDH were thickness dependent and the values fell on the same straight line (WVP = 0.187x + 1.01,  $R^2 = 0.9928$ , Fig. 4-4). The WVP of films with a combination of LDH and SA, however, was independent of the thickness. Therefore, the combination of LDH and SA was more successful in producing films with hydrophobic characteristics (water vapour barrier properties) than SA alone. The raw data and calculations relating to Figure 4-4 can be seen in Table A-4 and A-5 in Appendix D. The method for calculating the WVP is also described in Appendix D.





*Figure 4-4* Thickness dependence of WVP of films with no filler, SA only or LDH only showing hydrophilic tendencies and those with combinations of SA and LDH showing hydrophobic tendencies.

For the films with constant thickness and amount of filler, a broad minimum in the WVP is observed at filler compositions ranging from 80SA/20LDH to 50SA/50LDH (Fig. 4-5). These results were explained and corroborated by SEM, XRD and tensile (Young's modulus) data. The raw data and calculations relating to Figure 4-5 can be seen in Table A-6 and A-7 in Appendix D.

The film with 100% SA in the filler, showed only a 17% decrease in the WVP. This is in good agreement with the results obtained by Wu *et al.* [1] for meat patties wrapped in starch/alginate/glycerol/SA films in relation to starch/alginate/glycerol films. The replacement of only 20% of the SA by the LDH, however, caused the WVP to decrease to 80% of that of the blank film (Fig. 4-5).





*Figure 4-5* WVP measurements of constant-thickness films with fillers varying from 100SA/0LDH to 0SA/100LDH, showing a wide range of filler compositions yielding a minimum in the WVP.

When using tap water, one would expect the Ca<sup>2+</sup> and Mg<sup>2+</sup> ions to bind to the alginate, cross-linking it and thus improving the WVP, but the Ca<sup>2+</sup> ions would decrease the solubility of the alginate which could, in turn, be detrimental to film formation. The use of tap water, however, had no detrimental effects on the results, as the WVP value fell within the variation in WVP seen within the curve (Fig. 4-5). This is beneficial since the water does not have to be demineralised or deionised for large-scale applications.

Films containing other sheet-like fillers at the same mass % dosage level, i.e. talc and bentonite showed a similar WVP (Fig. 4-5). Therefore, the WVP reached a minimum due to the improved dispersion of the LDH, talc and bentonite into the polymer matrices by the SA, a conclusion which is also corroborated by SEM results. The 60SA/40LDH film which was also tested at 38°C and 90% RH, had a WVP of  $13.5 \pm 0.5$  g.mm.m<sup>-2</sup>.day<sup>-1</sup>.kPa<sup>-1</sup>, which is close to the border between the poor (10-100 g.mm.m<sup>-2</sup>.day<sup>-1</sup>.kPa<sup>-1</sup>) and moderate (0.1-10 g.mm.m<sup>-2</sup>.day<sup>-1</sup>.kPa<sup>-1</sup>) WVP regions according to the categorization of Krochta *et al.* [13]. In order to produce edible films or paper coatings with better performance in terms of WVP, the dextrin, which has poor WVP characteristics, could be replaced by polymers such as methyl cellulose, hydroxypropyl methyl cellulose, corn zein (protein), wheat gluten, poly(lactic acid) or cellulose acetate, which reside in the moderate WVP category according to Krochta *et al.* [13] Sodium alginate could also be replaced by sodium carboxymethyl cellulose in order to increase the hydrophobicity of the films.

# 4.3.3. Scanning Electron Microscopy (SEM)

The microstructures of the films with filler compositions of 100SA/0LDH through to 0SA/100LDH are shown in Figs. 4-6 (A-L). The SA could not alter the WVP characteristics of the matrix because the SA did not intimately mix with it, but formed dispersed globules (Fig. 4-6B) rather than oriented high aspect ratio sheets. The decrease in WVP (Fig. 4-5) corresponded to the presence of flat (white) plate-like structures (200-1000 nm thick and > 20  $\mu$ m long) in the microstructure. The LDH-SA intercalates agglomerated in starch or dextrin solutions alone, but the viscous surface-active sodium alginate helped to disperse it into the dextrin-alginate solutions. These structures were first seen at filler composition 80SA/20LDH (Fig. 4-6D), where the reduction in WVP occurs. Beyond the filler composition of 50SA/50LDH (Fig. 4-6G), these structures gradually disappeared and the WVP increased again to higher values. These flat structures are typical of the surfactant intercalated LDHs. [10,11] Long crevices can also be seen where the LDH-SA were pulled out of the matrix due to poor adhesion. Using, for example, 12-hydroxy stearic acid instead of SA could improve the adhesion and compatibility of the intercalated clays with the hydrophilic matrix. The more hydrophobic polymers mentioned previously could also improve adhesion to the LDH-SA intercalates, reducing pullout and increasing Young's modulus.

The films with bentonite and talc (Figs. 4-6M and 4-6N) also had an oriented structure due to the orientation of the filler particles. Wilhelm *et al.* [6] also observed the orientation of hectorite within fractured starch films. This orientation and dispersion of the fillers, therefore, account for the similar WVP results obtained for films with the same mass % LDH, talc or bentonite and SA.

LDH particles usually have sand-rose structures (Fig. 4-60). The particles consist of many intergrown smaller particles that reduce accessibility to the surface area as a whole. [11] In Fig. 4-6P a fully intact LDH particulate is shown, which was released from the sand-rose structure and was captured and oriented within the larger plate-like structure of the LDH-SA. Under the influence of the SA the crystallites were aligned and reacted to form the LDH-SA layered structure (thickness ca. 100 nm, Fig. 4-6Q), with increased accessibility to the surfaces of the particles. If completely intercalated, the 100 nm thick plates could be interpreted as 20 layers of the LDH-SA (ca. 50 Å interlayer distances according to XRD). If intercalation did not take place, the 100 nm implies 131 layers (7.6 Å interlayer distances). Clearly, exfoliation to single layers did not occur. Single layer exfoliation would not be observable by SEM. According to He et al. [16] LDH crystals are only stable when they form stacking structures of approximately 20 layers. According to XRD two phases were present, namely LDH-SA and unreacted LDH-CO<sub>3</sub>. Therefore, the plate-like structures probably consist of between 20 and 131 layers.





Figure 4-6 Scanning electron micrographs of the films.

A) Blank film. Undissolved alginic acid particles can be seen. Bar is 10  $\mu$ m.

*B*) 100SA/0LDH. Some emulsified pockets of stearic acid can be seen. Bar is 10  $\mu$ m.

*C*) 90SA/10LDH. Small, unoriented flat products of the SA-LDH reaction can be seen. Bar is 5  $\mu$ m.

D) 80SA/20LDH. The reaction product of the SA and LDH were larger and more oriented. Bar is 10  $\mu$ m.

*E*) 70SA/30LDH. The LDH-SA intercalate formed long, flat structures. Bar is 10  $\mu$ m.

*F*) 60SA/40LDH. The LDH-SA intercalate formed long, flat structures. Bar is 10  $\mu$ m.





*Figure 4-6* Scanning electron micrographs of the films.

- G) 50SA/50LDH. The LDH-SA was smaller and less oriented. Bar is 10  $\mu m.$
- H) 40SA/60LDH. Bar is 10  $\mu m.$
- I) 30SA/70LDH. Bar is 10  $\mu$ m.
- J) 20SA/80LDH. Bar is 10  $\mu$ m.
- K) 10SA/90LDH. Bar is 10  $\mu m.$
- L) 0SA/100LDH. Bar is 10  $\mu m.$







Figure 4-6 Scanning electron micrographs of the films.

- *M*) 70SA/30bentonite. The bentonite is oriented within the film. Bar is 10  $\mu$ m.
- N) 70SA/30talc. The talc is oriented within the film. Bar is 10  $\mu m.$
- O) Sand-rose structure of the LDH powder. Bar is 2  $\mu m.$
- *P*) Large magnification of 80SA/20LDH showing intact LDH particle. Bar is 0,2  $\mu$ m.
- Q) Large magnification of 60SA/40LDH showing thickness of plates. Bar is 0,1  $\mu m.$

## 4.3.4. Optical Microscopy

When looking at film solutions which had a SA/LDH ratio of about 80/20 to 40/60, "needlelike" structures (Fig. 4-7) approximately 20  $\mu$ m long could be seen. These "needles" are in actual fact plates of *ca*. 20  $\mu$ m diameter (refer to SEM section) seen from the side. They are transparent from the top. This gives an explanation for why the film solutions are white, but form clear films upon drying. In the solution the large plate-like structures are oriented randomly, scattering the light passing through it, but upon drying, the plate-like structures are all oriented horizontally (as seen by SEM also).



Figure 4-7 Optical microscope photo of the 60SA/40LDH film solution. Bar is 20  $\mu m.$ 

# 4.3.5. X-Ray Diffraction (XRD)

Depending on the amount of stearate present and the temperature employed, either a monolayer or bilayer could theoretically be intercalated (Fig. 4-8). The interlayer distance would be 32 Å for the monolayer and 52-53 Å for the bilayer. [10,17] Through molecular modelling calculations, Pospíšil *et al.* [18] reported a transition state between mono- and bilayer intercalation of octadecylammonium chloride in montmorillonite, with an interlayer distance of 47.8 Å.



*Figure 4-8* Monolayer (A) and bilayer (B) arrangement of stearate intercalated within LDH.

The XRD spectrum of the blank film (no LDH or SA) indicated a completely amorphous structure, with only a broad hump centred around  $20^{\circ} 2\theta$ . The 100SA/0LDH film had a reflection at around 40 Å (due to the unreacted stearic acid bilayer, polymorph C [19]) and a small peak at about 8.1 Å due to the formation of some alginic acid (2-fold screw axis with fiber period of 8.7 Å, [20]). Upon the addition of LDH to the SA in the film, an interlayer distance of 52 Å is reached at the filler composition of 80SA/20LDH. With an increasing amount of LDH the intensity of the basal reflection and the interlayer distance decreased (Figs. 9 and 10), indicating that some exfoliation (delamination) took place at filler compositions in the region of 60SA/40LDH to 70SA/30LDH. The exfoliation behaviour around the middle of the series can be explained in terms of the exfoliation energy. Pospíšil *et al.* [18] calculated the exfoliation energy (total



interaction energy per supercell between two layers) of octadecylammonium chloride intercalated montmorillonite. It was found to decrease dramatically for the bilayer arrangements. In the 60SA/40LDH and 70SA/30LDH films, the interlayer distance should have been the largest (> 54 Å, lowest exfoliation energy), but due to exfoliation the higher interlayer distance reflections disappeared, and a lower interlayer distance phase remained, with a lower intensity. At the filler composition of 50SA/50LDH, the bilayer structure was present once again (basal reflection at 54 Å). Upon further increasing the LDH content (decreasing SA content), the basal spacing decreased again; this time not due to exfoliation but due to a lack of SA. Stearate intercalated to form structures between mono- and bilayers.



*Figure 4-9* Variation in intensity of the basal reflection of the intercalated phase (LDH-SA) as function of filler composition. The dip in intensity indicated that exfoliation (delamination) took place.





*Figure 4-10* Variation of the interlayer distance of the intercalated phase (LDH-SA) as function of the filler composition. The dip in interlayer distance indicated that exfoliation took place, leaving only a phase with smaller interlayer distance.

Fig. 4-11 shows which crystalline phases were present in the 70SA/30LDH film at 10 minutes, 30 minutes and 60 minutes of reaction. At 10 minutes, almost no crystalline phases were present. The LDH basal reflection at 7.7 Å had a low intensity, because the LDH particles were still mostly agglomerated, settling to the bottom and not forming part of the cast film. At 30 minutes the sand-rose structures had broken down and the LDH particulates were suspended in the film solution. The 7.7 Å reflection was the most intense. Some LDH-SA had also formed at 30 minutes (52.2 Å). The 52.2 Å basal reflection had a higher intensity than the 17.9 Å (non-basal) reflection. At 60 minutes, however, the basal reflection being the most intense. This loss of intensity of the basal reflection is a strong indication that exfoliation took place between 30 and 60 minutes. It is

believed that the alginate, being a poly-anionic polysaccharide [21], aided the exfoliation of the LDH-SA without need for high shear mixing.



*Figure 4-11* The crystalline phases present in the dried film 70SA/30LDH at 10, 30 and 60 minutes of reaction, showing the relative amounts of the LDH-CO<sub>3</sub> and LDH-SA phases and the lower interlayer distance LDH-SA phase remaining after exfoliation.

# 4.3.6. Tensile properties

Only the film 0SA/100 LDH has a higher tensile strength than the blank film. The other films (which all contain SA as well) are weaker due to the lack of mechanical strength of the SA (Fig. 4-12). All the films are less ductile (lower % strain at break) than the blank film except the film 70SA/30Talc (Fig. 4-13). It is unknown why the talc increased the ductility. The complete set of mechanical properties of these films can be seen in Appendix E.



Figure 4-12 Stress at break of films as function of filler composition.



Figure 4-13 Percentage strain at break of films as function of filler composition.

The Young's moduli of our films were an order of magnitude lower and the elongation at break an order of magnitude larger than the starch films of Wilhelm *et al.* [6] because of the presence of the sodium alginate.

Fig. 4-14 shows the Young's moduli of films with different filler compositions. A maximum modulus was achieved at about 60SA/40LDH. This point probably corresponded to the minimum amount of SA needed to effectively break up the sand-rose structure in order to increase the surface area and efficiency of the reinforcing interaction between the LDH and the alginate, and possibly the dextrin. After the 60SA/40LDH point the amount of LDH available became less and thus also the reinforcing capabilities. The talc and bentonite, at the same mass %, did not have the same reinforcing effect (Fig. 4-14). For LDH we obtained a maximum increase in Young's modulus of 213% in comparison to the blank dextrin-alginate film. Wilhelm *et al.* [6] obtained only a 72% increase in modulus at 30% m/m loading of Ca<sup>2+</sup> hectorite in comparison to pristine thermoplastic starch (glycerol-plasticized). De Carvalho *et al.* [5] observed a 50%



increase in modulus of starch/calcined kaolin composites at 50 phr kaolin (50 parts kaolin per 100 parts thermoplastic starch) in comparison to the pristine thermoplastic starch. Hence, the reinforcing capability of the LDH can probably be attributed to the electrostatic interaction between the positively charged LDH layers and the anionic alginate chains, which is absent in the case of talc and bentonite.



Figure 4-14 Young's moduli of films as function of filler composition.

Leaching of Mg<sup>2+</sup> from the Mg<sub>2</sub>Al-LDH used in this study (due to the presence of the acidic SA) was not expected because Hibino *et al.* [22] found that no leaching of Mg<sup>2+</sup> cations took place in LDHs with Mg/Al ratio of 2 when treated with aqueous paramolybdate solutions (low pH), whereas substantial leaching took place in LDHs with Mg/Al ratios of 3 and 4. However, the presence of alginate might drive the leaching of some cations. When polymers with carboxylic acid groups (such as alginate) are neutralized with divalent or trivalent metal ions; the viscosity increases due to the formation of cross-links between polymer chains. [21,23,24] However, film solutions containing an equivalent amount of



magnesium stearate had a higher viscosity than LDH-SA containing films, indicating that more Mg<sup>2+</sup> were available to cross-link the alginate and to increase Young's modulus (Fig. 4-14) [23].

#### 4.3.7. XRD, tensile and WVP results revisited

The WVP, intensity of basal reflection and Young's modulus data show correlated trends (Fig. 4-15). The curve of the intensity of the basal reflection of the LDH-SA and the curve of Young's moduli crossed midway between 50% and 60% SA. Below the 60% SA point in these curves, the intensity of the basal reflection was high, indicating that no exfoliation took place; consequently the modulus dropped drastically. The opposite is true between 60 and 70% SA (the moduli were high and the intensity of the basal reflections were low, indicating exfoliation). Hence, the hypothesis that exfoliation (or delamination) of the LDH-SA caused the increase in Young's modulus was further supported.







*Figure 4-15* Comparison of WVP, Young's modulus and intensity (XRD) data as function of filler composition. WVP values of Fig. 4-4 were subtracted from 100 for this graph.

#### 4.4. Conclusions

The combination of SA and LDH improves the WVP with respect to the use of only SA or only LDH. We believe that the use of the combination of a fatty acid (rather than any other acid) and a LDH is the most beneficial for preparation of films with low WVP because the fatty acid in itself lowers the WVP, it can intercalate into the LDH to form the large plate-like barriers and *in situ* leaching of LDH cations with concomitant cross-linking of the alginate can occur. Also, exfoliation of the LDH-SA by the poly-anionic alginate was evidenced. More research needs to be done in order to determine the contributions of the two mechanisms (exfoliation vs. cross-linking) to the increased Young's modulus (increased stiffness) and decreased WVP, but from qualitative viscosity



observations it seems that cross-linking due to leaching of Mg<sup>2+</sup> from the LDH plays only a minor role.

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# Chapter 5

# **Conclusions and Recommendations**

This section describes some general conclusions regarding the success of this research; more specific conclusions are given within each chapter.

# 5.1. Conclusions

A technique for intercalating stearate anions into Mg<sub>4</sub>Al<sub>2</sub>(OH)<sub>12</sub>CO<sub>3</sub>·3H<sub>2</sub>O (LDH-CO<sub>3</sub>) was developed. The intercalation reaction mechanism consisted of an acidbase exchange between stearic acid (or any other fatty acid) and the carbonate anion of the LDH-CO<sub>3</sub>. The use of surfactants was beneficial, preventing agglomeration during the reaction and in cases where LDO (calcined LDH) was used, the surfactant improved the yield of the stearate intercalated LDH (LDH-SA) and prevented the formation of Mg/Al salts of the fatty acids. The newly developed method gave better intercalation results in comparison to some wellknown literature methods.

The anionic polymer poly(vinyl sulfonate) intercalated into  $LDH-CO_3$  in the presence of stearic acid. The stearic acid intercalated as stearate anions, which was exchanged by the polymeric anion. This is an easy and facile way to produce nanocomposites. The anionic polymer and LDH interacts on the molecular level and the thicknesses of the resulting plate-like structures are in the nanometre range.

The stearate intercalated LDH (LDH-SA) successfully reduced the water vapour permeability of dextrin-alginate based films. In addition the Young's modulus increased, showing that the LDH-SA plate-like structures (which had thicknesses in the range of 100 nm), had reinforcing interactions with the polymer chains.

#### 5.2. Recommendations for future research

During this research project aqueous film-forming solutions were used and tested as paper coatings. The solutions tended to penetrate deep into the fibrous matrix of the paper, requiring a high loading of solution before forming a continuous barrier film on the paper. This problem could be overcome by forming a thermoplastic starch-alginate blend filled with the LDH-SA. The thermoplastic blend could be prepared in the method developed by Souza *et al.* [1]. The intercalation reaction would then take place *in situ* between the molten SA and the LDH as in the method developed by Carlino *et al* [2,3]. The thermoplastic blend could then be used for melt paper coating.

The intercalation reaction of stearic acid into the LDH-CO<sub>3</sub> could also be done *in situ* during the emulsion polymerization of polymers such as polystyrene, methyl methacrylate, polyvinyl chloride and many more, which could lead to the formation of exfoliated nanocomposites. Furthermore, the system of the PVS ion exchanging with stearate to intercalate, could be used as a model of intercalating other poly-anionic species, such as DNA into the LDH layers, where it could be protected and used as carriers for gene therapy.

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# Appendices

# Appendix A

# List of patents, publications and conference proceedings emanating from this research

# 1. Provisional patent

A provisional patent with title "Carboxylic acid intercalated layered double hydroxides" was filed in the Republic of South Africa on 6April 2005. The preliminary reference number is V16742.

# 2. Submitted articles

- 2.1. Landman EP, Focke WW, Stearate Intercalated Layered Double Hydroxides: a Comparison of Methods, *Journal of Materials Science*.
- 2.2. Landman EP, Focke WW, Stearate Intercalated Layered Double Hydroxides: Effect on the Physical Properties of Dextrin-Alginate Films, Journal of Materials Science.
- 2.3. Landman EP, Focke WW, Poly(vinyl sulfonate) Intercalation into Stearate Intercalated Layered Double Hydroxides, Journal of Colloid and Interface Science.

# 3. Conference Contributions

# 3.1. Invited Paper

Landman EP and Focke WW, **Modification of Hydrotalcite for use in Starch Nanocomposites – Exploring Alternatives**, proceedings of the 37<sup>th</sup> National Convention of the South African Chemical Institute, Pretoria, 4-9 July 2004, p 138.

# 3.2. Poster

Landman EP, Focke WW, **Modification of Hydrotalcite for use in Starch Nanocomposites**, proceedings of the 2<sup>nd</sup> International Conference of the African Materials Research Society, Johannesburg, 8-11 December 2003, p38.

# Appendix B

# XRF analysis of the layered double hydroxide

Table A-1 gives the XRF analysis of the LDH used in this study. It shows that the Mg/AI atomic ratio is 2.

| Oxide species                  | %     | Oxide species                  | %      |
|--------------------------------|-------|--------------------------------|--------|
| MgO                            | 34,54 | K <sub>2</sub> O               | 0,00   |
| Al <sub>2</sub> O <sub>3</sub> | 21,78 | P <sub>2</sub> O <sub>5</sub>  | 0,00   |
| SiO <sub>2</sub>               | 0,98  | Cr <sub>2</sub> O <sub>3</sub> | 0,00   |
| TiO <sub>2</sub>               | 0,00  | NiO                            | 0,08   |
| Fe <sub>2</sub> O <sub>3</sub> | 0,16  | V <sub>2</sub> O <sub>5</sub>  | 0,00   |
| MnO                            | 0,01  | ZrO <sub>2</sub>               | 0,01   |
| CaO                            | 0,47  | LOI                            | 41,97  |
| Na₂O                           | 0,00  | Total                          | 100,01 |

Table A-1 XRF analysis of the LDH used in this study.

# Appendix C

# XRD raw data for internal standard analyses

Each method was repeated twice. For each sample an XRD analysis was done in order to determine the intensity (in counts per second) of the reflections at around 50 Å (LDH-SA), 7,6 Å (LDH-CO<sub>3</sub>) and 9,3 Å (talc). The intensity ratio of 50 Å/9,3 Å and 7,6 Å/9,3 Å was determined for each sample. The two intensity ratios for the two samples of the same method were averaged. The standard deviation of the average was calculated by dividing the standard deviation of the two intensity ratios by the square root of 2 (amount of repetitions of each method). The raw data, calculated averages and standard deviations are given in Table A-2 (for the 50 Å phase) and Table A-3 (for the 7,6 Å phase).

| Table A-2 XRD intensity data for the amount of the 50 / | Å phase (LDH-SA) present |
|---|--------------------------|
| in the products of the different methods.               |                          |

| Water 3849 1189 3,2 4,0                   | 0,8 |
|---|-----|
|   |     |
| <i>Water</i> 4948 1026 4,8                | 0.0 |
| <i>Calcined-Water</i> 5951 2029 2,9 3,2   | 0,3 |
| <i>Calcined-Water</i> 4122 1170 3,5       |     |
| <i>Ethanol-water</i> 2908 1077 2,7 3,0    | 0,3 |
| <i>Ethanol-water</i> 3475 1053 3,3        |     |
| <i>Ethanol</i> 0 1147 0 0                 | 0   |
| <i>Ethanol</i> 0 1265 0                   |     |
| <b>SDS-water</b> 8360 1433 5,8 5,0        | 0,8 |
| <b>SDS-water</b> 4683 1115 4,2            |     |
| <b>SDS-water-24 h</b> 12457 1483 8,4 7,6  | 0,8 |
| <b>SDS-water-24 h</b> 9010 1327 6,8       |     |
| Calcined-SDS-water 8123 979 8,3 7,6       | 0,7 |
| <b>Calcined-SDS-water</b> 7245 1048 6,9   |     |
| Calcined-SDS-water-24 h 16104 2013 8 8    | 0,8 |
| Calcined-SDS-water-24 h 1564              |     |
| <i>Glycerol-water</i> 1624 1146 1,4 1,2   | 0,2 |
| <i>Glycerol-water</i> 1708 1612 1,0       |     |
| Calcined-glycerol-water 2867 1326 2,2 2,3 | 0,1 |
| Calcined-glycerol-water 2855 1181 2,4     |     |
| Calcined-Na stearate 412 1003 0,41 0,4    | 0,1 |
| <i>Calcined-Na stearate</i> 516 1322 0,39 |     |
| Carlino melt 1086 976 1,1 1,2             | 0,1 |
| <i>Carlino melt</i> 1215 934 1,3          |     |
| <b>Reference</b> 0 1405 0 0               | 0   |
| <b>Reference</b> 0 1293 0                 |     |

\* Intensity of the reflection in the region of 50 Å.

\*\* Intensity of the talc reflection at 9,3 Å.
*Table A-3* XRD intensity data for the amount of the 7,6 Å phase (LDH-CO<sub>3</sub>) present in the products of the different methods.

| Method                  | I <sub>7,6 Å</sub> | I <sub>9,3 Å</sub> * | I <sub>7,6 Å</sub> / I <sub>9,3 Å</sub> | Average<br>I <sub>7,6 Å</sub> / I <sub>9,3 Å</sub> | Standard<br>deviation<br>of average<br>I <sub>7,6 Å</sub> / I <sub>9,3 Å</sub> |
|-------------------------|--------------------|----------------------|---|--|--|
| Water                   | 2021               | 1189                 | 1,7                                     | 1,9  | 0,2  |
| Water                   | 2153               | 1026                 | 2,1                                     |  |  |
| Calcined-Water          | 137                | 2029                 | 0,0675                                  | 0,0679   | 0,0003   |
| Calcined-Water          | 80                 | 1170                 | 0,0683                                  |  |  |
| Ethanol-water           | 1509               | 1077                 | 1,4                                     | 1,7  | 0,3  |
| Ethanol-water           | 2110               | 1053                 | 2,0                                     |  |  |
| Ethanol                 | 4245               | 1147                 | 3,7                                     | 3,4  | 0,3  |
| Ethanol                 | 3919               | 1265                 | 3,1                                     |  |  |
| SDS-water               | 2577               | 1433                 | 1,8                                     | 2,1  | 0,3  |
| SDS-water               | 2675               | 1115                 | 2,4                                     |  |  |
| SDS-water-24 h          | 1630               | 1483                 | 1,1                                     | 1,3  | 0,2  |
| SDS-water-24 h          | 1989               | 1327                 | 1,5                                     |  |  |
| Calcined-SDS-water      | 105                | 979                  | 0,11                                    | 0,09   | 0,02   |
| Calcined-SDS-water      | 76                 | 1048                 | 0,07                                    |  |  |
| Calcined-SDS-water-24 h | 118                | 2013                 | 0,06                                    | 0,08   | 0,02   |
| Calcined-SDS-water-24 h | 159                | 1564                 | 0,10                                    |  |  |
| Glycerol-water          | 1029               | 1146                 | 0,90                                    | 0,86   | 0,04   |
| Glycerol-water          | 1327               | 1612                 | 0,82                                    |  |  |
| Calcined-glycerol-water | 28                 | 1326                 | 0,02                                    | 0,03   | 0,01   |
| Calcined-glycerol-water | 53                 | 1181                 | 0,04                                    |  |  |
| Calcined-Na stearate    | 148                | 1003                 | 0,15                                    | 0,13   | 0,02   |
| Calcined-Na stearate    | 143                | 1322                 | 0,11                                    |  |  |
| Carlino melt            | 1466               | 976                  | 1,5                                     | 1,4  | 0,1  |
| Carlino melt            | 1213               | 934                  | 1,3                                     |  |  |
| Reference               | 3229               | 1405                 | 2,3                                     | 2,0  | 0,3  |
| Reference               | 2197               | 1293                 | 1,7                                     |  |  |

\* Intensity of the talc reflection at 9,3 Å.



# Appendix D

### Water vapour permeability raw data and equations

Origin of the data in Chapter 4, Figure 4:

5 Films of each formulation were tested. The thicknesses of the films are given in Table A-4 (T1-T13). The average thickness (T) of each film was calculated as well as the standard deviation (s(T)) and the relative standard deviation of the average thickness (rs(T), Equation E1).

$$rs(T) = \frac{s(T)}{T}$$
 E1

The masses (*m1-m9*) of the cups, filled with dry silica gel and sealed with the films, were measured at different time intervals (Table A-5). The mass was plotted as a function of time. The slope (*S*, Equation E2) and the standard deviation of the slope (*s*(*S*), Equation E3) of the mass vs. time plot were determined with the *linest* function of Microsoft Excel<sup>®</sup> (E2 and E3). The relative standard deviation in the slope was determined in the same way as in Equation E1 for the relative standard deviation in the thickness.

$$S = index(linest(y values, x values),1)$$
E2 $s(S) = index(linest(y values, x values,true,true),2)$ E3

The water vapour permeability ( $WVP_x$ ) of the individual films was determined by Equation E4. The WVPs of the 5 individual films of each formulation was averaged (Av WVP).

$$WVP_x = \frac{S \times T}{A \times P} = \frac{S \times T}{\Pi R^2 \times P}$$
 E4

Where  $A = 0,0018 \text{ m}^2$  (Area of the opening of the cup) And  $P = p_o - p_i = 2,3768 \text{ kPa}^{a,b}$ .

*P* is the difference in the water vapour pressure on the outside ( $p_o$ ) and the inside ( $p_i$ ) of the cup. The relative humidity (*RH*) is assumed to be 0% on the inside (silica gel) and 75% on the outside (excess NaCl in contact with saturated solution of NaCl). The actual *RH*s were not measured. The relationship between the water vapour pressure (p) at a certain temperature and the *RH* is given by Equation E5.

$$p = \frac{RH \times p_w}{100} \quad [a]$$
 E5

Where  $p_w = 3.1690$  kPa, the water vapour pressure at 25 °C for pure water.

<sup>&</sup>lt;sup>a</sup> A. WEXLER, in "Handbook of Physics and Chemistry", 79<sup>th</sup> edition, edited by D.R. Lide (CRC Press, Boca Raton, 1998) p. **15-**25.

<sup>&</sup>lt;sup>b</sup> Vapor pressure of water from 0 to 370 °C, "Handbook of Physics and Chemistry", 79<sup>th</sup> edition, edited by D.R. Lide (CRC Press, Boca Raton, 1998) p. **6**-8.

The error in the WVP ( $E_x$ ) for the individual films was calculated by Equation E6, which was derived from the general Equation E7 on the propagation of errors [c]. The pooled error (*PE*) of the *Av WVP* was determined by Equation E8.

$$E_{x} = \sqrt{WVP^{2} \times \{rs(S)^{2} + rs(T)^{2} + 4ru(R)^{2}\}}$$
 E6

Where

R = 0,024 m (radius of the opening of the cup)

u(R) = 0,001 m (uncertainty in the radius measurement, measured with a ruler) ru(R) = u(R)/R = 0,04 (relative uncertainty in the radius measurement)

$$E_x^2 = \left(\frac{\partial WVP}{\partial S}\right)^2 \times s(S)^2 + \left(\frac{\partial WVP}{\partial T}\right)^2 \times s(T)^2 + \left(\frac{\partial WVP}{\partial R}\right)^2 \times u(R)^2 \quad [C] \quad E7$$

In Equation E7 the contribution of the error in the difference in the water vapour pressure (P) is assumed to be zero because the actual water vapour pressures and the errors therein were not measured.

$$PE = \frac{\sqrt{E_1^2 + E_2^2 + E_3^2 + E_4^2 + E_5^2}}{\sqrt{5}}$$
E8

The same calculations were done for the films of which the *WVP* data are shown in Chapter 4, Figure 5. The thickness and mass data and calculated values are shown separately in Tables A-6 and A-7 because of the different time intervals of taking measurements. A different cup size was also used and the relevant constants are as follows:

R = 0,0181 mu(R) = 0,0005 m (measured with a vernier) ru(R) = 0,027 $A = 0,0010 \text{ m}^2$ 

<sup>&</sup>lt;sup>c</sup> H.D. YOUNG, Statistical Treatment of Experimental Data, (McGraw-Hill Book Company, New York, 1962) p. 96-98.

For the sample tested at 38 °C/90% *RH*  $p_o$ - $p_i$  is 5,9668 kPa<sup>a,b</sup> and  $p_w$  is 6,6298 kPa at 38 °C and A = 0,0010 m<sup>2</sup>.



| Table A-4 Thickness | data fo | r films  | relating to | Chapter 4. | Figure 4.  |
|---------------------|---------|----------|-------------|------------|------------|
|                     | autu io | 1 111110 | roluting to | onuplor i, | i iguio i. |

|            | <i>T1</i> /mm | <i>T2</i> /mm | <i>T3</i> /mm | <i>T4</i> /mm | <i>T5</i> /mm | <i>T6</i> /mm | <i>T7</i> /mm | <i>T8</i> /mm | <i>T9</i> /mm | <i>T10/</i> mm | <i>T11/</i> mm | <i>T12</i> /mm | <i>T13</i> /mm | T/mm  | s(T)/mm | rs(T) |
|------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|----------------|----------------|----------------|----------------|-------|---------|-------|
| Blank      |               |               |               |               |               |               |               |               |               |                |                |                |                |       |         |       |
| 1          | 0,061         | 0,061         | 0,059         | 0,056         | 0,051         | 0,052         | 0,056         | 0,057         | 0,055         | 0,058          | 0,053          | 0,056          | 0,058          | 0,056 | 0,00087 | 0,015 |
| 2          | 0,059         | 0,063         | 0,066         | 0,065         | 0,064         | 0,065         | 0,062         | 0,060         | 0,063         | 0,062          | 0,064          | 0,066          | 0,064          | 0,063 | 0,00059 | 0,009 |
| 3          | 0,061         | 0,060         | 0,064         | 0,064         | 0,065         | 0,060         | 0,057         | 0,060         | 0,064         | 0,061          | 0,063          | 0,064          | 0,062          | 0,062 | 0,00065 | 0,010 |
| 4          | 0,060         | 0,060         | 0,058         | 0,057         | 0,058         | 0,057         | 0,060         | 0,061         | 0,058         | 0,066          | 0,058          | 0,058          | 0,061          | 0,059 | 0,00067 | 0,011 |
| 5          | 0,061         | 0,063         | 0,062         | 0,058         | 0,059         | 0,057         | 0,061         | 0,062         | 0,059         | 0,063          | 0,062          | 0,059          | 0,063          | 0,061 | 0,00057 | 0,009 |
| LDH alone  |               |               |               |               |               |               |               |               |               |                |                |                |                |       |         |       |
| 1          | 0,089         | 0,113         | 0,075         | 0,077         | 0,108         | 0,157         | 0,120         | 0,134         | 0,108         | 0,122          | 0,092          | 0,132          | 0,111          | 0,111 | 0,00651 | 0,059 |
| 2          | 0,155         | 0,156         | 0,127         | 0,153         | 0,152         | 0,147         | 0,147         | 0,173         | 0,165         | 0,146          | 0,158          | 0,161          | 0,163          | 0,154 | 0,00313 | 0,020 |
| 3          | 0,130         | 0,150         | 0,136         | 0,152         | 0,153         | 0,165         | 0,167         | 0,151         | 0,163         | 0,138          | 0,161          | 0,180          | 0,170          | 0,155 | 0,00402 | 0,026 |
| 4          | 0,175         | 0,176         | 0,148         | 0,130         | 0,164         | 0,185         | 0,136         | 0,138         | 0,153         | 0,185          | 0,133          | 0,132          | 0,141          | 0,154 | 0,00579 | 0,038 |
| 5          | 0,135         | 0,114         | 0,126         | 0,163         | 0,145         | 0,130         | 0,133         | 0,129         | 0,118         | 0,133          | 0,145          | 0,140          | 0,119          | 0,133 | 0,00367 | 0,028 |
| SA alone   |               |               |               |               |               |               |               |               |               |                |                |                |                |       |         |       |
| 1          | 0,144         | 0,134         | 0,128         | 0,126         | 0,134         | 0,131         | 0,147         | 0,145         | 0,132         | 0,133          | 0,129          | 0,139          | 0,142          | 0,136 | 0,00193 | 0,014 |
| 2          | 0,136         | 0,143         | 0,145         | 0,138         | 0,143         | 0,153         | 0,163         | 0,153         | 0,136         | 0,136          | 0,145          | 0,147          | 0,152          | 0,145 | 0,00227 | 0,016 |
| 3          | 0,109         | 0,100         | 0,106         | 0,112         | 0,118         | 0,125         | 0,131         | 0,127         | 0,107         | 0,122          | 0,109          | 0,115          | 0,116          | 0,115 | 0,00254 | 0,022 |
| 4          | 0,115         | 0,109         | 0,110         | 0,123         | 0,110         | 0,124         | 0,127         | 0,137         | 0,119         | 0,118          | 0,120          | 0,116          | 0,125          | 0,119 | 0,00219 | 0,018 |
| 5          | 0,118         | 0,118         | 0,114         | 0,112         | 0,115         | 0,118         | 0,122         | 0,133         | 0,121         | 0,121          | 0,107          | 0,117          | 0,123          | 0,118 | 0,00173 | 0,015 |
| 1:1 LDH:SA |               |               |               |               |               |               |               |               |               |                |                |                |                |       |         |       |
| 1          | 0,103         | 0,097         | 0,102         | 0,115         | 0,123         | 0,126         | 0,132         | 0,098         | 0,119         | 0,160          | 0,098          | 0,098          | 0,091          | 0,112 | 0,00538 | 0,048 |
| 2          | 0,111         | 0,086         | 0,100         | 0,088         | 0,085         | 0,077         | 0,071         | 0,085         | 0,097         | 0,086          | 0,136          | 0,115          | 0,074          | 0,093 | 0,00511 | 0,055 |
| 3          | 0,086         | 0,090         | 0,085         | 0,087         | 0,079         | 0,082         | 0,085         | 0,090         | 0,082         | 0,092          | 0,100          | 0,106          | 0,083          | 0,088 | 0,00211 | 0,024 |
| 4          | 0,167         | 0,131         | 0,105         | 0,085         | 0,113         | 0,119         | 0,149         | 0,105         | 0,084         | 0,095          | 0,103          | 0,095          | 0,093          | 0,111 | 0,00690 | 0,062 |
| 5          | 0,095         | 0,118         | 0,088         | 0,096         | 0,091         | 0,096         | 0,113         | 0,093         | 0,113         | 0,130          | 0,101          | 0,124          | 0,122          | 0,106 | 0,00397 | 0,037 |
| 2:1 LDH:SA |               |               |               |               |               |               |               |               |               |                |                |                |                |       |         |       |
| 1          | 0,082         | 0,118         | 0,109         | 0,116         | 0,101         | 0,103         | 0,075         | 0,073         | 0,076         | 0,077          | 0,092          | 0,116          | 0,093          | 0,095 | 0,00471 | 0,050 |
| 2          | 0,079         | 0,082         | 0,103         | 0,100         | 0,091         | 0,087         | 0,088         | 0,085         | 0,081         | 0,080          | 0,095          | 0,087          | 0,094          | 0,089 | 0,00212 | 0,024 |
| 3          | 0,095         | 0,112         | 0,102         | 0,126         | 0,107         | 0,108         | 0,102         | 0,102         | 0,106         | 0,104          | 0,100          | 0,101          | 0,094          | 0,105 | 0,00225 | 0,022 |
| 4          | 0,133         | 0,092         | 0,097         | 0,093         | 0,103         | 0,132         | 0,106         | 0,097         | 0,108         | 0,092          | 0,097          | 0,100          | 0,106          | 0,104 | 0,00377 | 0,036 |
| 5          | 0,106         | 0,103         | 0,112         | 0,120         | 0,126         | 0,146         | 0,130         | 0,107         | 0,114         | 0,115          | 0,134          | 0,122          | 0,120          | 0,120 | 0,00339 | 0,028 |



#### Table A-5 Mass increase data and calculations for films relating to Chapter 4, Figure 4.

|               | t/day | 0            | 0,1          | 0,2          | 0,9          | 1,0          | 2,0          | 3,0          | 4,0          | 7,0          |           |                      |       |  |                |           |    |
|---------------|-------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-----------|----------------------|-------|--|----------------|-----------|----|
|               |       | <i>m1</i> /g | <i>m2/</i> g | <i>m3/</i> g | <i>m4</i> /g | <i>m5</i> /g | <i>m6</i> /g | <i>m7</i> /g | <i>m8</i> /g | <i>m9</i> /g | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | E <sub>x</sub> | Av<br>WVP | PE |
| Blank         | 1     | 139,3552     | 139,4242     | 139,4811     | 140,2618     | 140,3950     | 141,4589     | 142,3971     | 143,1735     | 145,2979     | 0,87      | 0,0337               | 0,04  | 11   | 1              | 12        | 1  |
|               | 2     | 139,2650     | 139,3264     | 139,3768     | 140,133      | 140,2557     | 141,2504     | 142,1510     | 142,8899     | 144,8819     | 0,83      | 0,0327               | 0,04  | 12   | 1              |           |    |
|               | 3     | 139,2010     | 139,2737     | 139,3324     | 140,1499     | 140,2855     | 141,3015     | 142,2811     | 143,0597     | 145,1734     | 0,88      | 0,0348               | 0,04  | 13   | 1              |           |    |
|               | 4     | 139,2622     | 139,3393     | 139,3971     | 140,2343     | 140,3704     | 141,4012     | 142,3324     | 143,0798     | 145,1268     | 0,86      | 0,0377               | 0,04  | 12   | 1              |           |    |
|               | 5     | 136,8620     | 136,9333     | 136,9908     | 137,8023     | 137,9309     | 138,9457     | 139,8624     | 140,5899     | 142,5820     | 0,84      | 0,0370               | 0,04  | 12   | 1              |           |    |
| LDH<br>alone  | 1     | 139,4256     | 139,5167     | 139,5940     | 140,4959     | 140,6331     | 141,6984     | 142,6654     | 143,4380     | 145,4351     | 0,88      | 0,0450               | 0,05  | 23   | 3              | 28        | 3  |
|               | 2     | 140,3237     | 140,3925     | 140,4495     | 141,2445     | 141,3808     | 142,3624     | 143,2521     | 144,0026     | 146,0535     | 0,84      | 0,0328               | 0,04  | 30   | 3              |           |    |
|               | 3     | 140,4868     | 140,5627     | 140,6284     | 141,4686     | 141,5977     | 142,6143     | 143,5011     | 144,2244     | 146,2302     | 0,84      | 0,0379               | 0,05  | 30   | 3              |           |    |
|               | 4     | 140,2640     | 140,3444     | 140,4171     | 141,2742     | 141,4027     | 142,3702     | 143,2850     | 144,0579     | 146,1224     | 0,86      | 0,0355               | 0,04  | 30   | 3              |           |    |
|               | 5     | 140,0224     | 140,1078     | 140,1814     | 141,0032     | 141,1408     | 142,1541     | 143,0556     | 143,7822     | 145,7727     | 0,84      | 0,0384               | 0,05  | 26   | 3              |           |    |
| SA<br>alone   | 1     | 137,1115     | 137,1200     | 137,225      | 138,0179     | 138,1360     | 139,1042     | 140,0090     | 140,7353     | 142,7846     | 0,83      | 0,0325               | 0,04  | 26   | 2              | 24        | 2  |
|               | 2     | 139,9684     | 140,0236     | 140,0771     | 140,8523     | 140,9787     | 141,9294     | 142,7860     | 143,5004     | 145,4594     | 0,81      | 0,0323               | 0,04  | 27   | 3              |           |    |
|               | 3     | 139,9268     | 140,0015     | 140,0691     | 140,9022     | 141,0331     | 142,0171     | 142,9162     | 143,6497     | 145,6274     | 0,84      | 0,0374               | 0,04  | 22   | 2              |           |    |
|               | 4     | 140,1941     | 140,2665     | 140,3300     | 141,1496     | 141,284      | 142,2798     | 143,1811     | 143,9231     | 145,9461     | 0,84      | 0,0358               | 0,04  | 23   | 2              |           |    |
|               | 5     | 140,2950     | 140,3668     | 140,4312     | 141,2147     | 141,3395     | 142,3173     | 143,1955     | 143,9281     | 145,9365     | 0,83      | 0,0331               | 0,04  | 23   | 2              |           |    |
| 1:1<br>LDH:SA | 1     | 139,7316     | 139,7411     | 139,7512     | 139,9302     | 139,9608     | 140,2381     | 140,5555     | 140,851      | 141,9580     | 0,315     | 0,0092               | 0,03  | 8  | 1              | 7         | 1  |
|               | 2     | 140,0043     | 140,0151     | 140,0257     | 140,2194     | 140,2500     | 140,5334     | 140,8203     | 141,0871     | 141,9858     | 0,284     | 0,0025               | 0,01  | 6  | 1              |           |    |
|               | 3     | 139,3577     | 139,2721     | 139,3856     | 139,6194     | 139,6563     | 139,9716     | 140,3181     | 140,6289     | 141,6933     | 0,339     | 0,0052               | 0,02  | 7  | 1              |           |    |
|               | 4     | 139,3222     | 139,3320     | 139,3434     | 139,5163     | 139,5450     | 139,8020     | 140,0908     | 140,3572     | 141,1830     | 0,268     | 0,0029               | 0,01  | 7  | 1              |           |    |
|               | 5     | 137,1644     | 137,1729     | 137,1827     | 137,3484     | 137,3746     | 137,6031     | 137,8575     | 138,0961     | 138,8862     | 0,246     | 0,0031               | 0,01  | 6  | 1              |           |    |
| 2:1<br>LDH:SA | 1     | 140,0288     | 140,0458     | 140,0636     | 140,3463     | 140,3917     | 140,8017     | 141,2405     | 141,6597     | 142,9410     | 0,419     | 0,0034               | 0,01  | 9  | 1              | 9         | 1  |
|               | 2     | 139,3650     | 139,3795     | 139,3947     | 139,6615     | 139,7032     | 140,1085     | 140,5687     | 140,9926     | 142,3636     | 0,431     | 0,0066               | 0,02  | 9  | 1              |           |    |
|               | 3     | 140,1331     | 140,1462     | 140,1606     | 140,3972     | 140,4349     | 140,7748     | 141,1478     | 141,4882     | 142,6018     | 0,354     | 0,0036               | 0,01  | 9  | 1              |           |    |
|               | 4     | 140,0244     | 140,0380     | 140,0519     | 140,3019     | 140,3421     | 140,7019     | 141,0646     | 141,4494     | 142,6036     | 0,370     | 0,0039               | 0,01  | 9  | 1              |           |    |
| _             | 5     | 139,5315     | 139,5426     | 139,5557     | 139,7699     | 139,8042     | 140,1187     | 140,4883     | 140,8465     | 141,9530     | 0,347     | 0,0060               | 0,02  | 10   | 1              |           |    |



| 100SA/0LDH | <i>T1</i> /mm | <i>T2</i> /mm | <i>T3</i> /mm | <i>T4</i> /mm | <i>T5</i> /mm | <i>T6/</i> mm | <i>T7</i> /mm | <i>T8</i> /mm | <i>T9</i> /mm | <i>T∕</i> mm | s( <i>T)</i> /mm | rs(T) |
|------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|------------------|-------|
| 1          | 0,139         | 0,147         | 0,136         | 0,132         | 0,138         | 0,147         | 0,147         | 0,137         | 0,144         | 0,141        | 0,00187          | 0,013 |
| 2          | 0,123         | 0,137         | 0,141         | 0,134         | 0,144         | 0,144         | 0,137         | 0,135         | 0,137         | 0,137        | 0,00212          | 0,015 |
| 3          | 0,143         | 0,136         | 0,132         | 0,126         | 0,130         | 0,138         | 0,143         | 0,135         | 0,14          | 0,136        | 0,00194          | 0,014 |
| 4          | 0,119         | 0,125         | 0,131         | 0,13          | 0,129         | 0,121         | 0,124         | 0,128         | 0,118         | 0,125        | 0,00162          | 0,013 |
| 90SA/10LDH |               |               |               |               |               |               |               |               |               |              |                  |       |
| 1          | 0,143         | 0,141         | 0,136         | 0,134         | 0,141         | 0,145         | 0,149         | 0,146         | 0,147         | 0,142        | 0,00167          | 0,012 |
| 2          | 0,131         | 0,125         | 0,117         | 0,124         | 0,127         | 0,126         | 0,134         | 0,135         | 0,129         | 0,128        | 0,00184          | 0,014 |
| 3          | 0,141         | 0,135         | 0,132         | 0,144         | 0,135         | 0,139         | 0,146         | 0,147         | 0,144         | 0,140        | 0,00180          | 0,013 |
| 4          | 0,141         | 0,133         | 0,139         | 0,138         | 0,145         | 0,144         | 0,145         | 0,142         | 0,15          | 0,142        | 0,00164          | 0,012 |
| 80SA/20LDH |               |               |               |               |               |               |               |               |               |              |                  |       |
| 1          | 0,126         | 0,109         | 0,111         | 0,135         | 0,13          | 0,118         | 0,124         | 0,131         | 0,131         | 0,124        | 0,00309          | 0,025 |
| 2          | 0,132         | 0,147         | 0,141         | 0,102         | 0,144         | 0,15          | 0,142         | 0,114         | 0,132         | 0,134        | 0,00536          | 0,040 |
| 3          | 0,139         | 0,158         | 0,156         | 0,106         | 0,148         | 0,163         | 0,147         | 0,122         | 0,15          | 0,143        | 0,00613          | 0,043 |
| 4          | 0,15          | 0,179         | 0,149         | 0,142         | 0,172         | 0,195         | 0,188         | 0,153         | 0,161         | 0,165        | 0,00628          | 0,038 |
| 70SA/30LDH |               |               |               |               |               |               |               |               |               |              |                  |       |
| 10 min     | 0.400         | 0.400         | 0 4 0 7       | 0.400         | 0.4.44        | 0.404         | 0.400         | 0.404         | 0.404         | 0.400        | 0.00470          | 0.040 |
| 1          | 0,123         | 0,132         | 0,137         | 0,129         | 0,141         | 0,134         | 0,136         | 0,134         | 0,134         | 0,133        | 0,00170          | 0,013 |
| 2          | 0,132         | 0,14          | 0,132         | 0,126         | 0,152         | 0,137         | 0,132         | 0,133         | 0,14          | 0,136        | 0,00249          | 0,018 |
| 3          | 0,128         | 0,13          | 0,132         | 0,126         | 0,14          | 0,136         | 0,143         | 0,132         | 0,14          | 0,134        | 0,00198          | 0,015 |
| 4          | 0,12          | 0,116         | 0,112         | 0,117         | 0,115         | 0,116         | 0,126         | 0,121         | 0,122         | 0,118        | 0,00142          | 0,012 |
| 30 min     |               |               |               |               |               |               |               |               |               |              |                  |       |
| 1          | 0,15          | 0,144         | 0,133         | 0,141         | 0,152         | 0,152         | 0,148         | 0,145         | 0,15          | 0,146        | 0,00206          | 0,014 |
| 2          | 0,156         | 0,105         | 0,111         | 0,147         | 0,125         | 0,131         | 0,155         | 0,157         | 0,152         | 0,138        | 0,00676          | 0,049 |
| 3          | 0,135         | 0,132         | 0,119         | 0,125         | 0,124         | 0,136         | 0,136         | 0,136         | 0,145         | 0,132        | 0,00266          | 0,020 |
| 4          | 0,116         | 0,122         | 0,120         | 0,119         | 0,123         | 0,123         | 0,121         | 0,121         | 0,124         | 0,121        | 0,00082          | 0,007 |
| 70SA/30LDH |               |               |               |               |               |               |               |               |               |              |                  |       |
| 60 min     |               |               |               |               |               |               |               |               |               |              |                  |       |
| 1          | 0,131         | 0,141         | 0,128         | 0,123         | 0,131         | 0,135         | 0,132         | 0,127         | 0,135         | 0,131        | 0,00175          | 0,013 |
| 2          | 0,133         | 0,14          | 0,129         | 0,128         | 0,131         | 0,132         | 0,136         | 0,134         | 0,132         | 0,133        | 0,00121          | 0,009 |
| 3          | 0,138         | 0,132         | 0,127         | 0,128         | 0,129         | 0,133         | 0,134         | 0,137         | 0,136         | 0,133        | 0,00133          | 0,010 |
| 4          | 0,12          | 0,127         | 0,114         | 0,111         | 0,121         | 0,122         | 0,125         | 0,117         | 0,128         | 0,121        | 0,00192          | 0,016 |



| Table A-6 contin | ued Thick     | ness data     | for films re  | elating to C  | hapter 4, I   | Figure 5.     |                |               |  |              |                  |       |
|------------------|---------------|---------------|---------------|---------------|---------------|---------------|----------------|---------------|--|--------------|------------------|-------|
|                  | <i>T1</i> /mm | <i>T2</i> /mm | <i>T3</i> /mm | <i>T4</i> /mm | <i>T5</i> /mm | <i>T6/</i> mm | <i>T7</i> /mm  | <i>T8</i> /mm | <b>T9/mm</b>   | <i>T/</i> mm | s( <i>T)</i> /mm | rs(T) |
| 60SA/40LDH       |               |               |               |               |               |               |                |               |  |              |                  |       |
| 1                | 0,126         | 0,125         | 0,12          | 0,116         | 0,121         | 0,13          | 0,128          | 0,118         | 0,124  | 0,123        | 0,00156          | 0,013 |
| 2                | 0,134         | 0,131         | 0,121         | 0,125         | 0,128         | 0,134         | 0,132          | 0,129         | 0,126  | 0,129        | 0,00146          | 0,011 |
| 3                | 0,132         | 0,136         | 0,138         | 0,129         | 0,136         | 0,135         | 0,136          | 0,131         | 0,139  | 0,135        | 0,00111          | 0,008 |
| 4                | 0,131         | 0,137         | 0,136         | 0,132         | 0,135         | 0,135         | 0,137          | 0,133         | 0,139  | 0,135        | 0,00087          | 0,006 |
| 50SA/50LDH       |               |               |               |               |               |               |                |               |  |              |                  |       |
| 1                | 0,12          | 0,124         | 0,132         | 0,131         | 0,142         | 0,124         | 0,126          | 0,131         | 0,127  | 0,129        | 0,00214          | 0,017 |
| 2                | 0,116         | 0,12          | 0,13          | 0,131         | 0,132         | 0,123         | 0,124          | 0,126         | 0,128  | 0,126        | 0,00178          | 0,014 |
| 3                | 0,121         | 0,127         | 0,126         | 0,12          | 0,123         | 0,129         | 0,128          | 0,123         | 0,129  | 0,125        | 0,00115          | 0,009 |
| 4                | 0,111         | 0,115         | 0,11          | 0,111         | 0,114         | 0,113         | 0,113          | 0,113         | 0,111  | 0,112        | 0,00055          | 0,005 |
| 40SA/60LDH       |               |               |               |               |               |               |                |               | and the second s |              |                  |       |
| 1                | 0,117         | 0,114         | 0,115         | 0,117         | 0,116         | 0,121         | 0,12           | 0,116         | 0,116  | 0,117        | 0,00075          | 0,006 |
| 2                | 0,121         | 0,12          | 0,122         | 0,121         | 0,129         | 0,125         | 0,129          | 0,126         | 0,127  | 0,124        | 0,00118          | 0,009 |
| 3                | 0,122         | 0,122         | 0,125         | 0,121         | 0,127         | 0,124         | 0,124          | 0,124         | 0,13   | 0,124        | 0,00093          | 0,007 |
| 4                | 0,126         | 0,118         | 0,127         | 0,126         | 0,13          | 0,123         | 0,13           | 0,132         | 0,131  | 0,127        | 0,00148          | 0,012 |
| 30SA/70LDH       |               |               |               |               |               |               | and the second |               |  |              |                  |       |
| 1                | 0,117         | 0,116         | 0,127         | 0,121         | 0,123         | 0,12          | 0,117          | 0,124         | 0,12   | 0,121        | 0,00121          | 0,010 |
| 2                | 0,13          | 0,13          | 0,132         | 0,134         | 0,127         | 0,13          | 0,134          | 0,133         | 0,132  | 0,131        | 0,00076          | 0,006 |
| 3                | 0,125         | 0,126         | 0,126         | 0,133         | 0,131         | 0,13          | 0,134          | 0,131         | 0,13   | 0,130        | 0,00107          | 0,008 |
| 4                | 0,128         | 0,129         | 0,121         | 0,12          | 0,123         | 0,13          | 0,129          | 0,123         | 0,126  | 0,125        | 0,00126          | 0,010 |
| 20SA/80LDH       |               |               |               |               |               |               |                |               |  |              |                  |       |
| 1                | 0,133         | 0,122         | 0,132         | 0,135         | 0,135         | 0,128         | 0,133          | 0,138         | 0,135  | 0,132        | 0,00158          | 0,012 |
| 2                | 0,129         | 0,122         | 0,119         | 0,13          | 0,132         | 0,126         | 0,131          | 0,132         | 0,133  | 0,128        | 0,00163          | 0,013 |
| 3                | 0,125         | 0,118         | 0,132         | 0,125         | 0,126         | 0,126         | 0,126          | 0,134         | 0,132  | 0,127        | 0,00163          | 0,013 |
| 4                | 0,105         | 0,105         | 0,114         | 0,114         | 0,118         | 0,113         | 0,11           | 0,113         | 0,114  | 0,112        | 0,00145          | 0,013 |
| 10SA/90LDH       |               |               |               |               |               |               |                |               |  |              |                  |       |
| 1                | 0,12          | 0,132         | 0,117         | 0,106         | 0,114         | 0,143         | 0,127          | 0,118         | 0,133  | 0,123        | 0,00379          | 0,031 |
| 2                | 0,131         | 0,136         | 0,13          | 0,128         | 0,141         | 0,14          | 0,138          | 0,135         | 0,142  | 0,136        | 0,00169          | 0,012 |
| 3                | 0,113         | 0,118         | 0,121         | 0,122         | 0,123         | 0,126         | 0,129          | 0,128         | 0,131  | 0,123        | 0,00191          | 0,015 |
| 4                | 0,117         | 0,129         | 0,132         | 0,134         | 0,139         | 0,135         | 0,135          | 0,142         | 0,14   | 0,134        | 0,00248          | 0,019 |

Appendices



| Table A-0 continu         |               | ess uala n   |               | aling to Gr   | аріег 4, гі   | guie 5.       |               |               |               |              |                  |       |
|---------------------------|---------------|--------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|------------------|-------|
|                           | <i>T1</i> /mm | <b>T2/mm</b> | <i>T3</i> /mm | <i>T4</i> /mm | <i>T5</i> /mm | <b>T6/</b> mm | <i>T7</i> /mm | <b>T8/</b> mm | <b>T9</b> /mm | <i>T/</i> mm | s( <i>T)</i> /mm | rs(T) |
| 0SA/100LDH                |               |              |               |               |               |               |               |               |               |              |                  |       |
| 1                         | 0,133         | 0,13         | 0,146         | 0,15          | 0,138         | 0,139         | 0,137         | 0,147         | 0,140         | 0,140        | 0,00220          | 0,016 |
| 2                         | 0,117         | 0,137        | 0,133         | 0,125         | 0,135         | 0,133         | 0,124         | 0,122         | 0,126         | 0,128        | 0,00225          | 0,018 |
| 3                         | 0,132         | 0,126        | 0,133         | 0,130         | 0,137         | 0,135         | 0,135         | 0,133         | 0,137         | 0,133        | 0,00117          | 0,009 |
| 4                         | 0,131         | 0,135        | 0,135         | 0,132         | 0,14          | 0,135         | 0,135         | 0,138         | 0,137         | 0,135        | 0,00093          | 0,007 |
| 0SA/0LDH<br>Blank         |               |              |               |               |               |               |               |               |               |              |                  |       |
| 1                         | 0.135         | 0.138        | 0.134         | 0.132         | 0.14          | 0.14          | 0.143         | 0.145         | 0.147         | 0.139        | 0.00170          | 0.012 |
| 2                         | 0,143         | 0,147        | 0,141         | 0,136         | 0,153         | 0,148         | 0,148         | 0,131         | 0,137         | 0,143        | 0,00235          | 0,016 |
| 3                         | 0.13          | 0.139        | 0.12          | 0.123         | 0.136         | 0.138         | 0.134         | 0.127         | 0.133         | 0.131        | 0.00221          | 0.017 |
| 4                         | 0,138         | 0,142        | 0,144         | 0,145         | 0,153         | 0,146         | 0,151         | 0,152         | 0,152         | 0,147        | 0,00176          | 0,012 |
| 70SA/30Bent<br>Bentonite  | ,             |              |               | ,             |               |               |               |               | ,             | ,            |                  |       |
| 1                         | 0,126         | 0,126        | 0,129         | 0,124         | 0,12          | 0,144         | 0,123         | 0,147         | 0,12          | 0,129        | 0,00331          | 0,026 |
| 2                         | 0,123         | 0,115        | 0,112         | 0,113         | 0,111         | 0,118         | 0,122         | 0,102         | 0,103         | 0,113        | 0,00246          | 0,022 |
| 3                         | 0,124         | 0,132        | 0,138         | 0,127         | 0,132         | 0,13          | 0,128         | 0,145         | 0,131         | 0,132        | 0,00209          | 0,016 |
| 4                         | 0,117         | 0,113        | 0,116         | 0,136         | 0,122         | 0,124         | 0,145         | 0,137         | 0,146         | 0,128        | 0,00425          | 0,033 |
| 70SA/30Talc               |               |              |               |               |               |               |               |               |               |              |                  |       |
| 1                         | 0,151         | 0,142        | 0,151         | 0,155         | 0,16          | 0,16          | 0,135         | 0,142         | 0,165         | 0,151        | 0,00332          | 0,022 |
| 2                         | 0,144         | 0,164        | 0,16          | 0,17          | 0,172         | 0,161         | 0,146         | 0,15          | 0,176         | 0,160        | 0,00385          | 0,024 |
| 3                         | 0,172         | 0,124        | 0,153         | 0,149         | 0,14          | 0,177         | 0,158         | 0,142         | 0,136         | 0,150        | 0,00568          | 0,038 |
| 4                         | 0,169         | 0,104        | 0,123         | 0,141         | 0,148         | 0,142         | 0,127         | 0,133         | 0,127         | 0,135        | 0,00606          | 0,045 |
| 70SA/30LDH<br>Tap water   |               |              |               |               |               |               |               |               |               |              |                  |       |
| 1                         | 0,145         | 0,141        | 0,128         | 0,127         | 0,132         | 0,142         | 0,143         | 0,137         | 0,139         | 0,1371       | 0,00221          | 0.016 |
| 2                         | 0,129         | 0,138        | 0,127         | 0,128         | 0,144         | 0,136         | 0,137         | 0,14          | 0,143         | 0,136        | 0,00213          | 0,016 |
| 3                         | 0,128         | 0,131        | 0,123         | 0,133         | 0,134         | 0,133         | 0,134         | 0,133         | 0,141         | 0,132        | 0,00162          | 0,012 |
| 4                         | 0,12          | 0,121        | 0,117         | 0,11          | 0,122         | 0,125         | 0,124         | 0,119         | 0,124         | 0,120        | 0,00154          | 0,013 |
| 70SA/30LDH<br>38°C/90% RH |               |              |               | · ·           | · ·           |               | · · ·         |               |               | ·            |                  |       |
| 1                         | 0,122         | 0,131        | 0,127         | 0,122         | 0,125         | 0,124         | 0,127         | 0,125         | 0,124         | 0,125        | 0,00094          | 0,008 |

#### Table A-6 continued Thickness data for films relating to Chapter 4, Figure 5.



|            | t/day       | 0          | 0,104  | 0,188  | 0,271  |           |                      |       |  |                       |           |     |
|------------|-------------|------------|--------|--------|--------|-----------|----------------------|-------|--|-----------------------|-----------|-----|
|            | <i>t</i> /h | 0          | 2,5    | 4,5    | 6,5    |           |                      |       |  |                       |           |     |
| 100SA/0LDH |             | m1         | m2     | т3     | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | <b>E</b> <sub>x</sub> | Av<br>WVP | PE  |
| 1          |             | 18,239     | 18,277 | 18,306 | 18,341 | 0,374     | 0,01017              | 0,027 | 21   | 1                     | 22        | 1   |
| 2          |             | 18,087     | 18,12  | 18,145 | 18,172 | 0,313     | 0,00289              | 0,009 | 17   | 1                     |           |     |
| 3          |             | 18,234     | 18,278 | 18,312 | 18,35  | 0,426     | 0,00648              | 0,015 | 24   | 1                     |           |     |
| 4          |             | 18,442     | 18,49  | 18,527 | 18,567 | 0,460     | 0,00446              | 0,010 | 23   | 1                     |           |     |
|            | t/day       | 0          | 0,094  | 0,177  | 0,260  |           |                      |       |  |                       |           |     |
|            | <i>t</i> /h | 0          | 2,25   | 4,25   | 6,25   |           |                      |       |  |                       |           |     |
| 90SA/10LDH |             | <i>m</i> 1 | m2     | т3     | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex                    | Av<br>WVP | PE  |
| 1          |             | 19,295     | 19,315 | 19,332 | 19,35  | 0,211     | 0,00152              | 0,007 | 12   | 1                     | 16        | 1   |
| 2          |             | 18,617     | 18,652 | 18,682 | 18,714 | 0,371     | 0,00301              | 0,008 | 19   | 1                     |           |     |
| 3          |             | 18,331     | 18,356 | 18,377 | 18,399 | 0,260     | 0,00194              | 0,007 | 15   | 1                     |           |     |
| 4          |             | 18,287     | 18,313 | 18,336 | 18,36  | 0,280     | 0,00189              | 0,007 | 16   | 1                     |           |     |
|            | t/day       | 0          | 0,104  | 0,188  | 0,271  |           |                      |       |  |                       |           |     |
|            | t/h         | 0          | 2,5    | 4,5    | 6,5    |           |                      |       |  |                       |           |     |
| 80SA/20LDH |             | m1         | m2     | т3     | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | E <sub>x</sub>        | Av<br>WVP | PE  |
| 1          |             | 18,426     | 18,437 | 18,444 | 18,453 | 0,098     | 0,00312              | 0,032 | 5,0  | 0,3                   | 4,6       | 0,4 |
| 2          |             | 18,193     | 18,203 | 18,21  | 18,218 | 0,092     | 0,00166              | 0,018 | 5,0  | 0,4                   |           |     |
| 3          |             | 18,183     | 18,192 | 18,197 | 18,204 | 0,076     | 0,00356              | 0,047 | 4,5  | 0,4                   |           |     |
| 4          |             | 17 088     | 17 005 | 17 000 | 18 005 | 0.0616    | 0 00207              | 0.048 | 12   | 03                    |           |     |

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|                      | t/day         | 0          | 0,083  | 0,146  | 0,229  |           |                      |       |  |                       |           |     |
|----------------------|---------------|------------|--------|--------|--------|-----------|----------------------|-------|--|-----------------------|-----------|-----|
|                      | t∕h           | 0          | 2      | 3,5    | 5,5    |           |                      |       |  |                       |           |     |
| 70SA/30LDH<br>60 min |               | m1         | m2     | т3     | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex                    | Av<br>WVP | PE  |
| 1                    |               | 18,485     | 18,494 | 18,5   | 18,512 | 0,116     | 0,00743              | 0,064 | 6,2  | 0,5                   | 6,8       | 0,5 |
| 2                    |               | 18,359     | 18,369 | 18,376 | 18,389 | 0,130     | 0,00717              | 0,055 | 7,0  | 0,6                   |           |     |
| 3                    |               | 18,39      | 18,401 | 18,408 | 18,421 | 0,134     | 0,00593              | 0,044 | 7,2  | 0,5                   |           |     |
| 4                    |               | 18,521     | 18,532 | 18,539 | 18,553 | 0,138     | 0,00803              | 0,058 | 6,8  | 0,6                   |           |     |
|                      | <i>t</i> /day | 0          | 0,104  | 0,188  | 0,271  |           |                      |       |  |                       |           |     |
|                      | t/h           | 0          | 2,5    | 4,5    | 6,5    |           |                      |       |  |                       |           |     |
| 60SA/40LDH           |               | <i>m</i> 1 | m2     | т3     | m4     | S/(g/day) | s(S)/(g/day)         | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>dav <sup>-1</sup> .kPa <sup>-1</sup> ) | <b>E</b> <sub>x</sub> | Av<br>WVP | PE  |
| 1                    |               | 18,33      | 18,338 | 18,344 | 18,352 | 0,080     | 0,00347              | 0,043 | 4,0  | 0,3                   | 4,5       | 0,4 |
| 2                    |               | 18,294     | 18,302 | 18,309 | 18,318 | 0,088     | 0,00508              | 0,058 | 4,6  | 0,4                   |           |     |
| 3                    |               | 18,236     | 18,244 | 18,251 | 18,26  | 0,088     | 0,00508              | 0,058 | 4,8  | 0,4                   |           |     |
| 4                    |               | 18,056     | 18,063 | 18,069 | 18,078 | 0,080     | 0,00672              | 0,084 | 4,4  | 0,4                   |           |     |
|                      | t/day         | 0          | 0,104  | 0,188  | 0,271  |           |                      |       |  |                       |           |     |
|                      | ť/h           | 0          | 2,5    | 4,5    | 6,5    |           |                      |       |  |                       |           |     |
| 50SA/50LDH           |               | m1         | m2     | т3     | m4     | S/(g/day) | s(S)/(g/day)         | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex                    | Av<br>WVP | PE  |
| 1                    |               | 18,374     | 18,39  | 18,4   | 18,411 | 0,135     | 0,00506              | 0,037 | 7,1  | 0,5                   | 6,1       | 0,4 |
| 2                    |               | 18,124     | 18,138 | 18,147 | 18,156 | 0,118     | 0,00493              | 0,042 | 6,0  | 0,4                   |           |     |
| 3                    |               | 18,27      | 18,281 | 18,289 | 18,299 | 0,106     | 0,00306              | 0,029 | 5,4  | 0,3                   |           |     |
| 4                    |               | 18,292     | 18,307 | 18,316 | 18,327 | 0,128     | 0,00483              | 0,038 | 5,9  | 0,4                   |           |     |



|            | t/day         | 0          | 0,094  | 0,177      | 0,260  |           |                      |       |  |                |           |     |
|------------|---------------|------------|--------|------------|--------|-----------|----------------------|-------|--|----------------|-----------|-----|
|            | t∕h           | 0          | 2,25   | 4,25       | 6,25   |           |                      |       |  |                |           |     |
| 40SA/60LDH |               | m1         | m2     | т3         | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex             | Av<br>WVP | PE  |
| 1          |               | 18,282     | 18,298 | 18,312     | 18,327 | 0,172     | 0,00176              | 0,010 | 8,2  | 0,5            | 8,6       | 0,5 |
| 2          |               | 18,053     | 18,069 | 18,083     | 18,095 | 0,162     | 0,00445              | 0,027 | 8,2  | 0,5            |           |     |
| 3          |               | 17,894     | 17,911 | 17,924     | 17,939 | 0,171     | 0,00347              | 0,020 | 8,7  | 0,5            |           |     |
| 4          |               | 18,707     | 18,723 | 18,737     | 18,753 | 0,176     | 0,00379              | 0,022 | 9,1  | 0,6            |           |     |
|            | <i>t</i> /dav | 0          | 0.083  | 0.167      | 0.25   |           |                      |       |  |                |           |     |
|            | ťh            | 0          | 2      | 4          | 6      |           |                      |       |  |                |           |     |
| 30SA/70LDH |               | <i>m</i> 1 | m2     | т3         | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>dav <sup>-1</sup> kPa <sup>-1</sup> )  | E <sub>x</sub> | Av<br>WVP | PE  |
| 1          |               | 18,196     | 18,208 | 18,222     | 18,234 | 0,154     | 0,00339              | 0,022 | 7,6  | 0,5            | 9,0       | 0.5 |
| 2          |               | 18,199     | 18,214 | 18,229     | 18,243 | 0,176     | 0,00208              | 0,012 | 9,5  | 0,5            | ·         | ·   |
| 3          |               | 18,588     | 18,603 | 18,618     | 18,634 | 0,184     | 0,00208              | 0,011 | 9,7  | 0,6            |           |     |
| 4          |               | 18,155     | 18,17  | 18,184     | 18,2   | 0,179     | 0,00317              | 0,018 | 9,2  | 0,5            |           |     |
|            | #day          | 0          | 0 104  | 0 199      | 0.271  |           |                      |       |  |                |           |     |
|            | vuay<br>t∕h   | 0          | 25     | 4.5        | 65     |           |                      |       |  |                |           |     |
|            | 411           | 0          | 2,0    | т,5        | 0,0    |           |                      |       | WVP,/  |                |           |     |
| 20SA/80LDH |               | m1         | m2     | <i>m</i> 3 | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | (g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> )                            | Ex             | AV<br>WVP | PE  |
| 1          |               | 18,141     | 18,174 | 18,2       | 18,228 | 0,320     | 0,00347              | 0,011 | 17   | 1              | 17        | 1   |
| 2          |               | 18,379     | 18,412 | 18,44      | 18,473 | 0,345     | 0,01288              | 0,037 | 18   | 1              |           |     |
| 3          |               | 18,002     | 18,035 | 18,062     | 18,092 | 0,331     | 0,00707              | 0,021 | 17   | 1              |           |     |
| 4          |               | 18,061     | 18,098 | 18,126     | 18,158 | 0,356     | 0,00612              | 0,017 | 16   | 1              |           |     |



|                   | t/day         | 0      | 0,104  | 0,188  | 0,271  |           |                      |       |  |                |           |    |
|-------------------|---------------|--------|--------|--------|--------|-----------|----------------------|-------|--|----------------|-----------|----|
|                   | t/h           | 0      | 2,5    | 4,5    | 6,5    |           |                      |       |  |                |           |    |
| 10SA/90LDH        |               | m1     | m2     | т3     | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex             | Av<br>WVP | PE |
| 1                 |               | 18,346 | 18,383 | 18,409 | 18,439 | 0,341     | 0,00623              | 0,018 | 17   | 1              | 21        | 1  |
| 2                 |               | 18,329 | 18,37  | 18,398 | 18,433 | 0,380     | 0,01010              | 0,027 | 21   | 1              |           |    |
| 3                 |               | 18,001 | 18,049 | 18,084 | 18,124 | 0,451     | 0,00721              | 0,016 | 23   | 1              |           |    |
| 4                 |               | 18,411 | 18,456 | 18,488 | 18,525 | 0,418     | 0,00743              | 0,018 | 23   | 1              |           |    |
|                   | <i>t</i> /day | 0      | 0,104  | 0,188  | 0,271  |           |                      |       |  |                |           |    |
|                   | t/h           | 0      | 2,5    | 4,5    | 6,5    |           |                      |       |  |                |           |    |
| 0SA/100LDH        |               | m1     | m2     | т3     | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>*</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>dav <sup>-1</sup> .kPa <sup>-1</sup> ) | E <sub>x</sub> | Av<br>WVP | PE |
| 1                 |               | 18,382 | 18,43  | 18,464 | 18,505 | 0,450     | 0,01007              | 0,022 | 26   | 2              | 24        | 1  |
| 2                 |               | 18,252 | 18,294 | 18,324 | 18,361 | 0,398     | 0,01024              | 0,026 | 21   | 1              |           |    |
| 3                 |               | 18,328 | 18,376 | 18,41  | 18,451 | 0,450     | 0,01007              | 0,022 | 24   | 1              |           |    |
| 4                 |               | 18,361 | 18,409 | 18,444 | 18,486 | 0,457     | 0,01033              | 0,023 | 25   | 2              |           |    |
|                   | t/day         | 0      | 0,083  | 0,167  | 0,25   |           |                      |       |  |                |           |    |
|                   | ť/h           | 0      | 2      | 4      | 6      |           |                      |       |  |                |           |    |
| 0SA/0LDH<br>Blank |               | m1     | m2     | т3     | m4     | S/(g/day) | s(S)/(g/day)         | rs(S) | <i>WVP<sub>*</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>dav <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex             | Av<br>WVP | PE |
| 1                 |               | 18,101 | 18,138 | 18,173 | 18,215 | 0,452     | 0,01218              | 0,027 | 26   | 2              | 26        | 2  |
| 2                 |               | 18,15  | 18,186 | 18,223 | 18,259 | 0,437     | 0,00170              | 0,004 | 25   | 1              |           |    |
| 3                 |               | 18,187 | 18,224 | 18,262 | 18,301 | 0,456     | 0,00379              | 0,008 | 24   | 1              |           |    |
| 4                 |               | 17,86  | 17,898 | 17,936 | 17,975 | 0,460     | 0,00208              | 0,005 | 28   | 2              |           |    |



|                          | <i>t</i> /day | 0      | 0,083      | 0,146      | 0,229     |           |                      |       |  |                |           |     |
|--------------------------|---------------|--------|------------|------------|-----------|-----------|----------------------|-------|--|----------------|-----------|-----|
|                          | <i>t</i> /h   | 0      | 2          | 3,5        | 5,5       |           |                      |       |  |                |           |     |
| 70SA/30Bent<br>Bentonite |               | m1     | m2         | т3         | m4        | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex             | Av<br>WVP | PE  |
| 1                        |               | 18,763 | 18,778     | 18,788     | 18,805    | 0,182     | 0,00593              | 0,033 | 9,6  | 0,7            | 9,4       | 0,7 |
| 2                        |               | 17,846 | 17,867     | 17,88      | 17,901    | 0,238     | 0,00574              | 0,024 | 11,0   | 0,7            |           |     |
| 3                        |               | 18,419 | 18,428     | 18,434     | 18,444    | 0,108     | 0,00315              | 0,029 | 5,8  | 0,4            |           |     |
| 4                        |               | 18,351 | 18,369     | 18,381     | 18,401    | 0,216     | 0,00631              | 0,029 | 11,4   | 0,8            |           |     |
|                          | t/day         | 0      | 0 104      | 0 188      | 0.271     |           |                      |       |  |                |           |     |
|                          | t/h           | 0      | 2.5        | 4.5        | 65        |           |                      |       |  |                |           |     |
|                          | 411           | 0      | 2,5        | 4,5        | 0,5       |           |                      |       | WVPJ   |                |           |     |
| 70SA/30Talc              |               | m1     | <i>m</i> 2 | т3         | <i>m4</i> | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | (g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> )                            | Ex             | Av<br>WVP | PE  |
| 1                        |               | 18,329 | 18,343     | 18,35      | 18,363    | 0,122     | 0,00868              | 0,071 | 7,5  | 0,7            | 7,3       | 0,6 |
| 2                        |               | 18,013 | 18,022     | 18,027     | 18,035    | 0,079     | 0,00437              | 0,055 | 5,2  | 0,4            |           |     |
| 3                        |               | 18,214 | 18,228     | 18,237     | 18,249    | 0,127     | 0,00437              | 0,034 | 7,8  | 0,6            |           |     |
| 4                        |               | 17,959 | 17,976     | 17,988     | 18,003    | 0,161     | 0,00437              | 0,027 | 8,9  | 0,7            |           |     |
|                          | <i>t</i> /dav | 0      | 0.083      | 0.167      | 0.25      |           |                      |       |  |                |           |     |
|                          | t/h           | 0      | 2          | 4          | 6         |           |                      |       |  |                |           |     |
| 70SA/30LDH<br>10 min     |               | m1     | m2         | <i>m</i> 3 | m4        | S/(g/day) | s(S)/(g/day)         | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>dav <sup>-1</sup> .kPa <sup>-1</sup> ) | E <sub>x</sub> | Av<br>WVP | PE  |
| 1                        |               | 18,256 | 18,275     | 18,297     | 18,322    | 0,26      | 0,01138              | 0,04  | 14   | 1              | 15        | 1   |
| 2                        |               | 18,294 | 18,311     | 18,332     | 18,353    | 0,24      | 0,00831              | 0,03  | 13   | 1              |           |     |
| 3                        |               | 18,14  | 18,161     | 18,183     | 18,203    | 0,25      | 0,00317              | 0,01  | 14   | 1              |           |     |
| 4                        |               | 18,1   | 18,128     | 18,157     | 18,19     | 0,36      | 0,00982              | 0,03  | 17   | 1              |           |     |



|                           | t/day       | 0          | 0,083  | 0,167      | 0,25   |           |                      |       |  |                       |           |     |
|---------------------------|-------------|------------|--------|------------|--------|-----------|----------------------|-------|--|-----------------------|-----------|-----|
|                           | t/h         | 0          | 2      | 4          | 6      |           |                      |       |  |                       |           |     |
| 70SA/30LDH<br>30 min      |             | m1         | m2     | т3         | m4     | S/(g/day) | <i>s(S)</i> /(g/day) | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | Ex                    | Av<br>WVP | PE  |
| 1                         |             | 18,354     | 18,37  | 18,383     | 18,403 | 0,19      | 0,01138              | 0,06  | 11,5   | 0,9                   | 10,5      | 0,8 |
| 2                         |             | 18,035     | 18,048 | 18,06      | 18,078 | 0,17      | 0,01119              | 0,07  | 9,5  | 0,9                   |           |     |
| 3                         |             | 18,062     | 18,077 | 18,091     | 18,109 | 0,19      | 0,00710              | 0,04  | 10,0   | 0,7                   |           |     |
| 4                         |             | 18,236     | 18,253 | 18,271     | 18,291 | 0,22      | 0,00575              | 0,03  | 10,9   | 0,7                   |           |     |
|                           |             |            |        |            |        |           |                      |       |  |                       |           |     |
|                           | t/day       | 0          | 0,083  | 0,167      | 0,25   |           |                      |       |  |                       |           |     |
|                           | <i>t</i> /h | 0          | 2      | 4          | 6      |           |                      |       |  |                       |           |     |
| 60SA/40LDH<br>Tap water   |             | <i>m</i> 1 | m2     | <i>m</i> 3 | m4     | S/(g/day) | s(S)/(g/day)         | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | <b>E</b> <sub>x</sub> | Av<br>WVP | PE  |
| 1                         |             | 18,18      | 18,192 | 18,204     | 18,215 | 0,14      | 0,00208              | 0,01  | 7,9  | 0,5                   | 7,6       | 0,5 |
| 2                         |             | 18,336     | 18,346 | 18,357     | 18,369 | 0,13      | 0,00379              | 0,03  | 7,3  | 0,5                   |           |     |
| 3                         |             | 18,548     | 18,557 | 18,569     | 18,581 | 0,13      | 0,00624              | 0,05  | 7,2  | 0,5                   |           |     |
| 4                         |             | 18,606     | 18,619 | 18,632     | 18,646 | 0,16      | 0,00208              | 0,01  | 7,8  | 0,5                   |           |     |
|                           |             |            |        |            |        |           |                      |       |  |                       |           |     |
|                           | t/day       | 0          | 0,104  | 0,292      |        |           |                      |       |  |                       |           |     |
|                           | <i>t</i> /h | 0          | 2,5    | 7          |        |           |                      |       |  |                       |           |     |
| 60SA/40LDH<br>38 C/90% RH |             | <i>m</i> 1 | m2     | т3         | m4     | S/(g/day) | s(S)/(g/day)         | rs(S) | <i>WVP<sub>x</sub>/</i><br>(g.mm.m <sup>-2</sup> .<br>day <sup>-1</sup> .kPa <sup>-1</sup> ) | <b>E</b> <sub>x</sub> | Av<br>WVP | PE  |
| 1                         |             | 18,039     | 18,105 | 18,231     |        | 0,66      | 0,01021              | 0.02  | 13,5   | 0,5                   | -         | -   |

# Appendix E

## Tensile data

Table A-8 gives the thickness data of the film tested. The width of the tensile specimens (at the middle of the dumbbells) were 6,2 mm and the gage length were 35 mm in all cases. These values were used by the Nexygen program from Lloyd Instruments to calculate the different parameters in Table A-9. The stress at break, % strain at break and the Young's modulus of samples of the same composition were averaged and the standard deviations of the averages were calculated in order to plot the graphs in Figures 12-14 (Chapter 4).

| Film              | _       | 5  | Sampl    | е <u>т</u> 1/ | mm        | T2/mm   | , · · | T.3/mm  | <i>T</i> /mr | n        |
|-------------------|---------|----|----------|---------------|-----------|---------|-------|---------|--------------|----------|
| composit          | ion     | r  | numbe    | er            |           |         |       |         |              |          |
| 100SA/0L          | .DH     |    | 1        | 0,1           | 54        | 0,113   |       | 0,169   | 0,14         | 5        |
|                   |         |    | 2        | 0,1           | /1        | 0,167   |       | 0,168   | 0,169        | )        |
| 90SA/10L          | .DH     |    | 1        | 0,1           | 21        | 0,114   |       | 0,114   | 0,110        | 5        |
|                   |         |    | 2        | 0,1           | 15        | 0,113   |       | 0,118   | 0,11         | 5        |
|                   |         |    | 3        | 0,1           | 16        | 0,113   |       | 0,118   | 0,110        | 3        |
| 80SA/20L          | .DH     |    | 1        | 0,0           | 90        | 0,132   |       | 0,138   | 0,120        | )        |
|                   |         |    | 2        | 0,1           | 19        | 0,130   |       | 0,105   | 0,118        | 3        |
|                   |         |    | 3        | 0,1           | 35        | 0,126   |       | 0,129   | 0,130        | )        |
| 70SA/30L          | .DH     |    | 1        | 0,1           | 18        | 0,123   |       | 0,120   | 0,120        | )        |
|                   |         |    | 2        | 0,1           | 18        | 0,112   |       | 0,112   | 0,114        | 4        |
|                   |         |    | 3        | 0,1           | 06        | 0,110   |       | 0,104   | 0,10         | 7        |
| 60SA/40L          | .DH     |    | 1        | 0,1           | 26        | 0,126   |       | 0,123   | 0,12         | 5        |
|                   |         |    | 2        | 0,1           | 27        | 0,124   |       | 0,118   | 0,123        | 3        |
|                   |         |    | 3        | 0,1           | 23        | 0,122   |       | 0,120   | 0,122        | 2        |
|                   |         |    | 4        | 0,1           | 21        | 0,127   |       | 0,130   | 0,120        | 3        |
| 50SA/50L          | .DH     |    | 1        | 0.1           | 19        | 0,123   |       | 0,132   | 0.12         | 5        |
|                   |         |    | 2        | 0.1           | 22        | 0.129   |       | 0.133   | 0.128        | 3        |
|                   |         |    | 3        | 0.1           | 27        | 0.127   |       | 0.145   | 0.13         | 3        |
| 40SA/60L          | DH      |    | 1        | 0.1           | 37        | 0.131   |       | 0.134   | 0.13         | 4        |
|                   |         |    | 2        | 0.1           | 28        | 0 127   |       | 0 128   | 0 128        | 3        |
|                   |         |    | 3        | 0,1           | 04        | 0 1 1 0 |       | 0 130   | 0,12         | 5        |
| 3054/701          | рн      |    | 1        | 0,1           | 26        | 0 131   |       | 0 127   | 0,11         | 2        |
| 303A//01          |         |    | 2        | 0,1           | 20        | 0,101   |       | 0,127   | 0,120        | ן<br>1   |
|                   |         |    | 2        | 0,1           | 20        | 0,120   |       | 0,111   | 0,12         | ı<br>1   |
|                   |         |    | 1        | 0,1           | 20        | 0,110   |       | 0,090   | 0,11         | י<br>ר   |
| 109 / /001        | РΠ      |    | 4        | 0,1           | 96        | 0,129   |       | 0,13    | 0,130        | ן<br>ר   |
| 1034/901          | .00     |    | ו<br>ר   | 0,0           | 21        | 0,105   |       | 0,107   | 0,09         | ש<br>כ   |
|                   |         |    | 2        | 0,1           | 21        | 0,119   |       | 0,120   | 0,12         | с<br>С   |
| 06 4 /4 0 01      | пп      |    | <u>ح</u> | 0,1           | 21        | 0,121   |       | 0,127   | 0,12         | 2<br>7   |
| 05A/100L          | . Оп    |    | ו<br>ר   | 0,0           | 193       | 0,070   |       | 0,090   | 0,00         | י<br>ר   |
|                   |         |    | 2        | 0,0           | 197       | 0,060   |       | 0,110   | 0,090        | 2        |
| Disci             |         |    | 3        | 0,1           | 15        | 0,098   |       | 0,106   | 0,100        | 2<br>-   |
| Blank             |         |    | 1        | 0,1           | 69<br>50  | 0,161   |       | 0,165   | 0,16         | 2        |
|                   |         |    | 2        | 0,1           | 58        | 0,163   |       | 0,150   | 0,15         | (<br>    |
|                   |         |    | 3        | 0,1           | 59        | 0,160   |       | 0,158   | 0,15         | 9        |
| 700 4 /0          |         |    | 4        | 0,1           | 60        | 0,149   |       | 0,159   | 0,150        | C        |
| 705A/3<br>Bontoni | U<br>to |    | 1        | 0,1           | 02        | 0,096   |       | 0,096   | 0,098        | 3        |
| Dentom            | le      |    | 2        | 0.1           | 00        | 0 106   |       | 0 003   | 0 10         | 2        |
|                   |         |    | 2        | 0,1           | 09        | 0,100   |       | 0,095   | 0,10         | ר<br>2   |
| 7094/3            | 0       |    | 5        | 0,0           | 90        | 0,100   |       | 0,100   | 0,10         | <u> </u> |
| 703A/3<br>Talc    | U       |    | 1        | 0,            | 13        | 0,124   |       | 0,133   | 0,129        | 9        |
| Taic              |         |    | 2        | 0.1           | 22        | 0 128   |       | 0 1 2 6 | 0 12         | 5        |
|                   |         |    | 2        | 0,1           | 17        | 0 112   |       | 0 120   | 0,12         | 5        |
| Ma stear          | ate*    |    | 1        | 0,1           | 43        | 0.16/   |       | 0 151   | 0.15         | י<br>ג   |
| wy stedie         | ale     |    | י<br>ר   | 0,1           |           | 0,104   |       | 0,131   | 0,15         | ך<br>א   |
|                   |         |    | 2        | 0,1           | ∠ ı<br>37 | 0,170   |       | 0,177   | 0,100        | 5        |
| * Maaa            | 0/      | of | ۍ<br>Ma  | U, I          | 37<br>in  | film    | ic    | 0,120   | 0,13         | ر<br>~   |
| 11/1022           | /0      | 01 | ivig     | Siearale      | 111       | 111111  | 12    | Same    | a 3          | 5        |

Table A-8 Thickness data for films shown in Figures 12-14 (Chapter 4).

and

LDH



|             | •      |        | , ,,          |              |             |            | J.         |
|-------------|--------|--------|---------------|--------------|-------------|------------|------------|
| Film        | Sample | Max    | Deflection at | Stress at    | % Strain at | Work to    | Stiffness/ |
| composition | number | Load/N | Max Load/mm   | Max Load/MPa | Max Load    | Max Load/J | (N/m)      |
| 100SA/0LDH  | 1      | 1,730  | 25,705        | 1,924        | 73,443      | 0,022      | 76,519     |
|             | 2      | 1,802  | 34,210        | 1,720        | 97,743      | 0,031      | 63,276     |
| 90SA/10LDH  | 1      | 1,092  | 28,469        | 1,531        | 81,340      | 0,016      | 87,969     |
|             | 2      | 1,444  | 32,694        | 2,007        | 93,410      | 0,023      | 81,120     |
|             | 3      | 1,463  | 30,130        | 1,967        | 86,086      | 0,021      | 87,202     |
| 80SA/20LDH  | 1      | 1,548  | 25,785        | 2,080        | 73,672      | 0,022      | 142,204    |
|             | 2      | 1,606  | 28,639        | 2,195        | 81,827      | 0,025      | 133,865    |
|             | 3      | 1,565  | 24,390        | 1,942        | 69,686      | 0,022      | 275,982    |
| 70SA/30LDH  | 1      | 1,057  | 33,533        | 1,495        | 95,810      | 0,019      | 192,018    |
|             | 2      | 0,950  | 28,367        | 1,432        | 81,049      | 0,015      | 203,714    |
| 60SA/40LDH  | 1      | 1,318  | 28,689        | 1,701        | 81,968      | 0,021      | 295,635    |
|             | 2      | 1,317  | 28,620        | 1,726        | 81,772      | 0,021      | 235,382    |
|             | 3      | 1,154  | 23,623        | 1,526        | 67,495      | 0,016      | 324,472    |
|             | 4      | 1,385  | 27,553        | 1,773        | 78,723      | 0,021      | 248,483    |
| 50SA/50LDH  | 1      | 1,085  | 33,916        | 1,400        | 96,901      | 0,021      | 129,356    |
|             | 2      | 1,206  | 34,131        | 1,520        | 97,516      | 0,023      | 157,327    |
|             | 3      | 1,390  | 34,561        | 1,686        | 98,746      | 0,026      | 137,983    |
| 40SA/60LDH  | 1      | 1,121  | 37,242        | 1,349        | 106,407     | 0,023      | 109,635    |
|             | 2      | 1,181  | 36,461        | 1,488        | 104,176     | 0,024      | 93,644     |
|             | 3      | 0,872  | 23,578        | 1,223        | 67,366      | 0,012      | 75,461     |
| 30SA/70LDH  | 1      | 1,377  | 34,483        | 1,735        | 98,524      | 0,024      | 82,955     |
|             | 3      | 1,105  | 24,928        | 1,606        | 71,222      | 0,015      | 99,109     |
| 10SA/90LDH  | 1      | 1,180  | 23,537        | 1,922        | 67,248      | 0,013      | 62,112     |
|             | 2      | 1,755  | 34,777        | 2,301        | 99,364      | 0,028      | 69,010     |
|             | 3      | 1,514  | 33,507        | 1,985        | 95,735      | 0,024      | 59,174     |
| 0SA/100LDH  | 1      | 2,030  | 28,099        | 3,763        | 80,283      | 0,027      | 92,840     |
|             | 2      | 1,964  | 25,084        | 3,233        | 71,670      | 0,023      | 95,477     |
|             | 3      | 2,493  | 31,625        | 3,793        | 90,356      | 0,036      | 96,515     |

Table A-9 Various parameters calculated by the Nexygen software from Lloyd Instruments for the films shown in Figures 12-14 (Chapter 4).



| Film composition | Sample<br>number | Max<br>Load/N | Deflection at<br>Max Load/mm | Stress at<br>Max Load/MPa | % Strain at<br>Max Load | Work to<br>Max Load/J | Stiffness/<br>(N/m) |
|------------------|------------------|---------------|------------------------------|---------------------------|-------------------------|-----------------------|---------------------|
| Blank            | 1                | 2,824         | 42,433                       | 2,761                     | 121,236                 | 0,048                 | 102,815             |
|                  | 2                | 2,705         | 37,802                       | 2,779                     | 108,006                 | 0,040                 | 112,979             |
|                  | 3                | 2,941         | 39,267                       | 2,983                     | 112,193                 | 0,046                 | 121,961             |
|                  | 4                | 2,274         | 32,712                       | 2,351                     | 93,464                  | 0,029                 | 114,249             |
| 70SA/30          |                  |               |                              |                           |                         |                       |                     |
| Bentonite        | 1                | 1,697         | 25,704                       | 2,793                     | 73,440                  | 0,022                 | 94,945              |
|                  | 3                | 1,442         | 27,319                       | 2,258                     | 78,054                  | 0,020                 | 69,240              |
| 70SA/30 Talc     | 1                | 1,326         | 42,225                       | 1,657                     | 120,642                 | 0,026                 | 39,624              |
|                  | 2                | 1,324         | 44,070                       | 1,708                     | 125,915                 | 0,028                 | 38,144              |
|                  | 3                | 1,107         | 37,835                       | 1,539                     | 108,101                 | 0,020                 | 37,683              |
| Mg stearate*     | 1                | 1,101         | 34,950                       | 1,161                     | 99,857                  | 0,023                 | 221,533             |
|                  | 2                | 1,058         | 27,158                       | 1,080                     | 77,594                  | 0,017                 | 191,039             |
|                  | 3                | 1,303         | 31,532                       | 1,556                     | 90,091                  | 0,022                 | 145,907             |

\* Mass % of Mg stearate in film is same as sum of SA and LDH



Table A-9 continued Various parameters calculated by the Nexygen software from Lloyd Instruments for the films shown in Figures 12-14 (Chapter 4).

| Film        | Sample | Young's     | Load at | Deflection at | Stress at | % Strain at | Work to |
|-------------|--------|-------------|---------|---------------|-----------|-------------|---------|
| composition | number | Modulus/MPa | Break/N | Break/mm      | Break/MPa | Break       | Break/J |
| 100SA/0LDH  | 1      | 2,979       | 1,557   | 25,773        | 1,732     | 73,639      | 0,022   |
|             | 2      | 2,114       | 1,622   | 34,938        | 1,548     | 99,822      | 0,032   |
| 90SA/10LDH  | 1      | 4,318       | 0,983   | 28,710        | 1,378     | 82,030      | 0,017   |
|             | 2      | 3,948       | 1,299   | 32,982        | 1,807     | 94,233      | 0,024   |
|             | 3      | 4,102       | 1,317   | 30,224        | 1,770     | 86,355      | 0,021   |
| 80SA/20LDH  | 1      | 6,690       | 1,393   | 25,908        | 1,872     | 74,023      | 0,022   |
|             | 2      | 6,404       | 1,445   | 28,808        | 1,975     | 82,309      | 0,025   |
|             | 3      | 11,984      | 1,408   | 24,558        | 1,747     | 70,165      | 0,022   |
| 70SA/30LDH  | 1      | 9,509       | 0,951   | 33,902        | 1,346     | 96,862      | 0,019   |
|             | 2      | 10,748      | 0,855   | 28,683        | 1,289     | 81,950      | 0,015   |
| 60SA/40LDH  | 1      | 13,351      | 1,186   | 29,107        | 1,531     | 83,163      | 0,022   |
|             | 2      | 10,803      | 1,185   | 29,011        | 1,554     | 82,888      | 0,021   |
|             | 3      | 15,014      | 1,039   | 23,967        | 1,373     | 68,476      | 0,016   |
|             | 4      | 11,133      | 1,246   | 27,685        | 1,595     | 79,101      | 0,021   |
| 50SA/50LDH  | 1      | 5,842       | 0,976   | 34,097        | 1,260     | 97,420      | 0,021   |
|             | 2      | 6,939       | 1,086   | 34,345        | 1,368     | 98,128      | 0,023   |
|             | 3      | 5,857       | 1,251   | 34,720        | 1,518     | 99,200      | 0,026   |
| 40SA/60LDH  | 1      | 4,619       | 1,009   | 37,359        | 1,214     | 106,740     | 0,024   |
|             | 2      | 4,130       | 1,063   | 36,544        | 1,340     | 104,410     | 0,024   |
|             | 3      | 3,704       | 0,785   | 23,911        | 1,101     | 68,318      | 0,012   |
| 30SA/70LDH  | 1      | 3,659       | 1,240   | 35,021        | 1,562     | 100,060     | 0,025   |
|             | 3      | 5,040       | 0,995   | 25,299        | 1,445     | 72,283      | 0,015   |
| 10SA/90LDH  | 1      | 3,542       | 1,062   | 23,780        | 1,730     | 67,942      | 0,014   |
|             | 2      | 3,167       | 1,579   | 35,106        | 2,071     | 100,304     | 0,029   |
|             | 3      | 2,716       | 1,362   | 33,582        | 1,787     | 95,949      | 0,024   |
| 0SA/100LDH  | 1      | 6,024       | 1,827   | 29,124        | 3,387     | 83,213      | 0,029   |
|             | 2      | 5,500       | 1,768   | 25,104        | 2,910     | 71,727      | 0,023   |
|             | 3      | 5,140       | 2,244   | 31,698        | 3,414     | 90,565      | 0,036   |



| Film composition | Sample<br>number | Young's<br>Modulus/MPa | Load at<br>Break/N | Deflection at<br>Break/mm | Stress at<br>Break/MPa | % Strain at<br>Break | Work to<br>Break/J |
|------------------|------------------|------------------------|--------------------|---------------------------|------------------------|----------------------|--------------------|
| Blank            | 1                | 3,518                  | 2,542              | 42,501                    | 2,485                  | 121,431              | 0,048              |
|                  | 2                | 4,062                  | 2,434              | 37,871                    | 2,501                  | 108,202              | 0,041              |
|                  | 3                | 4,330                  | 2,647              | 39,361                    | 2,685                  | 112,461              | 0,046              |
|                  | 4                | 4,134                  | 2,047              | 32,892                    | 2,116                  | 93,977               | 0,030              |
| 70SA/30          |                  |                        |                    |                           |                        |                      |                    |
| Bentonite        | 1                | 5,469                  | 1,527              | 26,035                    | 2,513                  | 74,385               | 0,023              |
|                  | 3                | 3,795                  | 1,298              | 27,428                    | 2,032                  | 78,365               | 0,020              |
| 70SA/30          |                  |                        |                    |                           |                        |                      |                    |
| Talc             | 1                | 1,734                  | 1,193              | 42,976                    | 1,492                  | 122,788              | 0,027              |
|                  | 2                | 1,723                  | 1,191              | 44,665                    | 1,537                  | 127,613              | 0,028              |
|                  | 3                | 1,834                  | 0,996              | 38,882                    | 1,385                  | 111,092              | 0,021              |
| Mg stearate*     | 1                | 8,174                  | 0,991              | 35,511                    | 1,045                  | 101,461              | 0,023              |
|                  | 2                | 6,826                  | 0,952              | 27,477                    | 0,972                  | 78,505               | 0,017              |
|                  | 3                | 6,101                  | 1,172              | 31,725                    | 1,401                  | 90,643               | 0,022              |

\* Mass % of Mg stearate in film is same as sum of SA and LDH